

STRUCTURAL CALCULATIONS

Location:

S.R. 618 Hillsborough County

Prepared for:

Tampa Hillsborough County Expressway Authority

Prepared by:

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Certificate of Authorization No. 696

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Florida P.E # 42690

MARCH 2020

This item has been digitally signed and sealed by Jorge L. Perez on the date indicated here.
Printed copies of this document are not considered signed and sealed and the signature must
be verified on any electronic copies.

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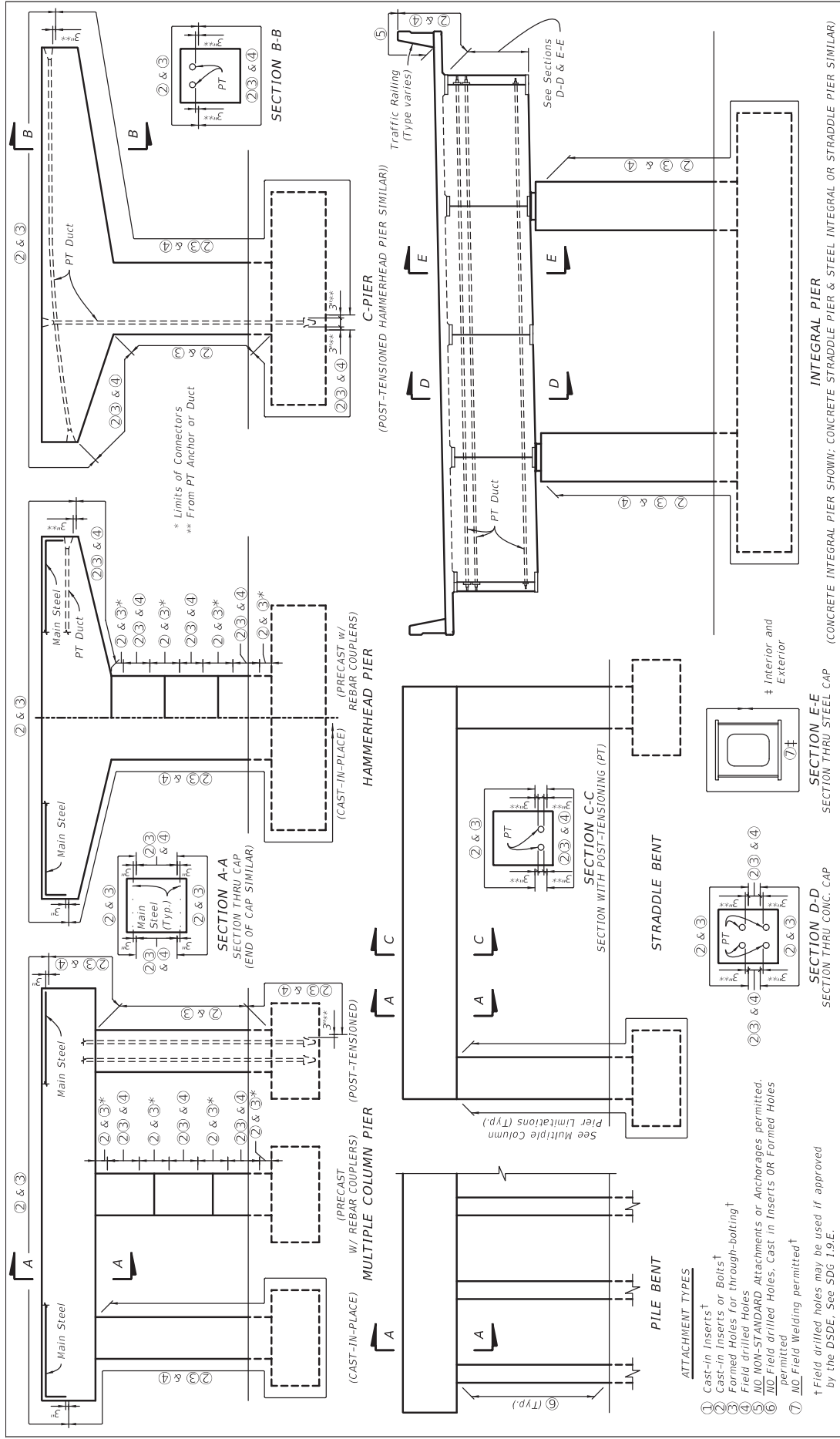
Summary :

The following structures for THEA have been analyzed through STAAD to ensure structural reliability and efficiency. Through the LTS 2017 Interim Revisions and the LTS 2015 1st edition the preceding wind loads and load combinations have been applied. Other programs utilized include Mathcad, HILTI, and Tedds for the connection assessment.



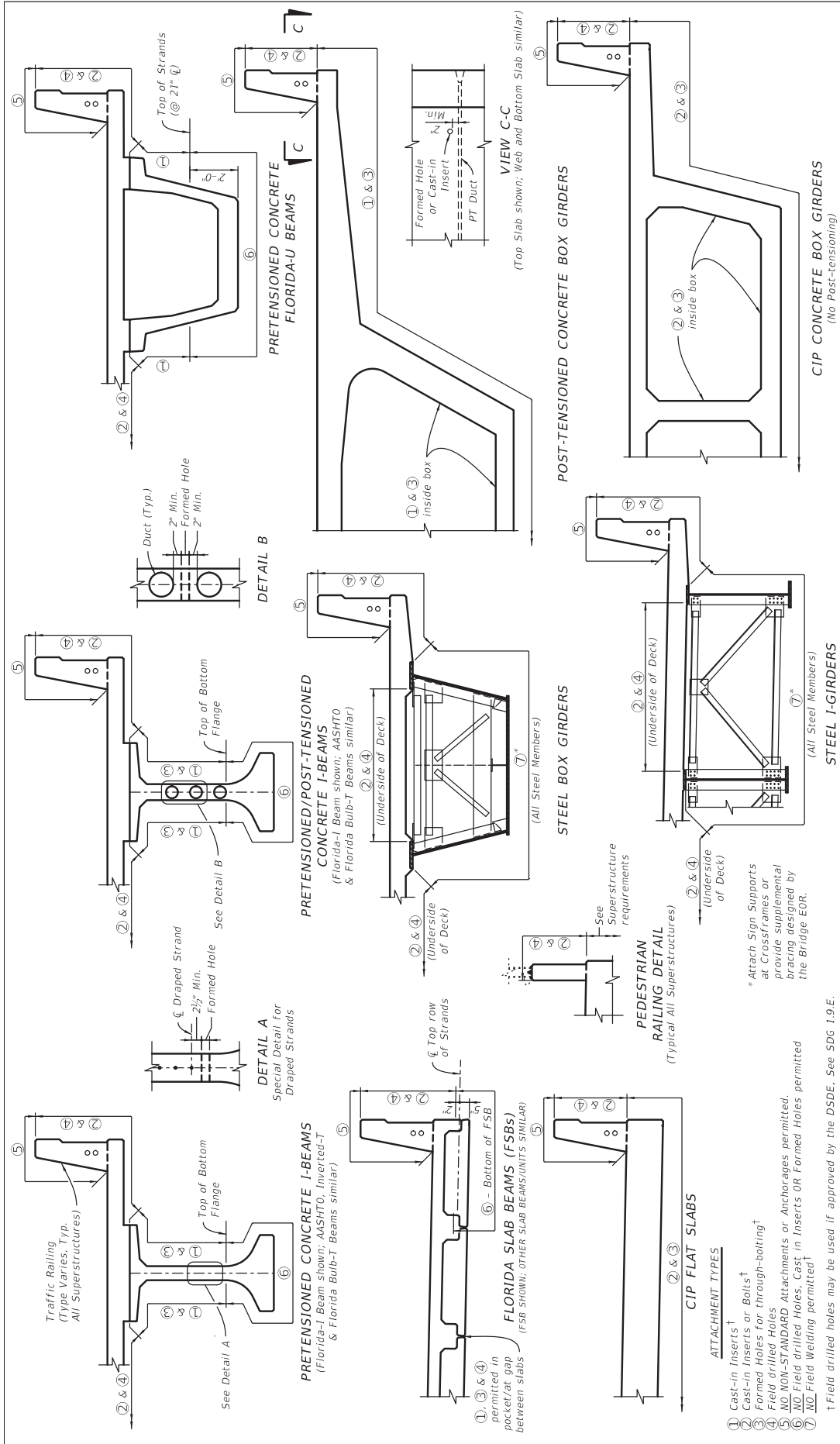
Design Standards & Cut Sheets

ALLOWABLE CONNECTION TYPES FOR MISCELLANEOUS ATTACHMENTS - SUBSTRUCTURES

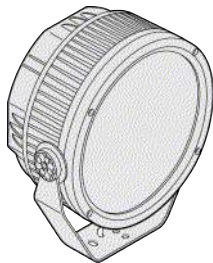


1A-1

ALLOWABLE CONNECTION TYPES FOR MISCELLANEOUS ATTACHMENTS - SUPERSTRUCTURES



1A-2



Client:

Project:

Type:

Order Code:

Quantity:



Dyna Drum HO Color is a high output, outdoor rated, quad color LED floodlight. It features an internal 100-277VAC power supply, onboard DMX+RDM driver, and each unit carries Acclaim’s Aria wireless DMX technology inside. The quad color chip provides superior color mixing and saturation over single source LED fixtures. It comes with a narrow 10° beam standard, with optional quick-change spread lenses for wider applications. It is ideal for facade lighting applications and as an area floodlight.

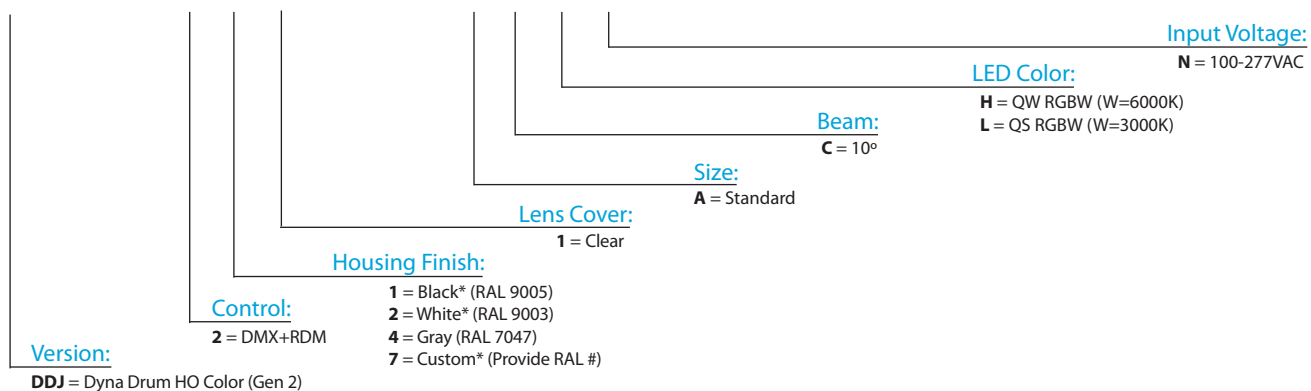
SPECIFICATIONS

Colors	QW: RGBW (W=6000K), QS: RGBW (W=3000K)
Beam Angles	10° standard, 20°, 40°, 60°, 10° x 60° spread lens options
Photometrics	7660 lumens, 161,203 cd, see page 4 for details
Effective Projected Area	1.75 ft ²
Control	DMX+RDM, Manual color setting in menu, photocell included, Aria wireless direct connect
Max Fixtures in Series	32 via DMX, power local to each fixture
Power Consumption	250W
Operating Voltage	100-277VAC, 50/60 Hz
Lumen Maintenance	L70 @ 150,000 hours (25° C)
Mounting	Surface mount bracket included, optional tenon mount and pipe clamp available
Finish	Gray standard (RAL 7047), black, white, and custom colors optional
Material	Die cast aluminum, glass top lens, optional marine coating available
Ambient Operating Temperature	-40° F to 125° F (-40° C to 51° C)
IP Rating	IP66, wet location
IK Rating	IK07, protection against 2 joule impact
Fixture Connectors	Attached 5’ (1.5m) IP66 hybrid cable, AC power +DMX/RDM
Warranty	5 Years, limited
Weight	30 lbs. (13.6 kg)
Dimensions	L: 14.8” x W: 15.4” x D: 8.2” (378mm x 393mm x 209mm)
Certifications	

ORDER CODES

* indicates special order

DDJ - 2 # 1 - A C # N



RELATED COMPONENTS

Optional Beam Accessories



DDHSL20

20° Spread lens for Dyna Drum HO Color



DDH2FSG

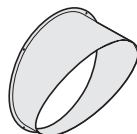
Full snoot for Dyna Drum HO Color, Gray

DDHSL40

40° Spread lens for Dyna Drum HO Color

DDHSL60

60° Spread lens for Dyna Drum HO Color



DDH2HSG

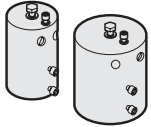
Half snoot for Dyna Drum HO Color, Gray

DDHSL1060

10° x 60° Spread lens for Dyna Drum HO Color

RELATED COMPONENTS

Optional Mounting Accessories



TM2
2" pipe, schedule 40 tenon mount
(2.51", 56mm inner dia.)

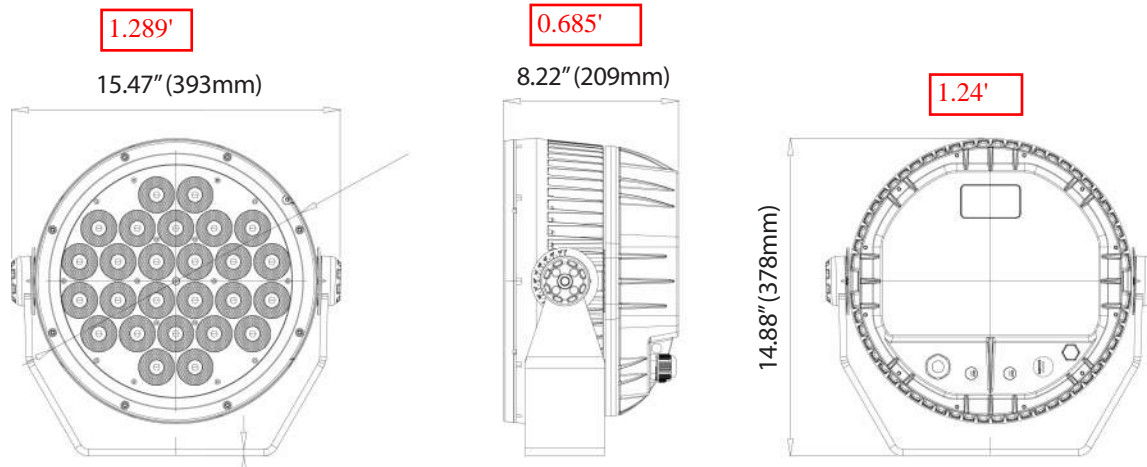
TM4
3.5" pipe, schedule 40 tenon mount
(4.13", 105mm inner dia.)



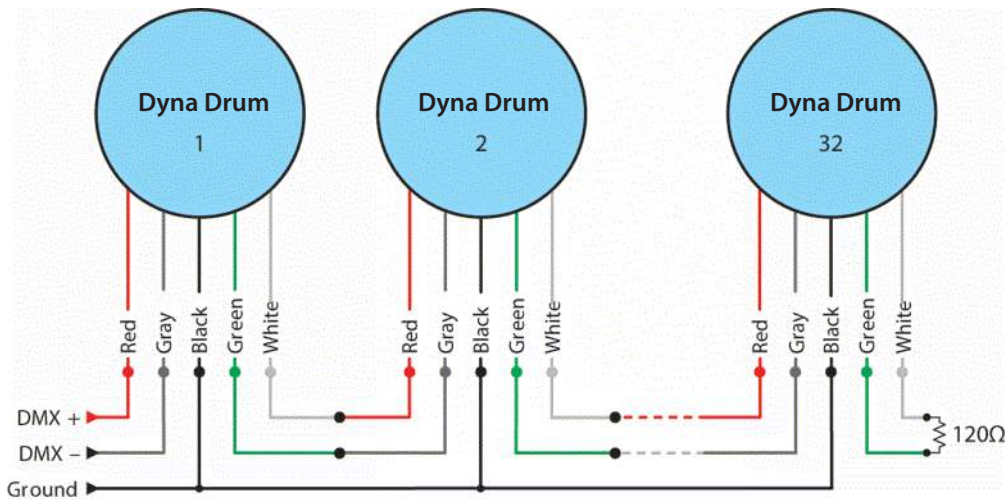
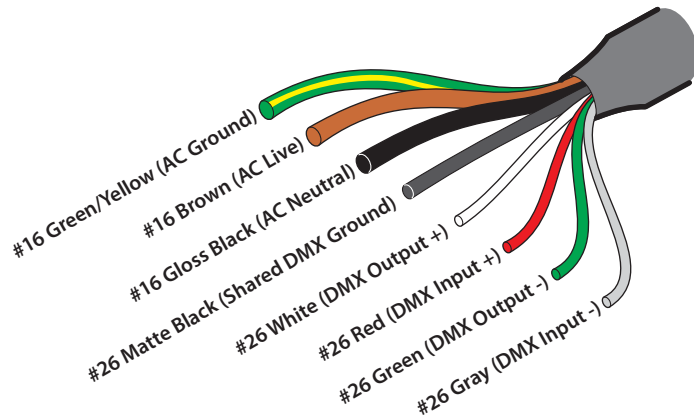
PC2
2" pipe, schedule 40 pipe clamp
mounts 1 or 2 fixtures

PC4
4" pipe, schedule 40 pipe clamp
mounts 1 or 2 fixtures

DIMENSIONS



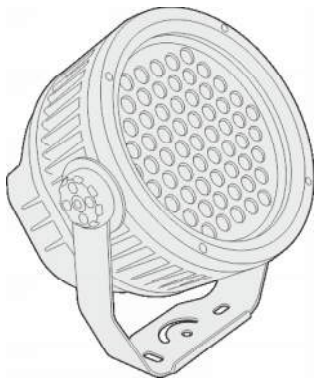
WIRING



PHOTOMETRICS

Color Temp / Beam	Lumens	Center Candela	Efficacy (l/pw)	CRI (Ra)	CRI (r9)
QW RGBW, 10°	7660	161,203	31	-	-
QS RGBW, 10°	7741	183,376	31	-	-

Dyna Drum SO™



Client:

Project:

Type:




Order Code:

Quantity:



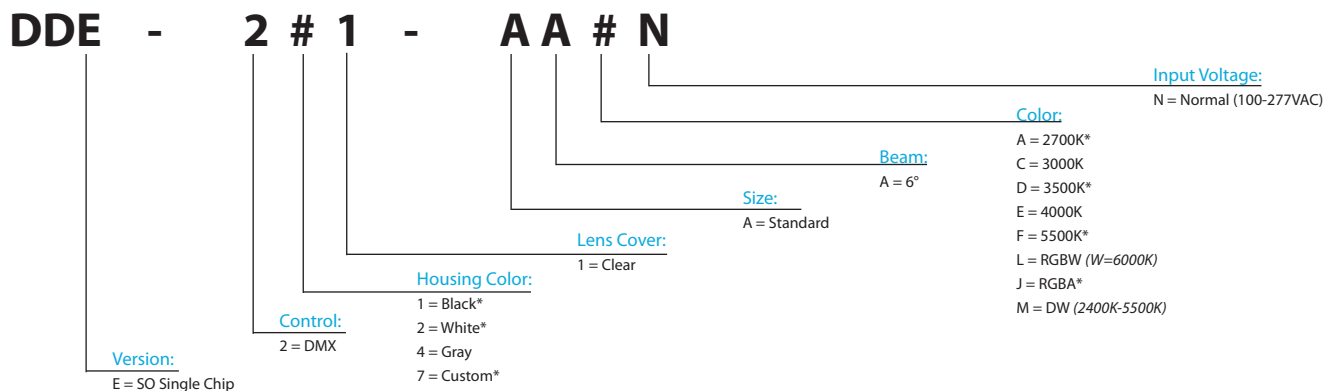
The **Dyna Drum SO** is a high output, outdoor rated, LED flood fixture. It features an adjustable yoke, on-board digital display, a 100-277VAC internal power supply, and a built in receiver for the Aria wireless DMX system. It is ideal for facade lighting applications, and as an area flood light.

Specifications

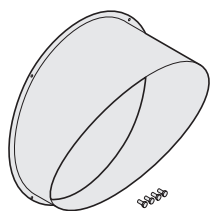
Color Temperature	RGBW, RGBA, 2700K, 3000K, 3500K, 4000K, 5500K, DW (2400K-5500K)
Beam Angle	6° (standard), 20°, 40°, 60°, 10° x 60° spread lens options
Total Lumens	7,769 at 5500K, 6° / 4656 at RGBW, 6°
Center Beam Candela	344,366 at 5500K, 6° / 148,001 at RGBW, 6°
Control	DMX-512, 4 channels (color), 3 Channels (DW), or 1 Channel (white)
Max Fixtures in Series	32, via DMX-512
Effective Projected Area	Front: 0.72, Side 0.74 (includes drag coefficient)
Power Consumption	157W at steady state
Operating Voltage	100-277VAC, 50/60Hz
Lumen Maintenance	L70 @ 120,000 Hours (25° C)
Finish	Gray (Standard), White or Black (Optional)
Housing Material	Die Cast Aluminum, Optional Marine Environment Coating Available
Operating Temperature	-40° F to 122° F (-40° C to 50° C)
IP Rating	IP66, Wet Location
Fixture Connectors	Attached 5' (1.5m) IP 66 AC Power + Signal Cable
Warranty	5 Year Limited Warranty
Weight	26.4 lbs (12 kg)
Dimensions	9.13" ø x W 8.39" x H 14.13" (232mm ø x W 213mm x H 359mm)
Certifications	  

Order Codes

* Indicates Special Order



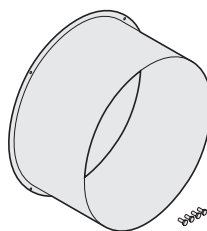
Related Components



Half Snoot

Gray: DDSOHSG
Black: DDSOHSB
White: DDSOHSW

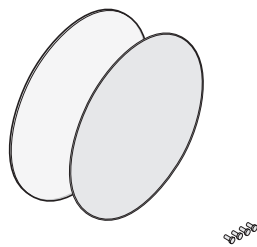
Includes four M4 mounting screws



Full Snoot

Gray: DDSOFSG
Black: DDSOFSB
White: DDSOFSW

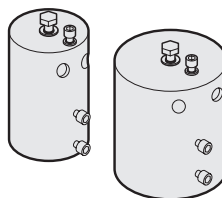
Includes four M4 mounting screws



Spread Lens Kits

20° Beam: DDSSL20
40° Beam: DDSSL40
60° Beam: DDSSL60
10° x 60° Beam: DDSSL1060

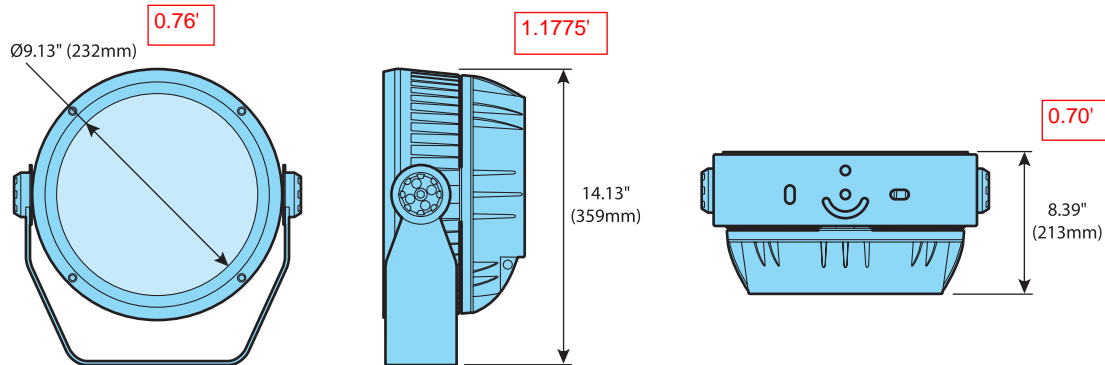
Includes four M4 mounting screws



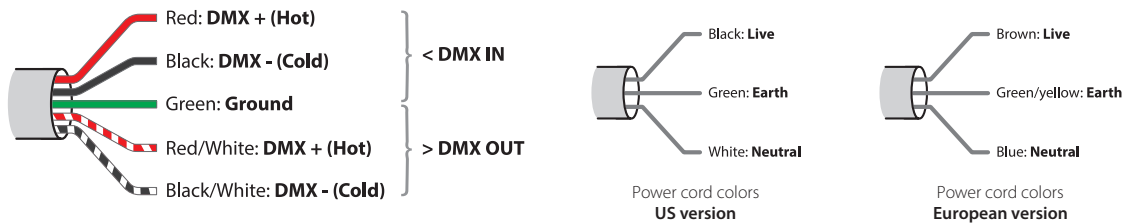
Tenon Mount

For 2" pipe: TM2
For 4" pipe: TM4

Dimensions



Wiring



Photometrics

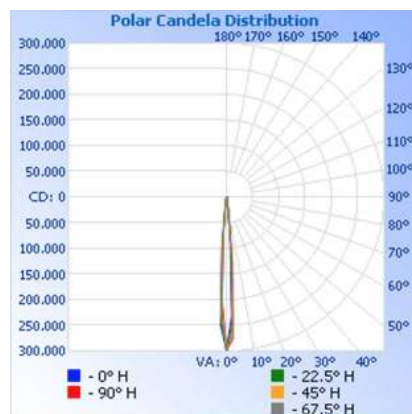
For IES & Revit files, please visit acclaimlighting.com

5500K, 6°

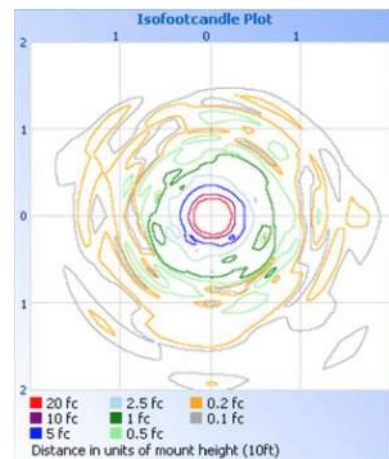
Zonal Lumen Summary

Zone	Lumens	%
0-60	7634	98.3
60-90	131.8	1.7
90-180	2.8	0.0
Total	7769	100

Polar Candela Distribution



Isofootcandle Plot



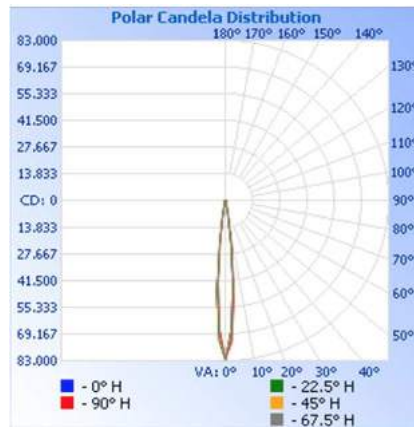
Photometrics (Con't)

RGBW, 6°

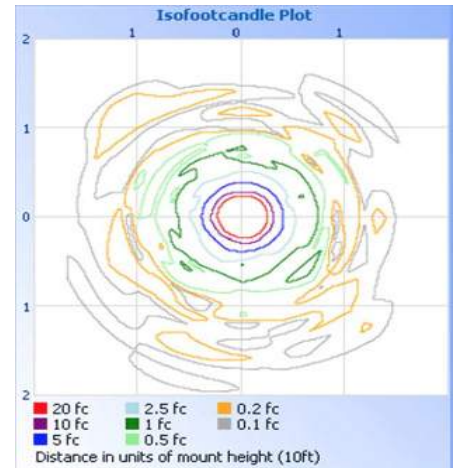
Zonal Lumen Summary

Zone	Lumens	%
0-60	4556	97.9
60-90	96.3	2.1
90-180	3.7	0.1
Total	4656	100

Polar Candela Distribution



Isofootcandle Plot





Wind Calculation

The following wind calculations are based on:

1. LRFD Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals (1st Edition 2015)
2. 2017 Interim Revisions to the LRFD Specifications for Structural Supports for Highway Signs, Luminaires, and Traffic Signals (1st Edition 2015)
3. FDOT Structures Design Guidelines (January 2018)

$G = 1.14$	(LRFD Spec. 2017 Revisions, 3.8.6)
$C_d = 0.5$	(LRFD Spec. 2017 Revisions, Table 3.8.7)
-From elevations worst case (70')	
$K_z = 1.17$	(LRFD Spec. 2015, Table C3.8.4-1)
$K_d = 0.85$	(LRFD Spec. 2015, Table C3.8.5-1)
$V = 150 \text{ mph}$	(FDOT SDG, Table 2.4.1-1, Hillsborough County)
$P_z = 0.00256 * V^2 * K_z * K_d * G * C_d$	(LRFD Spec. 2015, 3.8.1-1)
$P_z = 0.00256 * (150 \text{ mph})^2 * (1.17) * (0.85) * (1.14) * (0.5)$	
$P_z = 32.65 \text{ psf}$	

Luminaires (Dyna Drum HO QW Color):

$F_z = 32.65 * (1.289 * 1.24')$	$M_z = (52.2 \text{ lb} * 1.24' / 2)$
$F_z = 52.2 \text{ lbs}$	$M_z = 32.4 \text{ lb} * \text{ft}$
$F_x = 32.65 * (0.685 * 1.24')$	$M_x = (27.7 \text{ lb} * 1.24' / 2)$
$F_x = 27.7 \text{ lbs}$	$M_x = 17.0 \text{ lb} * \text{ft}$

Luminaires (Dyna Drum SO):

$F_z = 32.65 * (0.76 * 1.18')$	$M_z = (29.3 \text{ lb} * 1.18' / 2)$
$F_z = 29.3 \text{ lbs}$	$M_z = 17.3 \text{ lb} * \text{ft}$
$F_x = 32.65 * (0.70 * 1.18')$	$M_x = (27 \text{ lb} * 1.18' / 2)$
$F_x = 27 \text{ lbs}$	$M_x = 15.9 \text{ lb} * \text{ft}$

Wind Pressure on HSS:

$$P_z = 0.00256 * V^2 * K_z * K_d * G * C_d$$

$$C_d = 2 - 6 * r_s$$

$$r_s = \text{Cover Radius} / d$$

$$r_s = 2 * t / 3''$$

$$r_s = 2 * (3'' / 16) / 3'' = 0.125$$

$$C_d = 1.25$$

$$P_z = 0.00256 * (150 \text{ mph})^2 * (1.17) * (0.85) * (1.14) * (1.25)$$

$$P_z = 81.62 \text{ psf}$$

2.4 WIND LOADS

2.4.1 Wind Loads on Completed Structures: WL and WS [3.8]

(Rev. 01/18)

A. Design Wind Speed

Use the design 3-second gust wind speed, V , from Table 2.4.1-1 in lieu of *LRFD* [Figure 3.8.1.1.2-1].

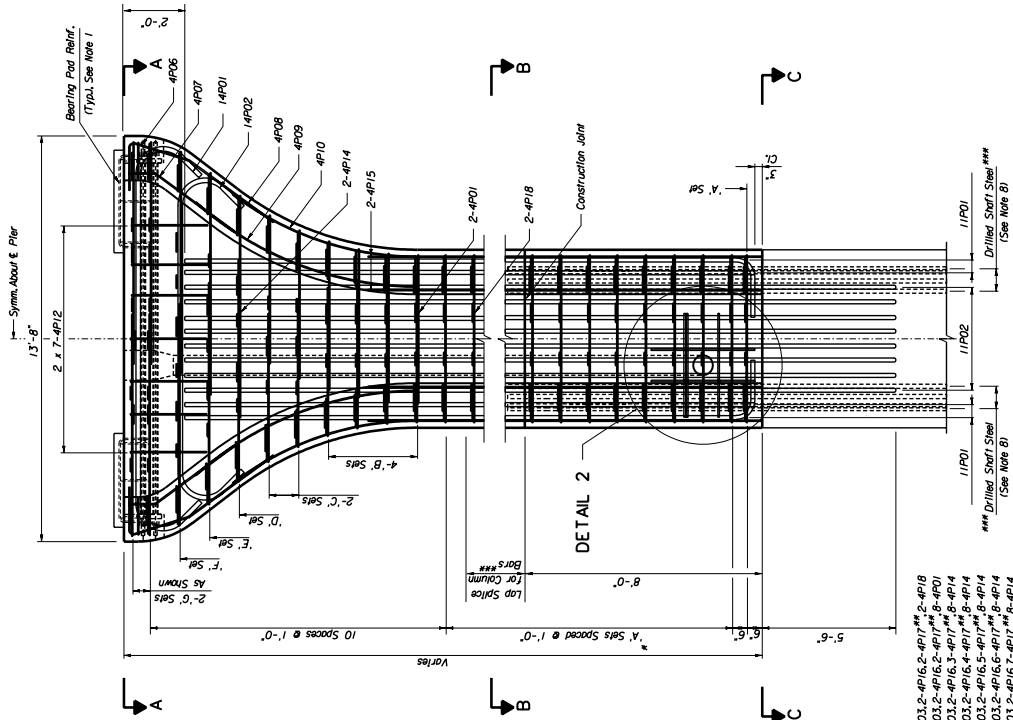
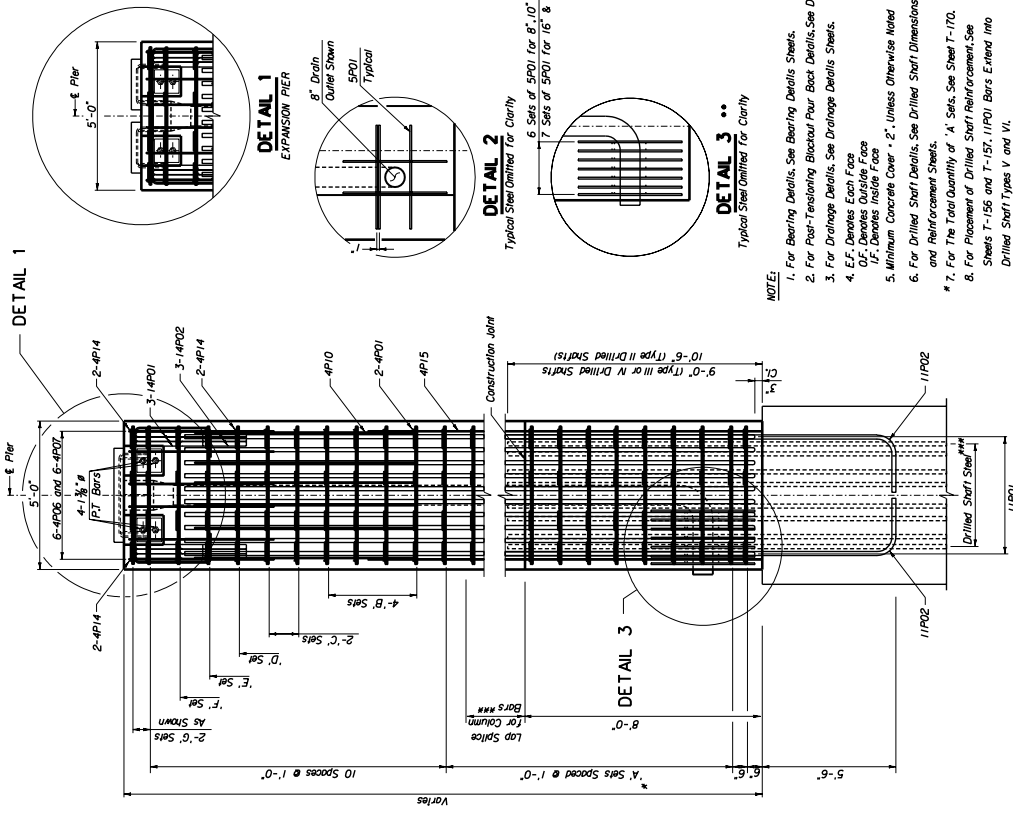
Table 2.4.1-1 Design Wind Speed, V

County (Dist)	Design Wind Speed (mph)	County (Dist)	Design Wind Speed (mph)	County (Dist)	Design Wind Speed (mph)
Alachua (2)	130	Hardee (1)	150	Nassau (2)	130
Baker (2)	130	Hendry (1)	150	Okaloosa (3)	150
Bay (3)	150	Hernando (7)	150	Okeechobee (1)	150
Bradford (2)	130	Highlands (1)	150	Orange (5)	150
Brevard (5)	170	Hillsborough (7)	150	Osceola (5)	150
Broward (4)	170	Holmes (3)	150	Palm Beach (4)	170
Calhoun (3)	130	Indian River (4)	170	Pasco (7)	150
Charlotte (1)	170	Jackson (3)	130	Pinellas (7)	150
Citrus (7)	150	Jefferson (3)	130	Polk (1)	150
Clay (2)	130	Lafayette (2)	130	Putnam (2)	130
Collier (1)	170	Lake (5)	150	St. Johns (2)	150
Columbia (2)	130	Lee (1)	170	St. Lucie (4)	170
DeSoto (1)	150	Leon (3)	130	Santa Rosa (3)	150
Dixie (2)	130	Levy (2)	150	Sarasota (1)	170
Duval (2)	130	Liberty (3)	130	Seminole (5)	150
Escambia (3)	170	Madison (2)	130	Sumter (5)	150
Flagler (5)	150	Manatee (1)	150	Suwannee (2)	130
Franklin (3)	150	Marion (5)	150	Taylor (2)	130
Gadsden (3)	130	Martin (4)	170	Union (2)	130
Gilchrist (2)	130	Miami-Dade (6)	170	Volusia (5)	150
Glades (1)	150	Miami-Dade Islands (6)	180	Wakulla (3)	130
Gulf (3)	150	Monroe (6)	170	Walton (3)	150
Hamilton (2)	130	Monroe Islands (6)	180	Washington (3)	150

Pier



Existing Structural Plans



HALF-ELEVATION TYPICAL PIER
HALF-ELEVATION EXPANSION PIER

(Interior Pier Shown)
 *** 11S01, 11S02 & 11S03 Bars Terminating at Top of Drilled Shaft Not Shown

- Pier Types I, II, III and IV
- 'A' Sets Contain 2-4P02, 2-4P03, 2-4P16, 2-4P17, 2-4P18
- 'B' Sets Contain 2-4P02, 2-4P03, 2-4P16, 2-4P17, 2-4P18, 3-4P01
- 'C' Sets Contain 2-4P02, 2-4P03, 2-4P16, 3-4P01, 3-4P02, 3-4P03, 3-4P04
- 'D' Sets Contain 2-4P02, 2-4P03, 2-4P16, 4-4P09, 4-4P10, 4-4P11, 4-4P12
- 'E' Sets Contain 2-4P02, 2-4P03, 2-4P16, 5-4P13, 5-4P14, 5-4P15, 5-4P16, 5-4P17, 5-4P18
- 'F' Sets Contain 2-4P02, 2-4P03, 2-4P16, 6-4P19, 6-4P20, 6-4P21, 6-4P22, 6-4P23, 6-4P24
- 'G' Sets Contain 2-4P02, 2-4P03, 2-4P16, 7-4P25, 7-4P26, 7-4P27, 7-4P28, 7-4P29, 7-4P30

Each set 'A' through 'G' contains an additional 2-4P17 for Pier Types II and III and an additional 4-4P17 for Pier Type IV.

DETAIL 2
 Typical Steel Reinforced For Clarity
 6 Sets of 5P01 For 8", 10" & 12" Pipes
 7 Sets of 5P01 For 16" & 18" Pipes

DETAIL 3
 Typical Steel Reinforced For Clarity

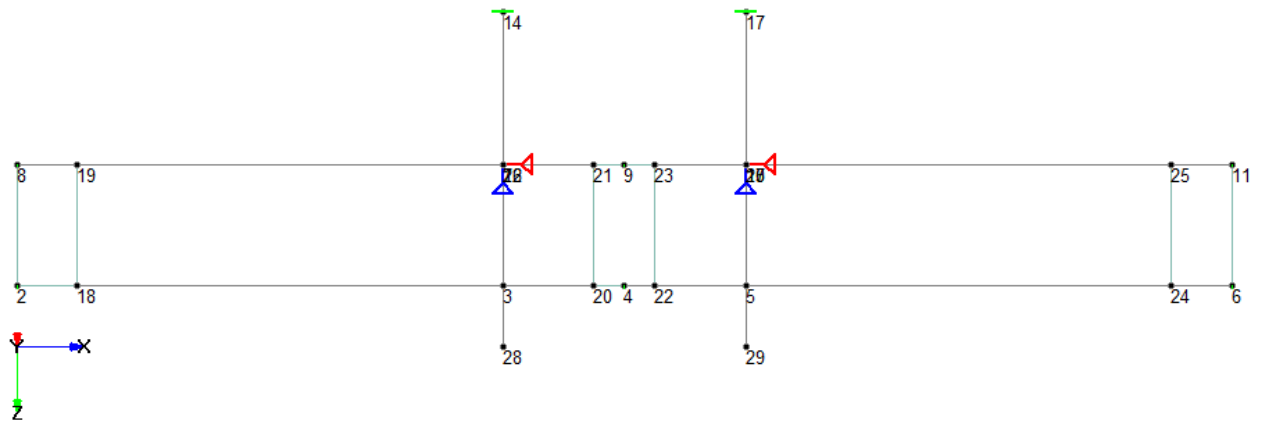
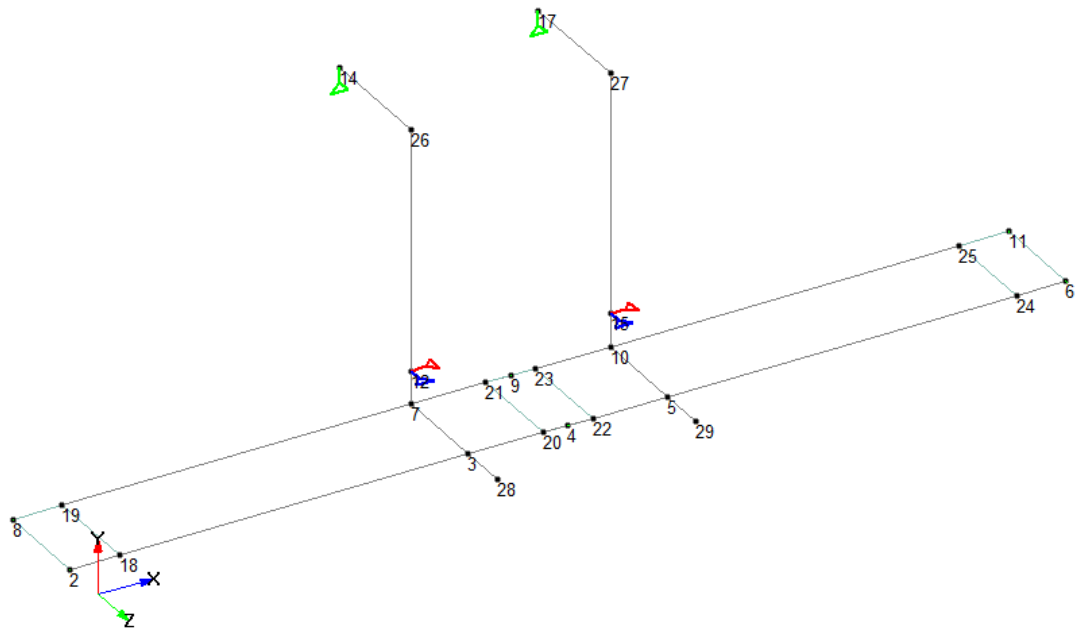
- NOTE:
- For Bearing Details. See Bearing Details Sheets.
 - For Post-Tensioning Blockout Four Back Details. See Drawing XXX
 - For Drainage Details. See Drainage Details Sheets.
 - E.F. Denotes Each Face
 - O.F. Denotes Outside Face
 - I.F. Denotes Inside Face
 - Minimum Concrete Cover - 2". Unless Otherwise Noted
 - For Drilled Shaft Details. See Drilled Shaft Dimensions and Reinforcement Sheets.
 - For Placement of Drilled Shaft Reinforcement. See Sheets T-156 and T-157. 11P01 Bars Extend into Drilled Shaft Types V and VI.
 - Contractor may Field Cut No More than 2-11P02 Bars for 8" and 10" Pipes and No More than 3-11P02 Bars for 12" and 16" Pipes.
 - Lap Splices at 8 Construction Joint Shall be a Minimum of 7'-2"

DATE	BY	DESCRIPTION	DATE	BY	DESCRIPTION

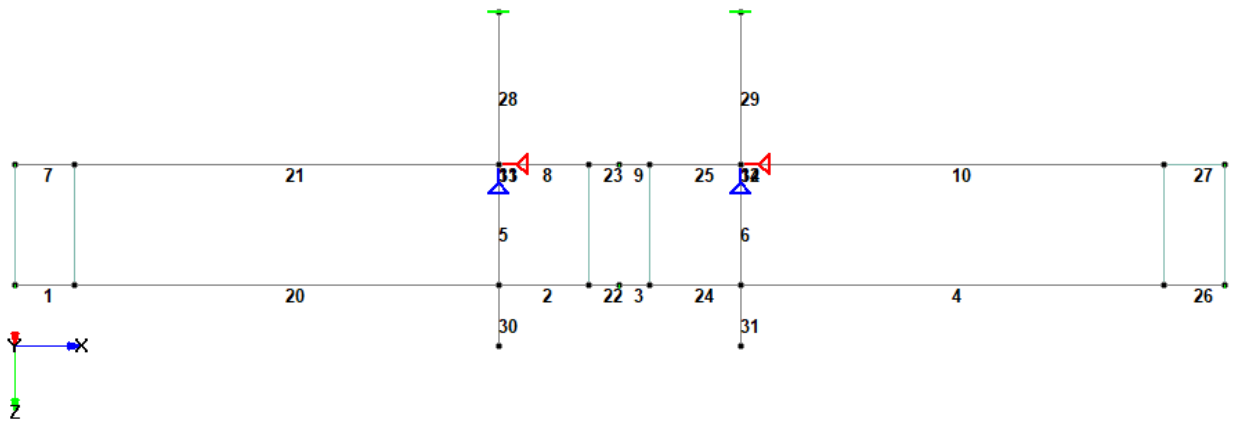
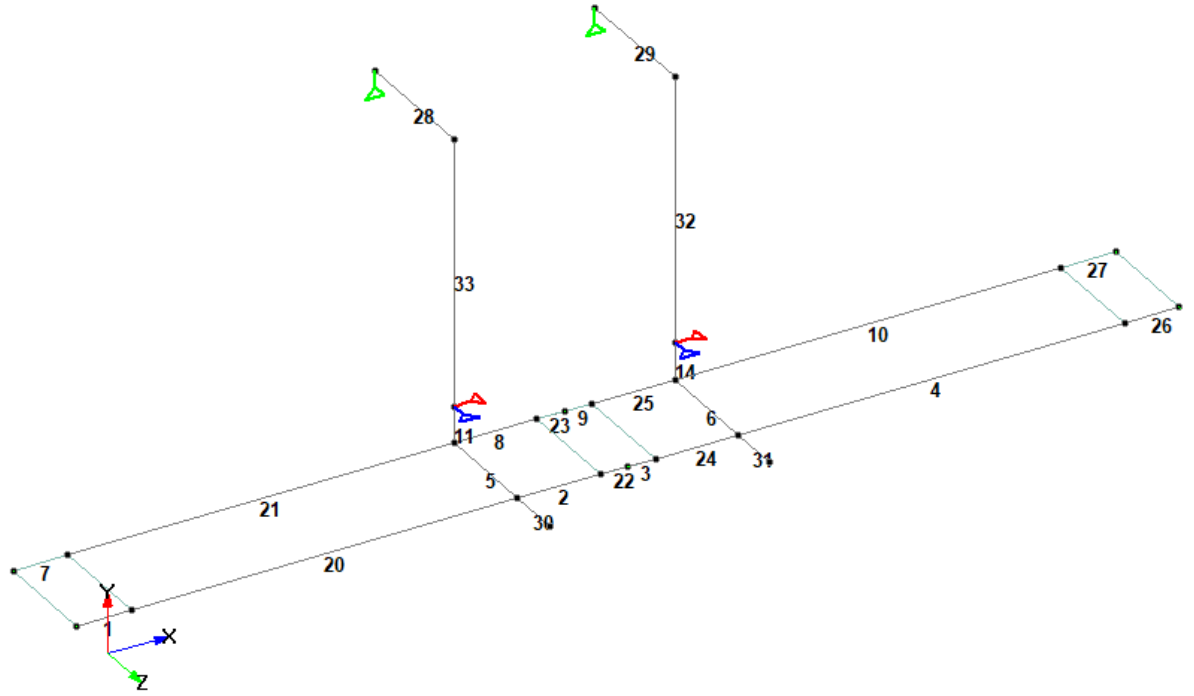
ENGINEER OF RECORD: J.M.F. 12-13-02 W.P.P. 12-13-02 J.M.F. 12-13-02 J. Rodriguez	COUNTY: HILLSBOROUGH PROJECT NO.: THCEA 5140.01	SHEET NO.: 100806 & 100812 DRAWING NO.: 1-169 PROJECT NAME: SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE
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STAAD Analysis

Stadd Model
Nodes



Stadd Model
Members





Software licensed to Kimley-Horn (Cary), N CAROLINA
CONNECTED User: Ivonne Rios

Job No 148872000	Sheet No 1	Rev 4
Part		
Ref		
By IERM	Date 2/12/2020	Chd
Client THEA	File THEA-Pier Model_CaseL	Date/Time 12-Feb-2020 16:39

Job Title Pier Analysis
Client THEA

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	2/12/2020		

Project ID	
Project Name	

Structure Type	SPACE FRAME
----------------	-------------

Number of Nodes	26	Highest Node	29
Number of Elements	26	Highest Beam	33
Number of Plates	3	Highest Plate	19

Number of Basic Load Cases	7
Number of Combination Load Cases	9

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	2	DYNO DRUM HO: LIGHT WIND LOAD (Z)
Primary	1	WEIGHT
Primary	10	WIND LOAD ON STRUCTURE (X) DIREC
Primary	11	WIND LOAD ON STRUCTURE (Y) DIREC
Primary	12	DYNO DRUM HO: LIGHT WIND LOAD (X)
Primary	16	WIND RESULTANT
Primary	9	COMPRESSION FORCE
Combination	3	1.1DL+1.0WR
Combination	4	1.25DL
Combination	5	1.1DL+1.0WX
Combination	6	CASE I: VX
Combination	7	1.1DL+1.0WZ
Combination	8	CASE I: VY
Combination	13	CASE III: VY
Combination	14	CASE III: VZ
Combination	15	CASE III: VX



Software licensed to Kimley-Horn (Cary), N CAROLINA
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
2

Rev
4

Job Title **Pier Analysis**

Part

Ref

By **IERM** Date **2/12/2020** Chd

Client **THEA**

File **THEA-Pier Model_CaseL** Date/Time **12-Feb-2020 16:39**

Nodes

Node	X (ft)	Y (ft)	Z (ft)
2	0	0	-1.000
3	8.000	0	-1.000
4	10.000	0	-1.000
5	12.000	0	-1.000
6	20.000	0	-1.000
7	8.000	0	-3.000
8	0	0	-3.000
9	10.000	0	-3.000
10	12.000	0	-3.000
11	20.000	0	-3.000
12	8.000	0.670	-3.000
14	8.000	5.500	-5.500
15	12.000	0.670	-3.000
17	12.000	5.500	-5.500
18	1.000	0	-1.000
19	1.000	0	-3.000
20	9.500	0	-1.000
21	9.500	0	-3.000
22	10.500	0	-1.000
23	10.500	0	-3.000
24	19.000	0	-1.000
25	19.000	0	-3.000
26	8.000	5.500	-3.000
27	12.000	5.500	-3.000
28	8.000	0	0
29	12.000	0	0

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	2	18	1.000	2	0
2	3	20	1.500	2	0
3	4	22	0.500	2	0
4	5	24	7.000	2	0
5	3	7	2.000	3	0
6	5	10	2.000	3	0
7	8	19	1.000	2	0
8	7	21	1.500	2	0
9	9	23	0.500	2	0
10	10	25	7.000	2	0
11	7	12	0.670	3	0
14	10	15	0.670	3	0
20	18	3	7.000	2	0



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Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
21	19	7	7.000	2	0
22	20	4	0.500	2	0
23	21	9	0.500	2	0
24	22	5	1.500	2	0
25	23	10	1.500	2	0
26	24	6	1.000	2	0
27	25	11	1.000	2	0
28	26	14	2.500	3	0
29	27	17	2.500	3	0
30	3	28	1.000	3	0
31	5	29	1.000	3	0
32	15	27	4.830	3	0
33	12	26	4.830	3	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
17	18	19	8	2	1
18	22	23	21	20	1
19	6	11	25	24	1

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
2	HSST3X3X0.188	1.890	2.460	2.460	3.927	STEEL
3	HSST3.5X3.5X0.25	2.910	5.040	5.040	8.125	STEEL

Plate Thickness

Prop	Node A (in)	Node B (in)	Node C (in)	Node D (in)	Material
1	0.250	0.250	0.250	0.250	STEEL_36_KS



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Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E -6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E -6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E -6
5	A500-GR.B	29E+3	0.300	0.000	6E -6
6	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
7	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
8	STEEL	29E+3	0.300	0.000283	6E -6
9	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6

Releases

There is no data of this type.

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip ft/deg)	rY (kip ft/deg)	rZ (kip ft/deg)
12	Fixed	-	Fixed	-	-	-
14	-	Fixed	-	-	-	-
15	Fixed	-	Fixed	-	-	-
17	-	Fixed	-	-	-	-

Primary Load Cases

Number	Name	Type
2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	Wind
1	WEIGHT	Dead
10	WIND LOAD ON STRUCTURE (X) DIREC	Wind
11	WIND LOAD ON STRUCTURE (Y) DIREC	Wind
12	DYNO DRUM HO: LIGHT WIND LOAD (X)	Wind
16	WIND RESULTANT	Wind
9	COMPRESSION FORCE	Dead



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Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
3	1.1DL+1.0WR	1	WEIGHT	1.10
		16	WIND RESULTANT	1.00
4	1.25DL	1	WEIGHT	1.25
5	1.1DL+1.0WX	1	WEIGHT	1.10
		12	DYNO DRUM HO: LIGHT WIND LOAD (X)	1.00
		10	WIND LOAD ON STRUCTURE (X) DIREC	1.00
6	CASE I: VX	10	WIND LOAD ON STRUCTURE (X) DIREC	1.00
7	1.1DL+1.0WZ	2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	1.00
		3	1.1DL+1.0WR	1.00
		1	WEIGHT	1.10
8	CASE I: VY	1	WEIGHT	1.00
13	CASE III: VY	1	WEIGHT	0.75
14	CASE III: VZ	3	1.1DL+1.0WR	0.75
		2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	0.75
		12	DYNO DRUM HO: LIGHT WIND LOAD (X)	0.75
15	CASE III: VX	12	DYNO DRUM HO: LIGHT WIND LOAD (X)	0.75

1 WEIGHT : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	-	-0.0261	-	-	-	-
4	-	-0.0261	-	-	-	-
6	-	-0.0261	-	-	-	-
8	-	-0.0261	-	-	-	-
9	-	-0.0261	-	-	-	-
11	-	-0.0261	-	-	-	-

1 WEIGHT : Selfweight

Direction	Factor	Assigned Geometry
Y	-1.000	ALL

2 DYNO DRUM HO: LIGHT WIND LOAD (Z) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	-	-	-0.0522	-	-	-
4	-	-	-0.0522	-	-	-
6	-	-	-0.0522	-	-	-
8	-	-	-0.0522	-	-	-
9	-	-	-0.0522	-	-	-
11	-	-	-0.0522	-	-	-



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9 COMPRESSION FORCE : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
14	-	-	3.000	-	-	-
17	-	-	3.000	-	-	-
26	-	-	-3.000	-	-	-
27	-	-	-3.000	-	-	-

10 WIND LOAD ON STRUCTURE (X) DIRECTION : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
5	UNI lbf/ft	GX	20.000	0	-	2.000	-
6	UNI lbf/ft	GX	20.000	0	-	2.000	-
11	UNI lbf/ft	GX	20.000	0	-	0.670	-
14	UNI lbf/ft	GX	20.000	0	-	0.670	-
30	UNI lbf/ft	GX	20.000	0	-	1.000	-
31	UNI lbf/ft	GX	20.000	0	-	1.000	-
32	UNI lbf/ft	GX	20.000	0	-	4.830	-
33	UNI lbf/ft	GX	20.000	0	-	4.830	-

11 WIND LOAD ON STRUCTURE (Y) DIRECTION : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI lbf/ft	GY	20.000	0	-	1.000	-
2	UNI lbf/ft	GY	20.000	0	-	1.500	-
3	UNI lbf/ft	GY	20.000	0	-	0.500	-
4	UNI lbf/ft	GY	20.000	0	-	7.000	-
5	UNI lbf/ft	GY	20.000	0	-	2.000	-
6	UNI lbf/ft	GY	20.000	0	-	2.000	-
7	UNI lbf/ft	GY	20.000	0	-	1.000	-
8	UNI lbf/ft	GY	20.000	0	-	1.500	-
9	UNI lbf/ft	GY	20.000	0	-	0.500	-
10	UNI lbf/ft	GY	20.000	0	-	7.000	-
20	UNI lbf/ft	GY	20.000	0	-	7.000	-
21	UNI lbf/ft	GY	20.000	0	-	7.000	-
22	UNI lbf/ft	GY	20.000	0	-	0.500	-
23	UNI lbf/ft	GY	20.000	0	-	0.500	-
24	UNI lbf/ft	GY	20.000	0	-	1.500	-
25	UNI lbf/ft	GY	20.000	0	-	1.500	-
26	UNI lbf/ft	GY	20.000	0	-	1.000	-
27	UNI lbf/ft	GY	20.000	0	-	1.000	-
30	UNI lbf/ft	GY	20.000	0	-	1.000	-
31	UNI lbf/ft	GY	20.000	0	-	1.000	-



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12 DYNO DRUM HO: LIGHT WIND LOAD (X) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	0.02777	-	-	-	-	-
4	0.02777	-	-	-	-	-
8	0.02777	-	-	-	-	-
9	0.02777	-	-	-	-	-
24	0.02777	-	-	-	-	-
25	0.02777	-	-	-	-	-

16 WIND RESULTANT : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	0.0295	-	-	-	-	-
3	0.042	-	-	-	-	-
5	0.042	-	-	-	-	-
8	0.0295	-	-	-	-	-
12	0.155	-	-	-	-	-
15	0.155	-	-	-	-	-
20	0.0295	-	-	-	-	-
21	0.0295	-	-	-	-	-
24	0.0295	-	-	-	-	-
25	0.0295	-	-	-	-	-
26	0.053	-	-	-	-	-
27	0.053	-	-	-	-	-
28	0.021	-	-	-	-	-
29	0.021	-	-	-	-	-

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6	-21.8E+3	0.002	-0.020
Min X	26	7:1.1DL+1.0W	-1.702	-1.06E+6	2.05E+6	2.31E+6	35.4E+3	-0.002	0.029
Max Y	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6	-21.8E+3	0.002	-0.022
Min Y	28	7:1.1DL+1.0W	0.157	-2.34E+6	-285E+3	2.36E+6	35.4E+3	-0.002	0.034
Max Z	14	7:1.1DL+1.0W	-1.632	0	2.05E+6	2.05E+6	35.4E+3	-0.002	0.029
Min Z	14	11:WIND LOA	1.085	0	-1.26E+6	1.26E+6	-21.8E+3	0.002	-0.020
Max rX	14	7:1.1DL+1.0W	-1.632	0	2.05E+6	2.05E+6	35.4E+3	-0.002	0.029
Min rX	14	11:WIND LOA	1.085	0	-1.26E+6	1.26E+6	-21.8E+3	0.002	-0.020
Max rY	3	11:WIND LOA	-0.120	1.18E+6	175E+3	1.19E+6	-21.8E+3	0.002	-0.022
Min rY	18	7:1.1DL+1.0W	0.184	-1.91E+6	-285E+3	1.93E+6	35.4E+3	-0.002	0.039
Max rZ	8	7:1.1DL+1.0W	0.239	-1.06E+6	-285E+3	1.1E+6	35.4E+3	-0.002	0.040
Min rZ	8	11:WIND LOA	-0.157	653E+3	175E+3	676E+3	-21.8E+3	0.002	-0.025
Max Rst	28	7:1.1DL+1.0W	0.157	-2.34E+6	-285E+3	2.36E+6	35.4E+3	-0.002	0.034



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Beam End Displacement Summary

Displacements shown in italic indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	28	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6
Min X	28	26	7:1.1DL+1.0W	-1.702	-1.06E+6	2.05E+6	2.31E+6
Max Y	30	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6
Min Y	30	28	7:1.1DL+1.0W	0.157	-2.34E+6	-285E+3	2.36E+6
Max Z	28	26	7:1.1DL+1.0W	-1.702	-1.06E+6	2.05E+6	2.31E+6
Min Z	28	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6
Max Rst	30	28	7:1.1DL+1.0W	0.157	-2.34E+6	-285E+3	2.36E+6

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	28	26	9:COMPRESSI	3.000	0.000	0.000	-0.000	-0.000	0.000
Min Fx	8	7	11:WIND LOA	-1.284	-0.340	-0.014	-7.549	0.126	-8.507
Max Fy	11	7	7:1.1DL+1.0W	-0.533	2.034	0.049	-0.000	22.152	18.528
Min Fy	14	10	7:1.1DL+1.0W	-0.642	-2.249	-0.148	0.000	-37.026	-15.906
Max Fz	11	7	16:WIND RESI	0.055	-0.104	0.206	-0.000	-1.123	1.339
Min Fz	27	25	2:DYNO DRUM	0.084	-0.001	-0.179	0.006	1.395	-0.005
Max Mx	8	7	7:1.1DL+1.0W	2.303	0.472	-0.009	11.258	-0.072	12.081
Min Mx	5	3	7:1.1DL+1.0W	-0.072	0.215	0.109	-14.139	-1.336	-6.696
Max My	14	15	11:WIND LOA	0.460	1.290	0.000	-0.000	25.560	-0.000
Min My	32	27	7:1.1DL+1.0W	-0.761	0.037	-0.037	0.000	-40.391	0.000
Max Mz	29	17	7:1.1DL+1.0W	-0.000	-0.816	-0.000	-0.000	0.000	64.046
Min Mz	29	17	11:WIND LOA	-0	0.460	0.000	-0.000	-0.000	-39.360

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	28	9:COMPRESSI	0	3.000	0.000	0.000	-0.000	-0.000	0.000
Min Fx	8	11:WIND LOA	0	-1.284	-0.340	-0.014	-7.549	0.126	-8.507
Max Fy	11	7:1.1DL+1.0W	0	-0.533	2.034	0.049	-0.000	22.152	18.528
Min Fy	14	7:1.1DL+1.0W	0	-0.642	-2.249	-0.148	0.000	-37.026	-15.906
Max Fz	11	16:WIND RESI	0	0.055	-0.104	0.206	-0.000	-1.123	1.339
Min Fz	27	2:DYNO DRUM	0	0.084	-0.001	-0.179	0.006	1.395	-0.005
Max Mx	8	7:1.1DL+1.0W	0	2.303	0.472	-0.009	11.258	-0.072	12.081
Min Mx	5	7:1.1DL+1.0W	0	-0.072	0.215	0.109	-14.139	-1.336	-6.696
Max My	14	11:WIND LOA	0.670	0.460	1.290	0.000	-0.000	25.560	-0.000



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Beam Force Detail Summary Cont...

	Beam	L/C	d (ft)	Axial Fx (kip)	Shear Fy (kip)	Fz (kip)	Torsion Mx (kip-in)	Bending My (kip-in)	Mz (kip-in)
Min My	32	7:1.1DL+1.0Wz	4.830	-0.761	0.037	-0.037	0.000	-40.391	0.000
Max Mz	29	7:1.1DL+1.0Wz	2.500	-0.000	-0.816	-0.000	-0.000	0.000	64.046
Min Mz	29	11:WIND LOA	2.500	-0	0.460	0.000	-0.000	-0.000	-39.360

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	2:DYNO DRUM	1.000	808.023	1.000	2	-896.777	1.000	1
	1:WEIGHT	1.000	213.567	1.000	3	-214.042	1.000	1
	10:WIND LOA	1.000	4.584	1.000	3	-4.826	1.000	1
	11:WIND LOA	1.000	35.503	0	1	-34.876	0	3
	12:DYNO DRU	1.000	20.377	1.000	2			
	16:WIND RESI	1.000	360.562	1.000	1	-304.328	1.000	2
	9:COMPRESSI	1.000	0.000	1.000	3	-0.000	1.000	1
	3:1.1DL+1.0Wf	1.000	595.486	1.000	4	-539.774	1.000	2
	4:1.25DL	1.000	266.959	1.000	3	-267.552	1.000	1
	5:1.1DL+1.0Wz	1.000	257.192	1.000	3	-231.068	1.000	1
	6:CASE I: VX	1.000	4.584	1.000	3	-4.826	1.000	1
	7:1.1DL+1.0Wz	1.000	966.864	1.000	3	-1E+3	1.000	1
	8:CASE I: VY	1.000	213.567	1.000	3	-214.042	1.000	1
	13:CASE III: V	1.000	160.175	1.000	3	-160.531	1.000	1
	14:CASE III: Vz	1.000	550.598	1.000	3	-575.379	1.000	1
	15:CASE III: VX	1.000	15.283	1.000	2			
2	2:DYNO DRUM	1.500	372.927	0	1	-770.020	0	2
	1:WEIGHT	1.500	1.25E+3	0	1	-1.24E+3	0	3
	10:WIND LOA	1.500	639.564	0	3	-611.547	0	1
	11:WIND LOA	1.500	2.15E+3	0	3	-2.16E+3	0	1
	12:DYNO DRU	1.500	175.047	0	2	-163.347	0	1
	16:WIND RESI	1.500	649.102	0	2	-455.636	0	1
	9:COMPRESSI	1.500	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0Wf	1.500	1.77E+3	0	1	-1.57E+3	0	3
	4:1.25DL	1.500	1.56E+3	0	1	-1.55E+3	0	3
	5:1.1DL+1.0Wz	1.500	1.26E+3	1.500	4	-1.22E+3	1.500	2
	6:CASE I: VX	1.500	639.564	0	3	-611.547	0	1
	7:1.1DL+1.0Wz	1.500	2.89E+3	0	1	-3.08E+3	0	3
	8:CASE I: VY	1.500	1.25E+3	0	1	-1.24E+3	0	3
	13:CASE III: V	1.500	934.913	0	1	-931.373	0	3
	14:CASE III: Vz	1.500	1.15E+3	0	1	-1.3E+3	0	3
	15:CASE III: VX	1.500	131.285	0	2	-122.511	0	1
3	2:DYNO DRUM	0.500				-258.921	0.500	2
	1:WEIGHT	0.500	2.29E+3	0.500	3	-2.19E+3	0.500	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	10:WIND LOAL	0.500	232.567	0.500	2	-232.567	0.500	4
	11:WIND LOAL	0.500	3.05E+3	0.500	1	-3.19E+3	0.500	3
	12:DYNO DRU	0.500	125.081	0.500	3	-110.417	0.500	1
	16:WIND RESI	0.500	343.758	0.500	2	-235.072	0.500	4
	9:COMPRESSI	0.500	0.000	0.500	1	-0.000	0.500	3
	3:1.1DL+1.0Wf	0.500	2.79E+3	0.500	3	-2.57E+3	0.500	1
	4:1.25DL	0.500	2.87E+3	0.500	3	-2.74E+3	0.500	1
	5:1.1DL+1.0Wj	0.500	2.64E+3	0.500	3	-2.51E+3	0.500	1
	6:CASE I: VX	0.500	232.567	0.500	2	-232.567	0.500	4
	7:1.1DL+1.0Wk	0.500	5.23E+3	0.500	3	-5.16E+3	0.500	1
	8:CASE I: VY	0.500	2.29E+3	0.500	3	-2.19E+3	0.500	1
	13:CASE III: V'	0.500	1.72E+3	0.500	3	-1.64E+3	0.500	1
	14:CASE III: V ₂	0.500	2.03E+3	0.500	3	-2.06E+3	0.500	1
	15:CASE III: VX	0.500	93.811	0.500	3	-82.813	0.500	1
4	2:DYNO DRUM	7.000	1.3E+3	0	1	-1.55E+3	0	2
	1:WEIGHT	7.000	3.82E+3	0	3	-3.82E+3	0	1
	10:WIND LOAL	7.000	101.440	0	1	-101.076	0	3
	11:WIND LOAL	7.000	5.07E+3	0	1	-5.07E+3	0	3
	12:DYNO DRU	7.000				-26.640	0	1
	16:WIND RESI	7.000	597.088	0	2	-542.405	0	1
	9:COMPRESSI	7.000	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0Wf	7.000	4.74E+3	0	3	-4.69E+3	0	1
	4:1.25DL	7.000	4.77E+3	0	3	-4.77E+3	0	1
	5:1.1DL+1.0Wj	7.000	4.09E+3	0	3	-4.12E+3	0	1
	6:CASE I: VX	7.000	101.440	0	1	-101.076	0	3
	7:1.1DL+1.0Wk	7.000	9.13E+3	0	3	-9.32E+3	0	1
	8:CASE I: VY	7.000	3.82E+3	0	3	-3.82E+3	0	1
	13:CASE III: V'	7.000	2.86E+3	0	3	-2.86E+3	0	1
	14:CASE III: V ₂	7.000	3.71E+3	0	3	-3.85E+3	0	1
	15:CASE III: VX	7.000				-19.980	0	1
5	2:DYNO DRUM	2.000	899.971	2.000	2	-846.659	2.000	4
	1:WEIGHT	2.000	1.78E+3	2.000	1	-1.79E+3	2.000	3
	10:WIND LOAL	2.000	700.758	2.000	3	-715.738	2.000	1
	11:WIND LOAL	2.000	2.31E+3	2.000	3	-2.3E+3	2.000	1
	12:DYNO DRU	2.000	151.032	2.000	2	-165.282	2.000	4
	16:WIND RESI	2.000	254.507	2.000	4	-341.616	2.000	2
	9:COMPRESSI	2.000	0.000	2.000	3	-0.000	2.000	1
	3:1.1DL+1.0Wf	2.000	1.81E+3	2.000	1	-1.9E+3	2.000	3
	4:1.25DL	2.000	2.23E+3	2.000	1	-2.24E+3	2.000	3
	5:1.1DL+1.0Wj	2.000	1.49E+3	2.000	2	-1.53E+3	2.000	4
	6:CASE I: VX	2.000	700.758	2.000	3	-715.738	2.000	1
	7:1.1DL+1.0Wk	2.000	4.35E+3	2.000	2	-4.4E+3	2.000	4
	8:CASE I: VY	2.000	1.78E+3	2.000	1	-1.79E+3	2.000	3
	13:CASE III: V'	2.000	1.34E+3	2.000	1	-1.34E+3	2.000	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	14:CASE III: V _z	2.000	1.84E+3	2.000	2	-1.87E+3	2.000	4
	15:CASE III: VX	2.000	113.274	2.000	2	-123.962	2.000	4
6	2:DYNO DRUM	2.000	900.192	2.000	4	-846.880	2.000	2
	1:WEIGHT	2.000	4.09E+3	2.000	3	-4.1E+3	2.000	1
	10:WIND LOAL	2.000	715.738	2.000	2	-700.758	2.000	4
	11:WIND LOAL	2.000	6.34E+3	2.000	1	-6.33E+3	2.000	3
	12:DYNO DRU	2.000	165.089	2.000	3	-150.891	2.000	1
	16:WIND RESI	2.000	585.376	2.000	2	-601.798	2.000	4
	9:COMPRESSI	2.000	0.000	2.000	1	-0.000	2.000	3
	3:1.1DL+1.0W _i	2.000	4.68E+3	2.000	3	-4.7E+3	2.000	1
	4:1.25DL	2.000	5.12E+3	2.000	3	-5.13E+3	2.000	1
	5:1.1DL+1.0W _j	2.000	4.13E+3	2.000	3	-4.11E+3	2.000	1
	6:CASE I: VX	2.000	715.738	2.000	2	-700.758	2.000	4
	7:1.1DL+1.0W _z	2.000	9.17E+3	2.000	3	-9.15E+3	2.000	1
	8:CASE I: VY	2.000	4.09E+3	2.000	3	-4.1E+3	2.000	1
	13:CASE III: V'	2.000	3.07E+3	2.000	3	-3.08E+3	2.000	1
	14:CASE III: V _z	2.000	3.55E+3	2.000	4	-3.53E+3	2.000	2
	15:CASE III: VX	2.000	123.817	2.000	3	-113.168	2.000	1
7	2:DYNO DRUM	1.000	897.537	1.000	2	-809.062	1.000	1
	1:WEIGHT	1.000	290.880	1.000	3	-291.444	1.000	1
	10:WIND LOAL	1.000	6.556	1.000	2	-6.526	1.000	4
	11:WIND LOAL	1.000	131.822	1.000	1	-131.077	1.000	3
	12:DYNO DRU	1.000	19.731	0	1			
	16:WIND RESI	1.000	334.522	1.000	1	-348.459	1.000	2
	9:COMPRESSI	1.000	0.000	1.000	1	-0.000	1.000	3
	3:1.1DL+1.0W _i	1.000	652.020	1.000	4	-666.576	1.000	2
	4:1.25DL	1.000	363.601	1.000	3	-364.305	1.000	1
	5:1.1DL+1.0W _j	1.000	330.205	1.000	3	-303.573	1.000	1
	6:CASE I: VX	1.000	6.556	1.000	2	-6.526	1.000	4
	7:1.1DL+1.0W _z	1.000	1.19E+3	1.000	3	-1.12E+3	1.000	1
	8:CASE I: VY	1.000	290.880	1.000	3	-291.444	1.000	1
	13:CASE III: V'	1.000	218.160	1.000	3	-218.583	1.000	1
	14:CASE III: V _z	1.000	651.653	1.000	3	-596.214	1.000	1
	15:CASE III: VX	1.000	14.798	0	1			
8	2:DYNO DRUM	1.500	819.536	0	1	-432.734	0	2
	1:WEIGHT	1.500	4.2E+3	0	3	-3.18E+3	0	1
	10:WIND LOAL	1.500	2E+3	0	1	-2.03E+3	0	3
	11:WIND LOAL	1.500	4.59E+3	0	1	-5.94E+3	0	3
	12:DYNO DRU	1.500	558.154	0	3	-599.239	0	1
	16:WIND RESI	1.500	1.23E+3	0	1	-1.44E+3	0	3
	9:COMPRESSI	1.500	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0W _i	1.500	3.85E+3	0	3	-2.93E+3	0	1
	4:1.25DL	1.500	5.25E+3	0	3	-3.97E+3	0	1
	5:1.1DL+1.0W _j	1.500	3.31E+3	0	3	-2.24E+3	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	6:CASE I: VX	1.500	2E+3	0	1	-2.03E+3	0	3
	7:1.1DL+1.0W ₂	1.500	8.63E+3	0	3	-6.19E+3	0	1
	8:CASE I: VY	1.500	4.2E+3	0	3	-3.18E+3	0	1
	13:CASE III: V'	1.500	3.15E+3	0	3	-2.38E+3	0	1
	14:CASE III: V ₂	1.500	3.03E+3	0	3	-2.05E+3	0	1
	15:CASE III: VX	1.500	418.615	0	3	-449.429	0	1
9	2:DYNO DRUM	0.500	212.591	0	1			
	1:WEIGHT	0.500	866.667	0.500	1	-92.067	0.500	3
	10:WIND LOA	0.500	581.498	0.500	3	-581.498	0.500	1
	11:WIND LOA	0.500	192.594	0.500	3	-1.22E+3	0.500	1
	12:DYNO DRU	0.500	227.558	0.500	2	-212.894	0.500	4
	16:WIND RES	0.500	425.346	0.500	3	-507.547	0.500	1
	9:COMPRESS	0.500	0.000	0.500	3	-0.000	0.500	1
	3:1.1DL+1.0W ₁	0.500	810.237	0	1	-40.378	0	2
	4:1.25DL	0.500	1.08E+3	0.500	1	-115.083	0.500	3
	5:1.1DL+1.0W ₂	0.500	868.021	0	1	-1.297	0	2
	6:CASE I: VX	0.500	581.498	0.500	3	-581.498	0.500	1
	7:1.1DL+1.0W ₂	0.500	1.77E+3	0	1			
	8:CASE I: VY	0.500	866.667	0.500	1	-92.067	0.500	3
	13:CASE III: V'	0.500	650.000	0.500	1	-69.050	0.500	3
	14:CASE III: V ₂	0.500	679.124	0	1			
	15:CASE III: VX	0.500	170.668	0.500	2	-159.671	0.500	4
10	2:DYNO DRUM	7.000	1.55E+3	0	1	-1.3E+3	0	2
	1:WEIGHT	7.000	3.37E+3	0	3	-3.37E+3	0	1
	10:WIND LOA	7.000	98.654	0	3	-99.018	0	1
	11:WIND LOA	7.000	4.31E+3	0	1	-4.31E+3	0	3
	12:DYNO DRU	7.000				-27.613	0	1
	16:WIND RES	7.000	507.675	0	2	-606.505	0	1
	9:COMPRESS	7.000	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0W ₁	7.000	4.21E+3	0	3	-4.3E+3	0	1
	4:1.25DL	7.000	4.22E+3	0	3	-4.22E+3	0	1
	5:1.1DL+1.0W ₂	7.000	3.79E+3	0	3	-3.82E+3	0	1
	6:CASE I: VX	7.000	98.654	0	3	-99.018	0	1
	7:1.1DL+1.0W ₂	7.000	8.3E+3	0	3	-8.15E+3	0	1
	8:CASE I: VY	7.000	3.37E+3	0	3	-3.37E+3	0	1
	13:CASE III: V'	7.000	2.53E+3	0	3	-2.53E+3	0	1
	14:CASE III: V ₂	7.000	3.44E+3	0	3	-3.33E+3	0	1
	15:CASE III: VX	7.000				-20.710	0	1
11	2:DYNO DRUM	0.670	464.323	0	2	-464.323	0	1
	1:WEIGHT	0.670	6.11E+3	0	2	-6.29E+3	0	1
	10:WIND LOA	0.670	1.99E+3	0.670	4	-1.92E+3	0.670	2
	11:WIND LOA	0.670	8.55E+3	0	1	-8.23E+3	0	2
	12:DYNO DRU	0.670	397.413	0	1	-416.594	0	3
	16:WIND RES	0.670	958.260	0.670	3	-920.721	0.670	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	9:COMPRESSI	0.670	0.000	0.670	1	-0.000	0.670	3
	3:1.1DL+1.0Wf	0.670	6.81E+3	0	3	-6.98E+3	0	1
	4:1.25DL	0.670	7.64E+3	0	2	-7.86E+3	0	1
	5:1.1DL+1.0Wj	0.670	6.36E+3	0	3	-6.52E+3	0	1
	6:CASE I: VX	0.670	1.99E+3	0.670	4	-1.92E+3	0.670	2
	7:1.1DL+1.0Wz	0.670	13.9E+3	0	2	-14.3E+3	0	1
	8:CASE I: VY	0.670	6.11E+3	0	2	-6.29E+3	0	1
	13:CASE III: V'	0.670	4.58E+3	0	2	-4.72E+3	0	1
	14:CASE III: Vz	0.670	5.42E+3	0	2	-5.54E+3	0	1
	15:CASE III:VX	0.670	298.060	0	1	-312.446	0	3
14	2:DYNO DRUM	0.670	874.350	0.670	1	-874.350	0.670	2
	1:WEIGHT	0.670	8.46E+3	0	1	-8.64E+3	0	2
	10:WIND LOAL	0.670	1.92E+3	0.670	3	-1.99E+3	0.670	1
	11:WIND LOAL	0.670	12.6E+3	0	2	-12.3E+3	0	1
	12:DYNO DRU	0.670	416.595	0	1	-397.414	0	3
	16:WIND RESI	0.670	1.15E+3	0.670	3	-1.19E+3	0.670	1
	9:COMPRESSI	0.670	0.000	0.670	2	-0.000	0.670	4
	3:1.1DL+1.0Wf	0.670	8.45E+3	0	1	-8.69E+3	0	2
	4:1.25DL	0.670	10.6E+3	0	1	-10.8E+3	0	2
	5:1.1DL+1.0Wj	0.670	7.79E+3	0	1	-8.04E+3	0	2
	6:CASE I: VX	0.670	1.92E+3	0.670	3	-1.99E+3	0.670	1
	7:1.1DL+1.0Wz	0.670	18.2E+3	0	1	-18.6E+3	0	2
	8:CASE I: VY	0.670	8.46E+3	0	1	-8.64E+3	0	2
	13:CASE III: V'	0.670	6.34E+3	0	1	-6.48E+3	0	2
	14:CASE III: Vz	0.670	6.64E+3	0	1	-6.82E+3	0	2
	15:CASE III:VX	0.670	312.446	0	1	-298.060	0	3
20	2:DYNO DRUM	7.000	1.29E+3	7.000	1	-1.54E+3	7.000	2
	1:WEIGHT	7.000	2.63E+3	7.000	3	-2.63E+3	7.000	1
	10:WIND LOAL	7.000	101.076	7.000	3	-101.440	7.000	1
	11:WIND LOAL	7.000	3.33E+3	7.000	1	-3.33E+3	7.000	3
	12:DYNO DRU	7.000	27.241	7.000	2			
	16:WIND RESI	7.000	626.343	7.000	2	-507.442	7.000	1
	9:COMPRESSI	7.000	0.000	7.000	3	-0.000	7.000	1
	3:1.1DL+1.0Wf	7.000	3.52E+3	7.000	3	-3.4E+3	7.000	1
	4:1.25DL	7.000	3.29E+3	7.000	3	-3.29E+3	7.000	1
	5:1.1DL+1.0Wj	7.000	3.01E+3	7.000	3	-2.98E+3	7.000	1
	6:CASE I: VX	7.000	101.076	7.000	3	-101.440	7.000	1
	7:1.1DL+1.0Wz	7.000	6.5E+3	7.000	4	-6.63E+3	7.000	2
	8:CASE I: VY	7.000	2.63E+3	7.000	3	-2.63E+3	7.000	1
	13:CASE III: V'	7.000	1.97E+3	7.000	3	-1.97E+3	7.000	1
	14:CASE III: Vz	7.000	2.71E+3	7.000	4	-2.8E+3	7.000	2
	15:CASE III:VX	7.000	20.431	7.000	2			
21	2:DYNO DRUM	7.000	1.54E+3	7.000	1	-1.3E+3	7.000	2
	1:WEIGHT	7.000	4.56E+3	7.000	3	-4.56E+3	7.000	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	10:WIND LOAL	7.000	99.018	7.000	1	-98.654	7.000	3
	11:WIND LOAL	7.000	6.05E+3	7.000	1	-6.05E+3	7.000	3
	12:DYNO DRU	7.000	27.013	7.000	3			
	16:WIND RESI	7.000	545.005	7.000	2	-619.758	7.000	1
	9:COMPRESSI	7.000	0.000	7.000	1	-0.000	7.000	3
	3:1.1DL+1.0Wf	7.000	5.5E+3	7.000	3	-5.57E+3	7.000	1
	4:1.25DL	7.000	5.7E+3	7.000	3	-5.7E+3	7.000	1
	5:1.1DL+1.0Wj	7.000	4.94E+3	7.000	3	-4.91E+3	7.000	1
	6:CASE I: VX	7.000	99.018	7.000	1	-98.654	7.000	3
	7:1.1DL+1.0Wz	7.000	10.9E+3	7.000	4	-10.8E+3	7.000	2
	8:CASE I: VY	7.000	4.56E+3	7.000	3	-4.56E+3	7.000	1
	13:CASE III: V'	7.000	3.42E+3	7.000	3	-3.42E+3	7.000	1
	14:CASE III: Vz	7.000	4.45E+3	7.000	4	-4.32E+3	7.000	2
	15:CASE III: VX	7.000	20.260	7.000	3			
22	2:DYNO DRUM	0.500				-222.179	0	1
	1:WEIGHT	0.500	1.5E+3	0.500	3	-1.4E+3	0.500	1
	10:WIND LOAL	0.500	232.567	0	3	-232.567	0	1
	11:WIND LOAL	0.500	1.95E+3	0.500	1	-2.09E+3	0.500	3
	12:DYNO DRU	0.500	110.404	0	1	-125.127	0	2
	16:WIND RESI	0.500	322.844	0	1	-214.157	0	2
	9:COMPRESSI	0.500	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0Wf	0.500	1.71E+3	0.500	3	-1.48E+3	0.500	1
	4:1.25DL	0.500	1.88E+3	0.500	3	-1.75E+3	0.500	1
	5:1.1DL+1.0Wj	0.500	1.65E+3	0.500	3	-1.55E+3	0.500	1
	6:CASE I: VX	0.500	232.567	0	3	-232.567	0	1
	7:1.1DL+1.0Wz	0.500	3.3E+3	0.500	3	-3.22E+3	0.500	1
	8:CASE I: VY	0.500	1.5E+3	0.500	3	-1.4E+3	0.500	1
	13:CASE III: V'	0.500	1.13E+3	0.500	3	-1.05E+3	0.500	1
	14:CASE III: Vz	0.500	1.24E+3	0.500	3	-1.27E+3	0.500	1
	15:CASE III: VX	0.500	82.803	0	1	-93.845	0	2
23	2:DYNO DRUM	0.500	262.766	0	1	-12.859	0	2
	1:WEIGHT	0.500	1.6E+3	0	3	-827.225	0	1
	10:WIND LOAL	0.500	581.498	0	1	-581.498	0	3
	11:WIND LOAL	0.500	1.25E+3	0	1	-2.27E+3	0	3
	12:DYNO DRU	0.500	212.848	0	4	-227.571	0	1
	16:WIND RESI	0.500	448.937	0	1	-531.138	0	2
	9:COMPRESSI	0.500	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0Wf	0.500	1.73E+3	0	3	-958.821	0	1
	4:1.25DL	0.500	2E+3	0	3	-1.03E+3	0	1
	5:1.1DL+1.0Wj	0.500	1.62E+3	0	3	-779.673	0	1
	6:CASE I: VX	0.500	581.498	0	1	-581.498	0	3
	7:1.1DL+1.0Wz	0.500	3.75E+3	0	3	-1.88E+3	0	1
	8:CASE I: VY	0.500	1.6E+3	0	3	-827.225	0	1
	13:CASE III: V'	0.500	1.2E+3	0	3	-620.419	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	14:CASE III: V _z	0.500	1.49E+3	0	3	-728.760	0	1
	15:CASE III: VX	0.500	159.636	0	4	-170.678	0	1
24	2:DYNO DRUM	1.500	409.001	1.500	4	-806.095	1.500	2
	1:WEIGHT	1.500	4.79E+3	1.500	3	-4.79E+3	1.500	1
	10:WIND LOAL	1.500	611.547	1.500	1	-639.564	1.500	3
	11:WIND LOAL	1.500	6.71E+3	1.500	1	-6.72E+3	1.500	3
	12:DYNO DRU	1.500	163.040	1.500	4	-174.739	1.500	2
	16:WIND RESI	1.500	379.521	1.500	1	-277.027	1.500	3
	9:COMPRESSI	1.500	0.000	1.500	1	-0.000	1.500	3
	3:1.1DL+1.0W _i	1.500	5.39E+3	1.500	4	-5.28E+3	1.500	2
	4:1.25DL	1.500	5.99E+3	1.500	3	-5.99E+3	1.500	1
	5:1.1DL+1.0W _j	1.500	5.06E+3	1.500	4	-5.09E+3	1.500	2
	6:CASE I: VX	1.500	611.547	1.500	1	-639.564	1.500	3
	7:1.1DL+1.0W _z	1.500	11.1E+3	1.500	4	-11.4E+3	1.500	2
	8:CASE I: VY	1.500	4.79E+3	1.500	3	-4.79E+3	1.500	1
	13:CASE III: V'	1.500	3.6E+3	1.500	3	-3.59E+3	1.500	1
	14:CASE III: V _z	1.500	4.35E+3	1.500	4	-4.57E+3	1.500	2
	15:CASE III: VX	1.500	122.280	1.500	4	-131.054	1.500	2
25	2:DYNO DRUM	1.500	760.263	1.500	1	-373.460	1.500	3
	1:WEIGHT	1.500	2.96E+3	1.500	1	-1.93E+3	1.500	3
	10:WIND LOAL	1.500	2.03E+3	1.500	4	-2E+3	1.500	2
	11:WIND LOAL	1.500	3.06E+3	1.500	3	-4.42E+3	1.500	1
	12:DYNO DRU	1.500	599.547	1.500	1	-558.461	1.500	3
	16:WIND RESI	1.500	1.02E+3	1.500	4	-1.1E+3	1.500	2
	9:COMPRESSI	1.500	0.000	1.500	3	-0.000	1.500	1
	3:1.1DL+1.0W _i	1.500	2.46E+3	1.500	1	-1.4E+3	1.500	3
	4:1.25DL	1.500	3.7E+3	1.500	1	-2.42E+3	1.500	3
	5:1.1DL+1.0W _j	1.500	2.14E+3	1.500	1	-938.302	1.500	3
	6:CASE I: VX	1.500	2.03E+3	1.500	4	-2E+3	1.500	2
	7:1.1DL+1.0W _z	1.500	6.48E+3	1.500	1	-3.9E+3	1.500	3
	8:CASE I: VY	1.500	2.96E+3	1.500	1	-1.93E+3	1.500	3
	13:CASE III: V'	1.500	2.22E+3	1.500	1	-1.45E+3	1.500	3
	14:CASE III: V _z	1.500	2.41E+3	1.500	1	-1.33E+3	1.500	3
	15:CASE III: VX	1.500	449.660	1.500	1	-418.846	1.500	3
26	2:DYNO DRUM	1.000	808.316	0	2	-897.070	0	1
	1:WEIGHT	1.000	255.049	0	3	-255.524	0	1
	10:WIND LOAL	1.000	4.826	0	1	-4.584	0	3
	11:WIND LOAL	1.000	83.151	0	1	-82.524	0	3
	12:DYNO DRU	1.000	2.370	0	1	-2.238	0	2
	16:WIND RESI	1.000	360.260	0	1	-332.245	0	2
	9:COMPRESSI	1.000	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0W _i	1.000	639.291	0	1	-611.797	0	2
	4:1.25DL	1.000	318.812	0	3	-319.405	0	1
	5:1.1DL+1.0W _j	1.000	281.424	0	3	-281.572	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	6:CASE I: VX	1.000	4.826	0	1	-4.584	0	3
	7:1.1DL+1.0W ₂	1.000	1.03E+3	0	3	-1.09E+3	0	1
	8:CASE I: VY	1.000	255.049	0	3	-255.524	0	1
	13:CASE III: V'	1.000	191.287	0	3	-191.643	0	1
	14:CASE III: V ₂	1.000	565.827	0	2	-611.772	0	1
	15:CASE III:VX	1.000	1.778	0	1	-1.678	0	2
27	2:DYNO DRUM	1.000	897.830	0	2	-809.355	0	1
	1:WEIGHT	1.000	235.561	0	3	-236.125	0	1
	10:WIND LOAL	1.000	6.526	0	3	-6.556	0	1
	11:WIND LOAL	1.000	50.503	0	1	-49.758	0	3
	12:DYNO DRU	1.000	2.399	0	1	-2.602	0	2
	16:WIND RESI	1.000	331.171	0	1	-360.384	0	2
	9:COMPRESSI	1.000	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0W ₁	1.000	590.288	0	1	-620.122	0	2
	4:1.25DL	1.000	294.451	0	3	-295.156	0	1
	5:1.1DL+1.0W ₂	1.000	267.020	0	3	-267.873	0	1
	6:CASE I: VX	1.000	6.526	0	3	-6.556	0	1
	7:1.1DL+1.0W ₂	1.000	1.05E+3	0	2	-994.497	0	1
	8:CASE I: VY	1.000	235.561	0	3	-236.125	0	1
	13:CASE III: V'	1.000	176.671	0	3	-177.094	0	1
	14:CASE III: V ₂	1.000	595.183	0	2	-551.202	0	1
	15:CASE III:VX	1.000	1.799	0	1	-1.951	0	2
28	2:DYNO DRUM	2.500				-0.000	2.292	1
	1:WEIGHT	2.500	3.47E+3	0	1	-3.47E+3	0	3
	10:WIND LOAL	2.500	982.292	0	3	-982.292	0	1
	11:WIND LOAL	2.500	4.79E+3	0	3	-4.79E+3	0	1
	12:DYNO DRU	2.500	290.717	0	1	-290.717	0	3
	16:WIND RESI	2.500	568.945	0	3	-568.945	0	1
	9:COMPRESSI	2.500	1.03E+3	0	1			
	3:1.1DL+1.0W ₁	2.500	3.25E+3	0	1	-3.25E+3	0	3
	4:1.25DL	2.500	4.34E+3	0	1	-4.34E+3	0	3
	5:1.1DL+1.0W ₂	2.500	3.13E+3	0	1	-3.13E+3	0	3
	6:CASE I: VX	2.500	982.292	0	3	-982.292	0	1
	7:1.1DL+1.0W ₂	2.500	7.08E+3	0	1	-7.08E+3	0	3
	8:CASE I: VY	2.500	3.47E+3	0	1	-3.47E+3	0	3
	13:CASE III: V'	2.500	2.61E+3	0	1	-2.61E+3	0	3
	14:CASE III: V ₂	2.500	2.44E+3	0	1	-2.44E+3	0	3
	15:CASE III:VX	2.500	218.038	0	1	-218.038	0	3
29	2:DYNO DRUM	2.500	874.350	2.292	3	-874.350	2.292	1
	1:WEIGHT	2.500	9.3E+3	2.500	3	-9.3E+3	2.500	1
	10:WIND LOAL	2.500	982.292	0	1	-982.292	0	3
	11:WIND LOAL	2.500	13.7E+3	2.500	1	-13.7E+3	2.500	3
	12:DYNO DRU	2.500	290.717	0	3	-290.717	0	1
	16:WIND RESI	2.500	910.312	2.500	3	-910.312	2.500	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	9:COMPRESSI	2.500	1.03E+3	0	1			
	3:1.1DL+1.0Wf	2.500	11.1E+3	2.500	3	-11.1E+3	2.500	1
	4:1.25DL	2.500	11.6E+3	2.500	3	-11.6E+3	2.500	1
	5:1.1DL+1.0Wj	2.500	10.2E+3	2.500	3	-10.2E+3	2.500	1
	6:CASE I: VX	2.500	982.292	0	1	-982.292	0	3
	7:1.1DL+1.0Wz	2.500	22.2E+3	2.500	3	-22.2E+3	2.500	1
	8:CASE I: VY	2.500	9.3E+3	2.500	3	-9.3E+3	2.500	1
	13:CASE III: V'	2.500	6.97E+3	2.500	3	-6.97E+3	2.500	1
	14:CASE III: Vz	2.500	9.01E+3	2.500	3	-9.01E+3	2.500	1
	15:CASE III: VX	2.500	218.038	0	3	-218.038	0	1
30	2:DYNO DRUM	1.000	0.000	1.000	1	-0.000	1.000	3
	1:WEIGHT	1.000	20.588	0	3	-20.588	0	1
	10:WIND LOAL	1.000	41.667	0	1	-41.667	0	2
	11:WIND LOAL	1.000	41.666	0	1	-41.666	0	3
	12:DYNO DRU	1.000	0.000	0	1	-0.000	0	3
	16:WIND RESI	1.000	56.769	0	1	-66.975	0	2
	9:COMPRESSI	1.000	0.000	1.000	3	-0.000	1.000	1
	3:1.1DL+1.0Wf	1.000	79.416	0	1	-89.621	0	2
	4:1.25DL	1.000	25.735	0	3	-25.735	0	1
	5:1.1DL+1.0Wj	1.000	64.313	0	1	-64.313	0	2
	6:CASE I: VX	1.000	41.667	0	1	-41.667	0	2
	7:1.1DL+1.0Wz	1.000	102.062	0	1	-112.268	0	2
	8:CASE I: VY	1.000	20.588	0	3	-20.588	0	1
	13:CASE III: V'	1.000	15.441	0	3	-15.441	0	1
	14:CASE III: Vz	1.000	59.562	0	1	-67.216	0	2
	15:CASE III: VX	1.000	0.000	0	1	-0.000	0	3
31	2:DYNO DRUM	1.000	0.000	0.917	1	-0.000	0.917	3
	1:WEIGHT	1.000	20.588	0	3	-20.588	0	1
	10:WIND LOAL	1.000	41.667	0	1	-41.667	0	2
	11:WIND LOAL	1.000	41.667	0	1	-41.667	0	3
	12:DYNO DRU	1.000	0.000	0	3	-0.000	0	1
	16:WIND RESI	1.000	56.769	0	1	-66.975	0	2
	9:COMPRESSI	1.000	0.000	0	2	-0.000	0	1
	3:1.1DL+1.0Wf	1.000	79.416	0	1	-89.622	0	2
	4:1.25DL	1.000	25.735	0	3	-25.735	0	1
	5:1.1DL+1.0Wj	1.000	64.314	0	1	-64.314	0	2
	6:CASE I: VX	1.000	41.667	0	1	-41.667	0	2
	7:1.1DL+1.0Wz	1.000	102.063	0	1	-112.269	0	2
	8:CASE I: VY	1.000	20.588	0	3	-20.588	0	1
	13:CASE III: V'	1.000	15.441	0	3	-15.441	0	1
	14:CASE III: Vz	1.000	59.562	0	1	-67.216	0	2
	15:CASE III: VX	1.000	0.000	0	3	-0.000	0	1
32	2:DYNO DRUM	4.830	874.350	0	1	-874.350	0	2
	1:WEIGHT	4.830	5.73E+3	0	1	-5.93E+3	4.830	2



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	10:WIND LOAL	4.830	1.92E+3	0	3	-1.99E+3	0	1
	11:WIND LOAL	4.830	9.03E+3	0	2	-8.72E+3	0	1
	12:DYNO DRU	4.830	300.308	0	1	-281.127	0	2
	16:WIND RESI	4.830	1.15E+3	0	3	-1.19E+3	0	1
	9:COMPRESSI	4.830	0.000	4.830	2	-0.000	4.830	1
	3:1.1DL+1.0Wf	4.830	6.62E+3	0	1	-6.89E+3	4.830	2
	4:1.25DL	4.830	7.16E+3	0	1	-7.42E+3	4.830	2
	5:1.1DL+1.0Wj	4.830	6.56E+3	0	1	-6.81E+3	0	2
	6:CASE I: VX	4.830	1.92E+3	0	3	-1.99E+3	0	1
	7:1.1DL+1.0Wz	4.830	13.8E+3	0	1	-14.3E+3	4.830	2
	8:CASE I: VY	4.830	5.73E+3	0	1	-5.93E+3	4.830	2
	13:CASE III: V'	4.830	4.3E+3	0	1	-4.45E+3	4.830	2
	14:CASE III: Vz	4.830	5.62E+3	0	1	-5.82E+3	4.830	2
	15:CASE III:VX	4.830	225.231	0	1	-210.845	0	2
33	2:DYNO DRUM	4.830	0.000	0	1	-0.000	0	2
	1:WEIGHT	4.830	3.38E+3	0	2	-3.59E+3	4.830	1
	10:WIND LOAL	4.830	1.99E+3	0	1	-1.92E+3	0	2
	11:WIND LOAL	4.830	4.95E+3	4.830	1	-4.63E+3	4.830	2
	12:DYNO DRU	4.830	281.127	0	2	-300.308	0	1
	16:WIND RESI	4.830	958.260	0	3	-920.721	0	1
	9:COMPRESSI	4.830	0.000	0	1	-0.000	0	2
	3:1.1DL+1.0Wf	4.830	4.68E+3	0	2	-4.85E+3	0	1
	4:1.25DL	4.830	4.23E+3	0	2	-4.48E+3	4.830	1
	5:1.1DL+1.0Wj	4.830	4.02E+3	0	2	-4.18E+3	0	1
	6:CASE I: VX	4.830	1.99E+3	0	1	-1.92E+3	0	2
	7:1.1DL+1.0Wz	4.830	8.4E+3	0	2	-8.77E+3	0	1
	8:CASE I: VY	4.830	3.38E+3	0	2	-3.59E+3	4.830	1
	13:CASE III: V'	4.830	2.54E+3	0	2	-2.69E+3	4.830	1
	14:CASE III: Vz	4.830	3.51E+3	0	2	-3.63E+3	0	1
	15:CASE III:VX	4.830	210.845	0	2	-225.231	0	1



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Plate Center Stress Summary

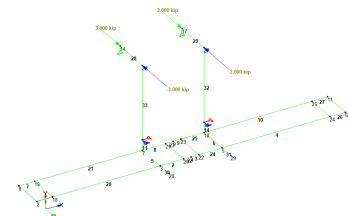
	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Max Qx	17	7:1.1DL+1.0Wz	13.066	-0.259	-0.054	-0.695	46.440	-2.318	-0.460	0.389
Min Qx	17	11:WIND LOA	-8.297	0.024	0.068318	0.216	0.050	1.462	0.415	-0.250
Max Qy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Qy	18	7:1.1DL+1.0Wz	-4.398	-3.035	-15.381	-53.154	35.615	1.584	2.158	-6.338
Max Sx	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Sx	18	7:1.1DL+1.0Wz	-4.398	-3.035	-15.381	-53.154	35.615	1.584	2.158	-6.338
Max Sy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Sy	18	7:1.1DL+1.0Wz	-4.398	-3.035	-15.381	-53.154	35.615	1.584	2.158	-6.338
Max Sxy	17	2:DYNO DRUM	0.317	0.001	-0.011	-0.044	77.028	-0.143	-0.043	0.008
Min Sxy	19	2:DYNO DRUM	-0.361	0.001	-0.011	-0.044	-77.028	0.143	0.042553	0.010
Max Mx	19	7:1.1DL+1.0Wz	-3.175	0.319	-0.185	-0.592	-52.763	4.392	1.541	0.050
Min Mx	19	11:WIND LOA	2.301	-0.064	0.068	0.216	-0.050	-3.000	-0.915	-0.037
Max My	18	7:1.1DL+1.0Wz	-4.398	-3.035	-15.381	-53.154	35.615	1.584	2.158	-6.338
Min My	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Max Mxy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Mxy	18	7:1.1DL+1.0Wz	-4.398	-3.035	-15.381	-53.154	35.615	1.584	2.158	-6.338

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	12	7:1.1DL+1.0Wz	1.887	0	-0.197	0	0	0
Min FX	15	7:1.1DL+1.0Wz	-2.396	0	0.001	0	0	0
Max FY	17	7:1.1DL+1.0Wz	0	0.816	0	0	0	0
Min FY	17	11:WIND LOA	0	-0.460	0	0	0	0
Max FZ	15	2:DYNO DRUM	0.010	0	0.157	0	0	0
Min FZ	12	16:WIND RESI	-0.251	0	-0.353	0	0	0
Max MX	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MX	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Max MY	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MY	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Max MZ	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MZ	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0

2.396 kips = 3 kips, therefore 3 kips applied at nodes 26, 14 and 27, 17 for compression member check (28, and 29).

$$PL^3/3EI = (3.00 \text{ kips}) * (5.5'/12)^3 / (3 * (29000 \text{ ksi}) * (5.04)) = 1.96", \text{ OK}$$





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Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.026	1.000	0.026	HSS FLEX+A	7	1.890	2.460	2.460	4.030
2	HSST3X3X0	HSST3X3X0	0.137	1.000	0.137	HSS TORSIO	7	1.890	2.460	2.460	4.030
3	HSST3X3X0	HSST3X3X0	0.174	1.000	0.174	HSS T+SH+F	7	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.263	1.000	0.263	HSS T+SH+F	7	1.890	2.460	2.460	4.030
5	HSST3.5X3.	HSST3.5X3.	0.148	1.000	0.148	HSS TORSIO	7	2.910	5.040	5.040	8.350
6	HSST3.5X3.	HSST3.5X3.	0.282	1.000	0.282	HSS T+SH+F	7	2.910	5.040	5.040	8.350
7	HSST3X3X0	HSST3X3X0	0.030	1.000	0.030	HSS FLEX+A	7	1.890	2.460	2.460	4.030
8	HSST3X3X0	HSST3X3X0	0.320	1.000	0.320	HSS T+SH+F	7	1.890	2.460	2.460	4.030
9	HSST3X3X0	HSST3X3X0	0.206	1.000	0.206	HSS TORSIO	7	1.890	2.460	2.460	4.030
10	HSST3X3X0	HSST3X3X0	0.231	1.000	0.231	HSS T+SH+F	7	1.890	2.460	2.460	4.030
11	HSST3.5X3.	HSST3.5X3.	0.362	1.000	0.362	HSS FLEX+A	7	2.910	5.040	5.040	8.350
14	HSST3.5X3.	HSST3.5X3.	0.470	1.000	0.470	HSS FLEX+A	7	2.910	5.040	5.040	8.350
20	HSST3X3X0	HSST3X3X0	0.180	1.000	0.180	HSS T+SH+F	7	1.890	2.460	2.460	4.030
21	HSST3X3X0	HSST3X3X0	0.314	1.000	0.314	HSS T+SH+F	7	1.890	2.460	2.460	4.030
22	HSST3X3X0	HSST3X3X0	0.134	1.000	0.134	HSS TORSIO	7	1.890	2.460	2.460	4.030
23	HSST3X3X0	HSST3X3X0	0.206	1.000	0.206	HSS TORSIO	7	1.890	2.460	2.460	4.030
24	HSST3X3X0	HSST3X3X0	0.359	1.000	0.359	HSS T+SH+F	7	1.890	2.460	2.460	4.030
25	HSST3X3X0	HSST3X3X0	0.234	1.000	0.234	HSS T+SH+F	7	1.890	2.460	2.460	4.030
26	HSST3X3X0	HSST3X3X0	0.028	1.000	0.028	HSS FLEX+A	7	1.890	2.460	2.460	4.030
27	HSST3X3X0	HSST3X3X0	0.027	1.000	0.027	HSS FLEX+A	7	1.890	2.460	2.460	4.030
28	HSST3.5X3.	HSST3.5X3.	0.180	1.000	0.180	HSS BEND Z	7	2.910	5.040	5.040	8.350
29	HSST3.5X3.	HSST3.5X3.	0.565	1.000	0.565	HSS BEND Z	7	2.910	5.040	5.040	8.350
30	HSST3.5X3.	HSST3.5X3.	0.003	1.000	0.003	HSS FLEX+A	7	2.910	5.040	5.040	8.350
31	HSST3.5X3.	HSST3.5X3.	0.003	1.000	0.003	HSS FLEX+A	7	2.910	5.040	5.040	8.350
32	HSST3.5X3.	N/A						2.910	5.040	5.040	8.350
33	HSST3.5X3.	N/A						2.910	5.040	5.040	8.350

Statics Check Results

L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2:DYNO DRUM F	Loads	0	0	-0.313	0	37.584	0
2:DYNO DRUM F	Reactions	-0.000	0.000	0.313	2.518	-37.584	0.000
	Difference	-0.000	0.000	0.000	2.518	-0.000	0.000
1:WEIGHT	Loads	0	-0.692	0	-18.888	0	-83.024
1:WEIGHT	Reactions	-0.000	0.692	0.000	45.663	-0.000	83.024
	Difference	-0.000	0.000	0.000	26.776	-0.000	0.000
10:WIND LOAD C	Loads	0.340	0	0	0	-10.080	-7.260
10:WIND LOAD C	Reactions	-0.340	-0.000	-0.000	-0.000	10.080	7.260
	Difference	0.000	-0.000	-0.000	-0.000	-0.000	-0.000
11:WIND LOAD C	Loads	0	0.920	0	21.360	0	110.400
11:WIND LOAD C	Reactions	0.000	-0.920	-0.000	-60.720	0.000	-110.400
	Difference	0.000	-0.000	-0.000	-39.360	0.000	-0.000



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Statics Check Results Cont...

L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
12:DYNO DRUM	Loads	0.167	0	0	0	-3.999	0
12:DYNO DRUM	Reactions	-0.167	0.000	0.000	0.000	3.999	0.000
	Difference	-0.000	0.000	0.000	0.000	-0.000	0.000
16:WIND RESUL	Loads	0.508	0	0.508	6.709	-74.564	-6.709
16:WIND RESUL	Reactions	-0.508	0.000	-0.508	-4.088	74.564	6.709
	Difference	-0.000	0.000	0.000	2.622	-0.000	0.000
9:COMPRESSIOI	Loads	0	0	0	0	0	0
9:COMPRESSIOI	Reactions	0.000	-0.000	0.000	0.000	-0.000	-0.000
	Difference	0.000	-0.000	0.000	0.000	-0.000	-0.000

Base Pressure Summary

	Node	L/C	FX (psi)	FY (psi)	FZ (psi)
Max FX	12	2:DYNO DRUM	0	0	0
Min FX	12	2:DYNO DRUM	0	0	0
Max FY	12	2:DYNO DRUM	0	0	0
Min FY	12	2:DYNO DRUM	0	0	0
Max FZ	12	2:DYNO DRUM	0	0	0
Min FZ	12	2:DYNO DRUM	0	0	0



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Job Title Pier Analysis

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	2/12/2020		

Project ID	
Project Name	

Structure Type	SPACE FRAME
----------------	-------------

Number of Nodes	26	Highest Node	29
Number of Elements	26	Highest Beam	33
Number of Plates	3	Highest Plate	19

Number of Basic Load Cases	7
Number of Combination Load Cases	9

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	2	DYNO DRUM HO: LIGHT WIND LOAD (Z)
Primary	1	WEIGHT
Primary	10	WIND LOAD ON STRUCTURE (X) DIREC
Primary	11	WIND LOAD ON STRUCTURE (Y) DIREC
Primary	12	DYNO DRUM HO: LIGHT WIND LOAD (X)
Primary	16	WIND RESULTANT
Primary	9	COMPRESSION FORCE
Combination	3	1.1DL+1.0WR
Combination	4	1.25DL
Combination	5	1.1DL+1.0WX
Combination	6	CASE I: VX
Combination	7	1.1DL+1.0WZ
Combination	8	CASE I: VY
Combination	13	CASE III: VY
Combination	14	CASE III: VZ
Combination	15	CASE III: VX



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Nodes

Node	X (ft)	Y (ft)	Z (ft)
2	0	0	-1.000
3	8.000	0	-1.000
4	10.000	0	-1.000
5	12.000	0	-1.000
6	20.000	0	-1.000
7	8.000	0	-3.000
8	0	0	-3.000
9	10.000	0	-3.000
10	12.000	0	-3.000
11	20.000	0	-3.000
12	8.000	0.670	-3.000
14	8.000	5.500	-5.500
15	12.000	0.670	-3.000
17	12.000	5.500	-5.500
18	1.000	0	-1.000
19	1.000	0	-3.000
20	9.500	0	-1.000
21	9.500	0	-3.000
22	10.500	0	-1.000
23	10.500	0	-3.000
24	19.000	0	-1.000
25	19.000	0	-3.000
26	8.000	5.500	-3.000
27	12.000	5.500	-3.000
28	8.000	0	0
29	12.000	0	0

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	2	18	1.000	2	0
2	3	20	1.500	2	0
3	4	22	0.500	2	0
4	5	24	7.000	2	0
5	3	7	2.000	3	0
6	5	10	2.000	3	0
7	8	19	1.000	2	0
8	7	21	1.500	2	0
9	9	23	0.500	2	0
10	10	25	7.000	2	0
11	7	12	0.670	3	0
14	10	15	0.670	3	0
20	18	3	7.000	2	0



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Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
21	19	7	7.000	2	0
22	20	4	0.500	2	0
23	21	9	0.500	2	0
24	22	5	1.500	2	0
25	23	10	1.500	2	0
26	24	6	1.000	2	0
27	25	11	1.000	2	0
28	26	14	2.500	3	0
29	27	17	2.500	3	0
30	3	28	1.000	3	0
31	5	29	1.000	3	0
32	15	27	4.830	3	0
33	12	26	4.830	3	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
17	18	19	8	2	1
18	22	23	21	20	1
19	6	11	25	24	1

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
2	HSST3X3X0.188	1.890	2.460	2.460	3.927	STEEL
3	HSST3.5X3.5X0.25	2.910	5.040	5.040	8.125	STEEL

Plate Thickness

Prop	Node A (in)	Node B (in)	Node C (in)	Node D (in)	Material
1	0.250	0.250	0.250	0.250	STEEL_36_KS



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Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E -6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E -6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E -6
5	A500-GR.B	29E+3	0.300	0.000	6E -6
6	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
7	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
8	STEEL	29E+3	0.300	0.000283	6E -6
9	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
12	Fixed	-	Fixed	-	-	-
14	-	Fixed	-	-	-	-
15	Fixed	-	Fixed	-	-	-
17	-	Fixed	-	-	-	-

Releases

There is no data of this type.

Primary Load Cases

Number	Name	Type
2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	Wind
1	WEIGHT	Dead
10	WIND LOAD ON STRUCTURE (X) DIREC	Wind
11	WIND LOAD ON STRUCTURE (Y) DIREC	Wind
12	DYNO DRUM HO: LIGHT WIND LOAD (X)	Wind
16	WIND RESULTANT	Wind
9	COMPRESSION FORCE	Dead



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Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
3	1.1DL+1.0WR	1	WEIGHT	1.10
		16	WIND RESULTANT	1.00
4	1.25DL	1	WEIGHT	1.25
5	1.1DL+1.0WX	1	WEIGHT	1.10
		12	DYNO DRUM HO: LIGHT WIND LOAD (X)	1.00
		10	WIND LOAD ON STRUCTURE (X) DIREC	1.00
6	CASE I: VX	10	WIND LOAD ON STRUCTURE (X) DIREC	1.00
7	1.1DL+1.0WZ	2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	1.00
		1	WEIGHT	1.10
8	CASE I: VY	1	WEIGHT	1.00
13	CASE III: VY	1	WEIGHT	0.75
14	CASE III: VZ	2	DYNO DRUM HO: LIGHT WIND LOAD (Z)	0.75
15	CASE III: VX	12	DYNO DRUM HO: LIGHT WIND LOAD (X)	0.75
		10	WIND LOAD ON STRUCTURE (X) DIREC	0.75

Load Generators

There is no data of this type.

1 WEIGHT : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	-	-0.0261	-	-	-	-
4	-	-0.0261	-	-	-	-
6	-	-0.0261	-	-	-	-
8	-	-0.0261	-	-	-	-
9	-	-0.0261	-	-	-	-
11	-	-0.0261	-	-	-	-

1 WEIGHT : Selfweight

Direction	Factor	Assigned Geometry
Y	-1.000	ALL



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2 DYNO DRUM HO: LIGHT WIND LOAD (Z) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	-	-	-0.0522	-	-	-
4	-	-	-0.0522	-	-	-
6	-	-	-0.0522	-	-	-
8	-	-	-0.0522	-	-	-
9	-	-	-0.0522	-	-	-
11	-	-	-0.0522	-	-	-

9 COMPRESSION FORCE : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
14	-	-	3.000	-	-	-
17	-	-	3.000	-	-	-
26	-	-	-3.000	-	-	-
27	-	-	-3.000	-	-	-

10 WIND LOAD ON STRUCTURE (X) DIRECTION : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
5	UNI lbf/ft	GX	20.000	0	-	2.000	-
6	UNI lbf/ft	GX	20.000	0	-	2.000	-
11	UNI lbf/ft	GX	20.000	0	-	0.670	-
14	UNI lbf/ft	GX	20.000	0	-	0.670	-
30	UNI lbf/ft	GX	20.000	0	-	1.000	-
31	UNI lbf/ft	GX	20.000	0	-	1.000	-
32	UNI lbf/ft	GX	20.000	0	-	4.830	-
33	UNI lbf/ft	GX	20.000	0	-	4.830	-



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11 WIND LOAD ON STRUCTURE (Y) DIRECTION : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)	
1	UNI	lbf/ft	GY	20.000	0	-	1.000	-
2	UNI	lbf/ft	GY	20.000	0	-	1.500	-
3	UNI	lbf/ft	GY	20.000	0	-	0.500	-
4	UNI	lbf/ft	GY	20.000	0	-	7.000	-
5	UNI	lbf/ft	GY	20.000	0	-	2.000	-
6	UNI	lbf/ft	GY	20.000	0	-	2.000	-
7	UNI	lbf/ft	GY	20.000	0	-	1.000	-
8	UNI	lbf/ft	GY	20.000	0	-	1.500	-
9	UNI	lbf/ft	GY	20.000	0	-	0.500	-
10	UNI	lbf/ft	GY	20.000	0	-	7.000	-
20	UNI	lbf/ft	GY	20.000	0	-	7.000	-
21	UNI	lbf/ft	GY	20.000	0	-	7.000	-
22	UNI	lbf/ft	GY	20.000	0	-	0.500	-
23	UNI	lbf/ft	GY	20.000	0	-	0.500	-
24	UNI	lbf/ft	GY	20.000	0	-	1.500	-
25	UNI	lbf/ft	GY	20.000	0	-	1.500	-
26	UNI	lbf/ft	GY	20.000	0	-	1.000	-
27	UNI	lbf/ft	GY	20.000	0	-	1.000	-
30	UNI	lbf/ft	GY	20.000	0	-	1.000	-
31	UNI	lbf/ft	GY	20.000	0	-	1.000	-

12 DYNO DRUM HO: LIGHT WIND LOAD (X) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	0.02777	-	-	-	-	-
4	0.02777	-	-	-	-	-
8	0.02777	-	-	-	-	-
9	0.02777	-	-	-	-	-
24	0.02777	-	-	-	-	-
25	0.02777	-	-	-	-	-



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16 WIND RESULTANT : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
2	0.0295	-	-	-	-	-
3	0.042	-	-	-	-	-
5	0.042	-	-	-	-	-
8	0.0295	-	-	-	-	-
12	0.155	-	-	-	-	-
15	0.155	-	-	-	-	-
20	0.0295	-	-	-	-	-
21	0.0295	-	-	-	-	-
24	0.0295	-	-	-	-	-
25	0.0295	-	-	-	-	-
26	0.053	-	-	-	-	-
27	0.053	-	-	-	-	-
28	0.021	-	-	-	-	-
29	0.021	-	-	-	-	-

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6	-21.8E+3	0.002	-0.020
Min X	26	4:1.25DL	-0.962	-556E+3	1.07E+6	1.21E+6	18.5E+3	-0.001	0.017
Max Y	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6	-21.8E+3	0.002	-0.022
Min Y	28	4:1.25DL	0.086	-1.22E+6	-149E+3	1.23E+6	18.5E+3	-0.001	0.018909
Max Z	14	4:1.25DL	-0.923	0	1.07E+6	1.07E+6	18.5E+3	-0.001	0.017
Min Z	14	11:WIND LOA	1.085	0	-1.26E+6	1.26E+6	-21.8E+3	0.002	-0.020
Max rX	14	4:1.25DL	-0.923	0	1.07E+6	1.07E+6	18.5E+3	-0.001	0.017
Min rX	14	11:WIND LOA	1.085	0	-1.26E+6	1.26E+6	-21.8E+3	0.002	-0.020
Max rY	3	11:WIND LOA	-0.120	1.18E+6	175E+3	1.19E+6	-21.8E+3	0.002	-0.022
Min rY	19	7:1.1DL+1.0W	0.128	-531E+3	-142E+3	549E+3	17.7E+3	-0.001	0.021
Max rZ	8	4:1.25DL	0.134	-556E+3	-149E+3	575E+3	18.5E+3	-0.001	0.022
Min rZ	8	11:WIND LOA	-0.157	653E+3	175E+3	676E+3	-21.8E+3	0.002	-0.025
Max Rst	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6	-21.8E+3	0.002	-0.022



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Beam Displacement Detail Summary

Displacements shown in *italic* indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	28	11:WIND LOA	0	1.131	653E+3	-1.26E+6	1.42E+6
Min X	28	4:1.25DL	0	-0.962	-556E+3	1.07E+6	1.21E+6
Max Y	30	11:WIND LOA	1.000	-0.102	1.44E+6	175E+3	1.45E+6
Min Y	30	4:1.25DL	1.000	0.086	-1.22E+6	-149E+3	1.23E+6
Max Z	28	4:1.25DL	0	-0.962	-556E+3	1.07E+6	1.21E+6
Min Z	28	11:WIND LOA	0	1.131	653E+3	-1.26E+6	1.42E+6
Max Rst	30	11:WIND LOA	1.000	-0.102	1.44E+6	175E+3	1.45E+6

Beam Maximum Relative Displacements

Distances to maxima are given from beam end A.

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
1	2	1.000	2:DYNO DRUM	0.004	0.250	0.000	0.500	0.004	0.250	3072
			1:WEIGHT	-0.03125	0.167	0.004	0.250	0.031	0.167	384
			10:WIND LOA	0.000	0.833	-0.000	0.500	0.000	0.500	> 10000
			11:WIND LOA	0.0625	0.250	0.008	0.500	0.062622	0.250	192
			12:DYNO DRU	0.000	0.167	-0.000	0.667	0.000	0.667	> 10000
			16:WIND RES	0.004	0.500	-0.000	0.250	0.004	0.500	3072
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0W	-0.03125	0.167	0.008	0.500	0.032	0.500	384
			4:1.25DL	-0.021	0.083	0.008	0.500	0.022	0.417	576
			5:1.1DL+1.0W	0.03125	0.167	-0.004	0.500	0.031	0.500	384
			6:CASE I: VX	0.000	0.833	-0.000	0.500	0.000	0.500	> 10000
			7:1.1DL+1.0W	-0.021	0.083	0	0	0.021	0.083	576
			8:CASE I: VY	-0.03125	0.167	0.004	0.250	0.031	0.167	384
			13:CASE III: V	-0.03125	0.250	0.004	0.500	0.031311	0.250	384
			14:CASE III: V	-0.002	0.167	0.000	0.500	0.002	0.500	6144
15:CASE III:VX	0.000	0.750	-0.000	0.417	0.000	0.417	> 10000			
2	3	1.500	2:DYNO DRUM	-0.004	0.250	-0.000	0.250	0.004	1.250	4608
			1:WEIGHT	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			10:WIND LOA	0.000	0.625	-0.000	0.375	0.000	0.625	> 10000
			11:WIND LOA	0.0625	0.250	-0.008	0.375	0.063	0.250	288
			12:DYNO DRU	-0.000	0.625	-0.000	0.375	0.000	0.500	> 10000
			16:WIND RES	-0.004	0.375	0.000	0.375	0.004	0.375	4608
			9:COMPRESS	0	0	0	0	0.000	1.375	
			3:1.1DL+1.0W	-0.021	0.125	-0.008	0.750	0.022	0.625	864
			4:1.25DL	-0.03125	0.125	0.008	0.375	0.032	0.375	576
			5:1.1DL+1.0W	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			6:CASE I: VX	0.000	0.625	-0.000	0.375	0.000	0.625	> 10000
			7:1.1DL+1.0W	0.03125	0.750	0.008	0.375	0.03125	0.750	576
			8:CASE I: VY	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			13:CASE III: V	-0.021	0.125	-0.004	0.375	0.021	0.250	864
			14:CASE III: V	-0.002	0.750	0.000	0.750	0.002	0.750	9216



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			15:CASE III:Vx	0.000	0.625	-0.000	0.375	0.000	0.625	> 10000
3	4	0.500	2:DYNO DRUM	-0.004	0.250	0.000	0.250	0.004	0.250	1536
			1:WEIGHT	0.03125	0.125	0	0	0.03125	0.125	192
			10:WIND LOA	-0.000	0.292	-0.000	0.250	0.000	0.250	> 10000
			11:WIND LOA	0.0625	0.250	0	0	0.0625	0.250	96
			12:DYNO DRU	0.000	0.292	-0.000	0.250	0.000	0.375	> 10000
			16:WIND RES	0	0	0	0	0.000	0.208	
			9:COMPRESS	0	0	0	0	0.000	0.458	
			3:1.1DL+1.0W	0.03125	0.250	0	0	0.03125	0.250	192
			4:1.25DL	0.03125	0.125	0.008	0.250	0.031	0.125	192
			5:1.1DL+1.0W	0.03125	0.125	0.004	0.250	0.031311	0.125	192
			6:CASE I: VX	-0.000	0.292	-0.000	0.250	0.000	0.250	> 10000
			7:1.1DL+1.0W	-0.03125	0.250	0.008	0.250	0.032	0.250	192
			8:CASE I: VY	0.03125	0.125	0	0	0.03125	0.125	192
			13:CASE III: V	-0.03125	0.250	0	0	0.03125	0.250	192
			14:CASE III: V	0.002	0.125	0	0	0.002	0.125	3072
			15:CASE III:Vx	-0.000	0.292	-0.000	0.333	0.000	0.333	> 10000
4	5	7.000	2:DYNO DRUM	0.004	1.750	0.004	1.750	0.006	1.750	> 10000
			1:WEIGHT	0.094	3.500	-0.004	3.500	0.094	3.500	896
			10:WIND LOA	-0.001	2.917	0.000	3.500	0.001	2.917	> 10000
			11:WIND LOA	0	0	-0.005	0.583	0.005	4.667	
			12:DYNO DRU	0.000	2.917	0.000	3.500	0.000	2.917	> 10000
			16:WIND RES	-0.003	0.583	-0.001	2.333	0.003	2.333	> 10000
			9:COMPRESS	0	0	0	0	0.000	6.417	
			3:1.1DL+1.0W	0.094	3.500	-0.008	3.500	0.094	3.500	896
			4:1.25DL	0.083	4.667	-0.008	3.500	0.083	4.667	1008
			5:1.1DL+1.0W	0.0625	1.750	0.003	0.583	0.063	2.333	1344
			6:CASE I: VX	-0.001	2.917	0.000	3.500	0.001	2.917	> 10000
			7:1.1DL+1.0W	0.094	1.750	-0.005	0.583	0.094	2.917	896
			8:CASE I: VY	0.094	3.500	-0.004	3.500	0.094	3.500	896
			13:CASE III: V	0.03125	3.500	0.003	0.583	0.03125	3.500	2688
			14:CASE III: V	-0.002	1.167	0.003	1.750	0.003	1.167	> 10000
			15:CASE III:Vx	-0.001	2.917	0.000	3.500	0.001	2.917	> 10000
5	3	2.000	2:DYNO DRUM	0.003	0.167	0.000	0.333	0.003	0.167	8192
			1:WEIGHT	-0.03125	0.500	0.000	0.833	0.03125	1.500	768
			10:WIND LOA	0.001	1.000	0.000	0.500	0.001	1.000	> 10000
			11:WIND LOA	0.052	0.333	-0.000	1.500	0.052	0.333	461
			12:DYNO DRU	-0.000	1.000	0.000	0.333	0.000	1.000	> 10000
			16:WIND RES	0.004	1.167	-0.000	0.500	0.004	1.167	6703
			9:COMPRESS	0	0	0	0	0.000	1.833	
			3:1.1DL+1.0W	-0.03125	0.167	-0.000	0.500	0.03125	0.500	768
			4:1.25DL	-0.03125	1.000	0.000	1.000	0.03125	1.000	768
			5:1.1DL+1.0W	0.046875	1.167	0.000	0.667	0.046875	1.167	512
			6:CASE I: VX	0.001	1.000	0.000	0.500	0.001	1.000	> 10000
			7:1.1DL+1.0W	0.052	1.833	0.000	0.500	0.052	1.833	461



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			8:CASE I: VY	-0.03125	0.500	0.000	0.833	0.03125	1.500	768
			13:CASE III: V'	0.021	0.167	0.000	1.167	0.021	1.167	1152
			14:CASE III: V _i	0.003	1.167	0.000	0.500	0.003	1.167	8674
			15:CASE III:VX	0.000	1.000	0.000	0.333	0.000	1.000	> 10000
6	5	2.000	2:DYNO DRUM	0.003	0.167	-0.000	0.500	0.003	0.167	7373
			1:WEIGHT	-0.03125	0.333	-0.000	1.667	0.03125	1.000	768
			10:WIND LOA	-0.001	1.000	0.000	1.000	0.001	1.000	> 10000
			11:WIND LOA	-0.047	0.833	0.000	0.667	0.046875	0.833	512
			12:DYNO DRU	0.000	1.000	0.000	0.167	0.000	1.000	> 10000
			16:WIND RES	0.003	0.667	-0.000	1.667	0.003	0.667	9216
			9:COMPRESS	0	0	0	0	0.000	1.833	
			3:1.1DL+1.0W	-0.021	0.167	-0.000	1.667	0.021	1.667	1152
			4:1.25DL	0.052	1.667	-0.000	1.333	0.052	1.667	461
			5:1.1DL+1.0W	-0.03125	0.167	-0.000	1.667	0.03125	1.500	768
			6:CASE I: VX	-0.001	1.000	0.000	1.000	0.001	1.000	> 10000
			7:1.1DL+1.0W	0.046875	1.833	-0.000	0.500	0.046875	1.833	512
			8:CASE I: VY	-0.03125	0.333	-0.000	1.667	0.03125	1.000	768
			13:CASE III: V'	0.029	0.167	-0.000	1.500	0.029	0.167	838
			14:CASE III: V _i	0.003	1.167	0.000	1.667	0.003	1.167	7022
			15:CASE III:VX	-0.000	1.000	-0.000	1.667	0.000	1.000	> 10000
7	8	1.000	2:DYNO DRUM	-0.001	0.083	0.000	0.500	0.001	0.417	9216
			1:WEIGHT	-0.016	0.083	0.004	0.250	0.016	0.250	768
			10:WIND LOA	-0.000	0.667	-0.000	0.167	0.000	0.500	> 10000
			11:WIND LOA	-0.03125	0.500	0.008	0.500	0.032	0.500	384
			12:DYNO DRU	0.000	0.583	-0.000	0.250	0.000	0.750	> 10000
			16:WIND RES	-0.002	0.250	-0.000	0.250	0.002	0.750	6144
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0W	-0.03125	0.167	0.008	0.500	0.032	0.500	384
			4:1.25DL	0.03125	0.500	0.008	0.500	0.032	0.500	384
			5:1.1DL+1.0W	-0.016	0.500	-0.004	0.500	0.016	0.500	768
			6:CASE I: VX	-0.000	0.667	-0.000	0.167	0.000	0.500	> 10000
			7:1.1DL+1.0W	-0.021	0.083	0	0	0.021	0.083	576
			8:CASE I: VY	-0.016	0.083	0.004	0.250	0.016	0.250	768
			13:CASE III: V'	-0.016	0.500	0.004	0.500	0.016	0.500	768
			14:CASE III: V _i	0.001	0.083	0.000	0.500	0.001	0.417	> 10000
			15:CASE III:VX	-0.000	0.583	0.000	0.750	0.000	0.750	> 10000
8	7	1.500	2:DYNO DRUM	0.002	0.125	-0.000	0.250	0.002	0.625	9216
			1:WEIGHT	0.010	0.125	-0.004	0.250	0.011125	0.250	1728
			10:WIND LOA	-0.001	0.625	-0.000	0.250	0.001	0.625	> 10000
			11:WIND LOA	-0.03125	0.750	-0.008	0.375	0.03125	0.750	576
			12:DYNO DRU	0.000	0.625	-0.000	0.250	0.000	0.625	> 10000
			16:WIND RES	-0.002	0.250	0.000	0.375	0.002	1.250	9216
			9:COMPRESS	0	0	0	0	0.000	1.375	
			3:1.1DL+1.0W	-0.021	0.125	-0.008	0.750	0.022	0.625	864
			4:1.25DL	0.03125	0.750	0.008	0.375	0.03125	0.750	576



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			5:1.1DL+1.0W	0.015625	0.750	-0.004	0.250	0.016	0.750	1152
			6:CASE I: VX	-0.001	0.625	-0.000	0.250	0.001	0.625	> 10000
			7:1.1DL+1.0W	0.03125	0.750	0.008	0.375	0.03125	0.750	576
			8:CASE I: VY	0.010	0.125	-0.004	0.250	0.011125	0.250	1728
			13:CASE III: V	-0.016	0.125	-0.004	0.375	0.016	1.125	1152
			14:CASE III: V	0.001	0.125	0.000	0.750	0.001	0.625	> 10000
			15:CASE III: VX	-0.001	0.625	-0.000	0.375	0.001	0.625	> 10000
9	9	0.500	2:DYNO DRUM	0.002	0.250	0.000	0.250	0.002	0.250	3072
			1:WEIGHT	-0.016	0.083	0	0	0.015625	0.083	384
			10:WIND LOA	0.000	0.292	-0.000	0.250	0.000	0.292	> 10000
			11:WIND LOA	0.03125	0.125	0	0	0.03125	0.125	192
			12:DYNO DRU	-0.000	0.292	-0.000	0.167	0.000	0.250	> 10000
			16:WIND RESI	0	0	0	0	0.000	0.250	
			9:COMPRESSI	0	0	0	0	0.000	0.458	
			3:1.1DL+1.0W	-0.03125	0.250	0	0	0.03125	0.250	192
			4:1.25DL	0.03125	0.125	0.008	0.250	0.031	0.125	192
			5:1.1DL+1.0W	0.015625	0.083	0.004	0.250	0.016	0.250	384
			6:CASE I: VX	0.000	0.292	-0.000	0.250	0.000	0.292	> 10000
			7:1.1DL+1.0W	0.03125	0.250	0.008	0.250	0.032	0.250	192
			8:CASE I: VY	-0.016	0.083	0	0	0.015625	0.083	384
			13:CASE III: V	-0.016	0.250	0	0	0.015625	0.250	384
			14:CASE III: V	-0.001	0.083	0	0	0.001	0.083	6144
			15:CASE III: VX	0.000	0.292	-0.000	0.208	0.000	0.208	> 10000
10	10	7.000	2:DYNO DRUM	-0.002	1.167	0.004	1.750	0.005	1.167	> 10000
			1:WEIGHT	0.046875	3.500	-0.004	3.500	0.047	3.500	1792
			10:WIND LOA	0.001	2.917	0.000	3.500	0.001	2.917	> 10000
			11:WIND LOA	0.03125	3.500	-0.005	0.583	0.03125	3.500	2688
			12:DYNO DRU	-0.000	2.917	0.000	3.500	0.000	3.500	> 10000
			16:WIND RESI	0.001	0.583	-0.001	2.333	0.002	4.667	> 10000
			9:COMPRESSI	0	0	0	0	0.000	6.417	
			3:1.1DL+1.0W	0.094	3.500	-0.008	3.500	0.094	3.500	896
			4:1.25DL	0.094	3.500	-0.008	3.500	0.094	3.500	896
			5:1.1DL+1.0W	0.046875	1.750	0.003	0.583	0.046875	1.750	1792
			6:CASE I: VX	0.001	2.917	0.000	3.500	0.001	2.917	> 10000
			7:1.1DL+1.0W	0.094	2.917	-0.005	0.583	0.094	2.917	896
			8:CASE I: VY	0.046875	3.500	-0.004	3.500	0.047	3.500	1792
			13:CASE III: V	0.046875	1.750	0.003	0.583	0.046875	1.750	1792
			14:CASE III: V	0.001	3.500	0.003	1.750	0.003	1.750	> 10000
			15:CASE III: VX	0.001	2.917	0.000	3.500	0.001	2.917	> 10000
11	7	0.670	2:DYNO DRUM	0	0	0.001	0.391	0.004	0.502	
			1:WEIGHT	0.000	0.279	0.005	0.112	0.032	0.447	> 10000
			10:WIND LOA	0.000	0.279	0.000	0.335	0.000	0.335	> 10000
			11:WIND LOA	-0.000	0.279	-0.007	0.391	0.063	0.502	> 10000
			12:DYNO DRU	-0.000	0.167	-0.000	0.391	0.000	0.391	> 10000
			16:WIND RESI	0.000	0.391	0.000	0.391	0.004	0.502	> 10000



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Client THEA

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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			9:COMPRESSI	0	0	0	0	0.000	0.502	
			3:1.1DL+1.0W	0.000	0.279	0.005	0.112	0.063	0.558	> 10000
			4:1.25DL	0.000	0.279	0.009	0.391	0.063	0.558	> 10000
			5:1.1DL+1.0W	0.000	0.335	0.008	0.279	0.031	0.335	> 10000
			6:CASE I: VX	0.000	0.279	0.000	0.335	0.000	0.335	> 10000
			7:1.1DL+1.0W	0.000	0.279	0.008	0.558	0.063	0.558	> 10000
			8:CASE I: VY	0.000	0.279	0.005	0.112	0.032	0.447	> 10000
			13:CASE III: V	0.000	0.279	-0.004	0.056	0.031	0.335	> 10000
			14:CASE III: V	-0.000	0.112	0.000	0.391	0.000	0.391	> 10000
			15:CASE III:VX	0.000	0.335	0.000	0.391	0.000	0.335	> 10000
14	10	0.670	2:DYNO DRUM	-0.000	0.335	0.001	0.558	0.004	0.614	> 10000
			1:WEIGHT	-0.000	0.279	0.005	0.223	0.031	0.447	> 10000
			10:WIND LOA	0.000	0.279	-0.000	0.335	0.000	0.335	> 10000
			11:WIND LOA	0.000	0.335	-0.010	0.614	0.063	0.558	> 10000
			12:DYNO DRU	-0.000	0.112	0.000	0.335	0.000	0.335	> 10000
			16:WIND RES	0.000	0.279	0.001	0.558	0.004	0.614	> 10000
			9:COMPRESSI	0	0	0	0	0.000	0.502	
			3:1.1DL+1.0W	-0.000	0.279	0.007	0.391	0.062622	0.502	> 10000
			4:1.25DL	-0.000	0.223	0.007	0.391	0.063	0.502	> 10000
			5:1.1DL+1.0W	-0.000	0.223	0.008	0.391	0.032	0.447	> 10000
			6:CASE I: VX	0.000	0.279	-0.000	0.335	0.000	0.335	> 10000
			7:1.1DL+1.0W	-0.000	0.279	0.009	0.391	0.063	0.558	> 10000
			8:CASE I: VY	-0.000	0.279	0.005	0.223	0.031	0.447	> 10000
			13:CASE III: V	-0.000	0.223	0.003	0.391	0.031	0.447	> 10000
			14:CASE III: V	0.000	0.335	0.000	0.112	0.000	0.614	> 10000
			15:CASE III:VX	0.000	0.391	-0.000	0.391	0.000	0.391	> 10000
20	18	7.000	2:DYNO DRUM	0.004	1.167	0.004	5.833	0.006	5.833	> 10000
			1:WEIGHT	-0.03125	3.500	-0.004	3.500	0.031	3.500	2688
			10:WIND LOA	0.001	4.083	-0.000	3.500	0.001	4.083	> 10000
			11:WIND LOA	0.042	0.583	-0.005	0.583	0.042	0.583	2016
			12:DYNO DRU	-0.000	4.083	-0.000	3.500	0.000	4.083	> 10000
			16:WIND RES	-0.003	0.583	-0.002	5.250	0.003	5.833	> 10000
			9:COMPRESSI	0	0	0	0	0.000	4.083	
			3:1.1DL+1.0W	0	0	-0.005	0.583	0.005	4.083	
			4:1.25DL	-0.021	0.583	0.008	3.500	0.022	0.583	4032
			5:1.1DL+1.0W	0.03125	1.167	-0.004	1.167	0.031	1.167	2688
			6:CASE I: VX	0.001	4.083	-0.000	3.500	0.001	4.083	> 10000
			7:1.1DL+1.0W	-0.03125	1.167	0.008	1.750	0.032	1.167	2688
			8:CASE I: VY	-0.03125	3.500	-0.004	3.500	0.031	3.500	2688
			13:CASE III: V	-0.03125	3.500	0.003	0.583	0.03125	3.500	2688
			14:CASE III: V	-0.002	1.167	0.003	5.250	0.003	5.833	> 10000
			15:CASE III:VX	0.001	4.083	-0.000	3.500	0.001	4.083	> 10000
21	19	7.000	2:DYNO DRUM	-0.001	0.583	0.004	5.833	0.004	5.833	> 10000
			1:WEIGHT	0.042	2.333	-0.004	3.500	0.042	4.083	2016
			10:WIND LOA	-0.001	4.083	-0.000	3.500	0.001	4.083	> 10000



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			11:WIND LOA	-0.083	4.667	-0.005	0.583	0.083	4.667	1008
			12:DYNO DRU	0.000	4.083	-0.000	3.500	0.000	3.500	> 10000
			16:WIND RES	0.001	0.583	-0.002	5.250	0.002	5.833	> 10000
			9:COMPRESS	0	0	0	0	0.000	4.083	
			3:1.1DL+1.0W	0.0625	2.333	-0.005	0.583	0.063	2.333	1344
			4:1.25DL	0.094	5.833	0.008	3.500	0.094	5.833	896
			5:1.1DL+1.0W	0.078125	4.083	-0.004	1.167	0.078	4.083	1075
			6:CASE I: VX	-0.001	4.083	-0.000	3.500	0.001	4.083	> 10000
			7:1.1DL+1.0W	0.083	2.333	0.008	1.750	0.083	2.333	1008
			8:CASE I: VY	0.042	2.333	-0.004	3.500	0.042	4.083	2016
			13:CASE III: V	0.046875	5.833	0.003	0.583	0.047	5.833	1792
			14:CASE III: V	-0.001	0.583	0.003	5.250	0.003	5.250	> 10000
			15:CASE III:VX	-0.001	4.083	-0.000	3.500	0.001	4.083	> 10000
22	20	0.500	2:DYNO DRUM	0.004	0.250	0	0	0.004	0.250	1536
			1:WEIGHT	-0.03125	0.250	0.004	0.250	0.031	0.250	192
			10:WIND LOA	0.000	0.208	0.000	0.208	0.000	0.208	> 10000
			11:WIND LOA	-0.0625	0.250	-0.008	0.250	0.063	0.250	96
			12:DYNO DRU	-0.000	0.208	0.000	0.208	0.000	0.333	> 10000
			16:WIND RES	-0.004	0.250	0.000	0.250	0.004	0.250	1536
			9:COMPRESS	0	0	0	0	0.000	0.458	
			3:1.1DL+1.0W	0.03125	0.125	0.008	0.250	0.031	0.125	192
			4:1.25DL	-0.03125	0.250	0	0	0.03125	0.250	192
			5:1.1DL+1.0W	0.03125	0.125	0	0	0.03125	0.125	192
			6:CASE I: VX	0.000	0.208	0.000	0.208	0.000	0.208	> 10000
			7:1.1DL+1.0W	-0.03125	0.125	0	0	0.03125	0.125	192
			8:CASE I: VY	-0.03125	0.250	0.004	0.250	0.031	0.250	192
			13:CASE III: V	0.03125	0.250	-0.004	0.250	0.031	0.250	192
			14:CASE III: V	0.002	0.125	-0.000	0.250	0.002	0.125	3072
			15:CASE III:VX	0.000	0.208	0.000	0.167	0.000	0.167	> 10000
23	21	0.500	2:DYNO DRUM	0.002	0.125	0	0	0.002	0.125	3072
			1:WEIGHT	-0.016	0.125	0.004	0.250	0.016	0.125	384
			10:WIND LOA	-0.000	0.208	0.000	0.208	0.000	0.208	> 10000
			11:WIND LOA	0.03125	0.125	-0.008	0.250	0.031	0.125	192
			12:DYNO DRU	0.000	0.208	0.000	0.417	0.000	0.125	> 10000
			16:WIND RES	0.002	0.250	0.000	0.250	0.002	0.250	3072
			9:COMPRESS	0	0	0	0	0.000	0.458	
			3:1.1DL+1.0W	0.03125	0.250	0.008	0.250	0.032	0.250	192
			4:1.25DL	-0.03125	0.250	0	0	0.03125	0.250	192
			5:1.1DL+1.0W	0.015625	0.125	0	0	0.015625	0.125	384
			6:CASE I: VX	-0.000	0.208	0.000	0.208	0.000	0.208	> 10000
			7:1.1DL+1.0W	-0.03125	0.250	0	0	0.03125	0.250	192
			8:CASE I: VY	-0.016	0.125	0.004	0.250	0.016	0.125	384
			13:CASE III: V	-0.016	0.125	-0.004	0.250	0.016	0.125	384
			14:CASE III: V	0.001	0.083	-0.000	0.250	0.001	0.250	6144
			15:CASE III:VX	-0.000	0.208	0.000	0.250	0.000	0.250	> 10000



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
24	22	1.500	2:DYNO DRUM	0.004	0.250	-0.000	0.750	0.004	0.750	4608
			1:WEIGHT	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			10:WIND LOA	-0.000	0.875	0.000	1.125	0.000	0.875	> 10000
			11:WIND LOA	-0.0625	0.250	0.008	0.375	0.063	0.250	288
			12:DYNO DRU	0.000	0.875	0.000	1.125	0.000	1.000	> 10000
			16:WIND RES	0.004	0.375	-0.000	0.375	0.004	1.125	4608
			9:COMPRESS	0	0	0	0	0.000	1.375	
			3:1.1DL+1.0W	-0.03125	0.750	-0.008	0.750	0.032	0.750	576
			4:1.25DL	0.03125	0.750	-0.008	0.750	0.032	0.750	576
			5:1.1DL+1.0W	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			6:CASE I: VX	-0.000	0.875	0.000	1.125	0.000	0.875	> 10000
			7:1.1DL+1.0W	0.03125	0.750	-0.008	0.750	0.032	0.750	576
			8:CASE I: VY	-0.021	0.125	-0.004	0.250	0.021	0.250	864
			13:CASE III: V	0.03125	0.250	0.004	0.375	0.031	0.250	576
			14:CASE III: V	-0.001	0.125	0.000	0.750	0.001	0.625	> 10000
15:CASE III:VX	-0.000	0.875	0.000	1.125	0.000	0.875	> 10000			
25	23	1.500	2:DYNO DRUM	-0.002	0.125	-0.000	0.750	0.002	0.625	9216
			1:WEIGHT	-0.016	0.750	-0.004	0.250	0.016	0.750	1152
			10:WIND LOA	0.001	0.875	0.000	1.000	0.001	0.875	> 10000
			11:WIND LOA	0.03125	0.750	0.008	0.375	0.03125	0.750	576
			12:DYNO DRU	-0.000	0.875	0.000	1.250	0.000	0.875	> 10000
			16:WIND RES	-0.002	0.250	-0.000	0.375	0.002	0.250	9216
			9:COMPRESS	0	0	0	0	0.000	1.375	
			3:1.1DL+1.0W	-0.021	0.125	-0.008	0.750	0.022	0.625	864
			4:1.25DL	-0.021	0.125	-0.008	0.750	0.022	0.625	864
			5:1.1DL+1.0W	-0.016	0.125	-0.004	0.250	0.016	0.125	1152
			6:CASE I: VX	0.001	0.875	0.000	1.000	0.001	0.875	> 10000
			7:1.1DL+1.0W	-0.03125	0.750	-0.008	0.750	0.032	0.750	576
			8:CASE I: VY	-0.016	0.750	-0.004	0.250	0.016	0.750	1152
			13:CASE III: V	0.015625	0.125	0.004	0.375	0.016	0.375	1152
			14:CASE III: V	0.001	0.125	0.000	0.750	0.001	0.625	> 10000
15:CASE III:VX	0.001	0.875	0.000	1.125	0.001	0.875	> 10000			
26	24	1.000	2:DYNO DRUM	-0.004	0.250	-0.000	0.500	0.004	0.750	3072
			1:WEIGHT	-0.03125	0.250	-0.004	0.500	0.031311	0.250	384
			10:WIND LOA	-0.000	0.167	-0.000	0.500	0.000	0.500	> 10000
			11:WIND LOA	0.0625	0.500	0.008	0.500	0.063	0.500	192
			12:DYNO DRU	-0.000	0.667	0.000	0.500	0.000	0.917	> 10000
			16:WIND RES	0.004	0.500	0.000	0.250	0.004	0.500	3072
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0W	-0.03125	0.250	-0.008	0.500	0.031	0.250	384
			4:1.25DL	0.03125	0.250	-0.008	0.500	0.031	0.250	384
			5:1.1DL+1.0W	0.03125	0.250	0.004	0.250	0.031	0.250	384
			6:CASE I: VX	-0.000	0.167	-0.000	0.500	0.000	0.500	> 10000
			7:1.1DL+1.0W	-0.03125	0.167	0.008	0.500	0.032	0.500	384
			8:CASE I: VY	-0.03125	0.250	-0.004	0.500	0.031311	0.250	384



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			13:CASE III: V'	0.03125	0.500	0.004	0.500	0.031	0.500	384
			14:CASE III: V _i	-0.002	0.167	-0.000	0.500	0.002	0.500	6144
			15:CASE III:V _x	-0.000	0.167	0.000	0.417	0.000	0.417	> 10000
27	25	1.000	2:DYNO DRUM	-0.001	0.083	-0.000	0.500	0.001	0.417	9216
			1:WEIGHT	-0.010	0.083	-0.004	0.500	0.011	0.417	1152
			10:WIND LOA	0.000	0.417	-0.000	0.167	0.000	0.500	> 10000
			11:WIND LOA	0.03125	0.167	0.008	0.500	0.032	0.500	384
			12:DYNO DRU	-0.000	0.417	0.000	0.917	0.000	0.917	> 10000
			16:WIND RES	0.002	0.250	0.000	0.250	0.002	0.750	6144
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0W	-0.03125	0.250	-0.008	0.500	0.031	0.250	384
			4:1.25DL	-0.03125	0.250	-0.008	0.500	0.031	0.250	384
			5:1.1DL+1.0W	-0.016	0.167	0.004	0.250	0.016	0.167	768
			6:CASE I: VX	0.000	0.417	-0.000	0.167	0.000	0.500	> 10000
			7:1.1DL+1.0W	0.03125	0.250	0.008	0.500	0.031	0.250	384
			8:CASE I: VY	-0.010	0.083	-0.004	0.500	0.011	0.417	1152
			13:CASE III: V'	0.015625	0.167	0.004	0.500	0.016	0.500	768
			14:CASE III: V _i	-0.001	0.083	-0.000	0.500	0.001	0.583	> 10000
			15:CASE III:V _x	0.000	0.417	0.000	0.750	0.000	0.750	> 10000
28	26	2.500	2:DYNO DRUM	-0.002	0.417	0.000	1.875	0.002	0.417	> 10000
			1:WEIGHT	0.021	0.417	0	0	0.021	0.417	1440
			10:WIND LOA	0.001	1.042	0.000	2.083	0.001	1.042	> 10000
			11:WIND LOA	-0.03125	0.417	-0.000	2.292	0.03125	0.417	960
			12:DYNO DRU	-0.000	1.042	-0.000	0.208	0.000	1.042	> 10000
			16:WIND RES	0.002	2.083	-0.000	1.458	0.002	2.083	> 10000
			9:COMPRESS	0	0	0	0	0.000	1.458	
			3:1.1DL+1.0W	0.026	1.458	-0.000	1.458	0.026	1.458	1152
			4:1.25DL	0.036	1.458	-0.000	0.417	0.036	1.458	823
			5:1.1DL+1.0W	0.021	0.417	-0.000	0.417	0.021	0.417	1440
			6:CASE I: VX	0.001	1.042	0.000	2.083	0.001	1.042	> 10000
			7:1.1DL+1.0W	0.026	1.458	0.000	2.292	0.026	1.458	1152
			8:CASE I: VY	0.021	0.417	0	0	0.021	0.417	1440
			13:CASE III: V'	0.015625	0.208	-0.000	0.417	0.015625	0.208	1920
			14:CASE III: V _i	0.002	1.458	0.000	2.083	0.002	1.458	> 10000
			15:CASE III:V _x	0.001	1.042	-0.000	2.292	0.001	1.042	> 10000
29	27	2.500	2:DYNO DRUM	0.002	2.292	0.000	1.250	0.002	2.292	> 10000
			1:WEIGHT	0.046875	1.042	-0.000	2.083	0.046875	1.042	640
			10:WIND LOA	-0.001	1.042	-0.000	0.417	0.001	1.042	> 10000
			11:WIND LOA	-0.03125	1.875	-0.000	1.875	0.03125	1.875	960
			12:DYNO DRU	0.000	1.042	-0.000	0.417	0.000	1.042	> 10000
			16:WIND RES	0.004	2.083	-0.000	1.250	0.004	2.083	8378
			9:COMPRESS	0	0	0	0	0.000	1.458	
			3:1.1DL+1.0W	0.039	2.083	0	0	0.039	2.083	768
			4:1.25DL	0.036	1.458	-0.000	1.667	0.036	1.458	823
			5:1.1DL+1.0W	0.057	1.458	0.000	2.292	0.057	1.458	524



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			6:CASE I: VX	-0.001	1.042	-0.000	0.417	0.001	1.042	> 10000
			7:1.1DL+1.0Wz	0.03125	1.875	-0.000	0.208	0.03125	1.875	960
			8:CASE I: VY	0.046875	1.042	-0.000	2.083	0.046875	1.042	640
			13:CASE III: V'	0.023	2.083	-0.000	0.417	0.023	2.083	1280
			14:CASE III: Vz	0.003	1.458	0.000	1.667	0.003	1.458	8777
			15:CASE III:Vx	-0.001	1.042	0.000	2.292	0.001	1.042	> 10000
30	3	1.000	2:DYNO DRUM	0.003	0.083	0.000	0.083	0.003	0.083	4608
			1:WEIGHT	0.03125	0.083	-0.000	0.500	0.03125	0.083	384
			10:WIND LOA	-0.000	0.083	0.000	0.583	0.000	0.583	> 10000
			11:WIND LOA	0.073	0.917	-0.000	0.333	0.073	0.917	165
			12:DYNO DRU	-0.000	0.083	-0.000	0.750	0.000	0.750	> 10000
			16:WIND RES	-0.005	0.583	0.000	0.083	0.005	0.583	2633
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0Wf	0.0625	0.667	0.000	0.083	0.0625	0.667	192
			4:1.25DL	-0.0625	0.250	-0.000	0.750	0.0625	0.250	192
			5:1.1DL+1.0Wz	0.03125	0.167	0.000	0.250	0.03125	0.167	384
			6:CASE I: VX	-0.000	0.083	0.000	0.583	0.000	0.583	> 10000
			7:1.1DL+1.0Wz	0.03125	0.500	-0.000	0.750	0.03125	0.500	384
			8:CASE I: VY	0.03125	0.083	-0.000	0.500	0.03125	0.083	384
			13:CASE III: V'	0.03125	0.250	0.000	0.500	0.03125	0.250	384
			14:CASE III: Vz	-0.004	0.833	-0.000	0.167	0.004	0.833	3072
			15:CASE III:Vx	0.000	0.833	-0.000	0.083	0.000	0.583	> 10000
31	5	1.000	2:DYNO DRUM	0.004	0.167	0.000	0.500	0.004	0.500	3072
			1:WEIGHT	-0.03125	0.500	0.000	0.417	0.03125	0.500	384
			10:WIND LOA	0.000	0.833	0	0	0.000	0.917	> 10000
			11:WIND LOA	0.0625	0.083	0.000	0.917	0.0625	0.083	192
			12:DYNO DRU	0.000	0.917	0.000	0.917	0.000	0.917	> 10000
			16:WIND RES	0	0	0.000	0.250	0.000	0.250	
			9:COMPRESS	0	0	0	0	0.000	0.917	
			3:1.1DL+1.0Wf	0.0625	0.667	0.000	0.333	0.0625	0.667	192
			4:1.25DL	0.0625	0.250	-0.000	0.750	0.0625	0.250	192
			5:1.1DL+1.0Wz	0.03125	0.167	-0.000	0.917	0.03125	0.167	384
			6:CASE I: VX	0.000	0.833	0	0	0.000	0.917	> 10000
			7:1.1DL+1.0Wz	-0.073	0.583	0.000	0.750	0.073	0.583	165
			8:CASE I: VY	-0.03125	0.500	0.000	0.417	0.03125	0.500	384
			13:CASE III: V'	-0.03125	0.250	0	0	0.03125	0.250	384
			14:CASE III: Vz	-0.003	0.833	0.000	0.667	0.003	0.833	3686
			15:CASE III:Vx	0.000	0.833	-0.000	0.167	0.000	0.833	> 10000
32	15	4.830	2:DYNO DRUM	0.000	0.402	0.013	4.025	0.013	4.025	> 10000
			1:WEIGHT	0.000	2.012	0.083	3.220	0.083	3.220	> 10000
			10:WIND LOA	0.003	1.610	-0.008	2.415	0.008	2.415	> 10000
			11:WIND LOA	-0.000	3.622	-0.115	2.817	0.115	2.817	> 10000
			12:DYNO DRU	-0.000	2.415	0.002	2.415	0.002	2.415	> 10000
			16:WIND RES	0.003	2.012	0.007	4.025	0.007	4.025	> 10000
			9:COMPRESS	0	0	0	0	0.000	4.025	



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Beam Maximum Relative Displacements Cont...

Beam	Node A	Length (ft)	L/C	y (in)	d (ft)	z (in)	d (ft)	Resultant (in)	d (ft)	Span Max z
			3:1.1DL+1.0Wf	0.003	2.012	0.125	2.817	0.125	2.817	> 10000
			4:1.25DL	-0.000	2.012	0.125	4.025	0.140	4.025	> 10000
			5:1.1DL+1.0Wf	0.003	2.012	0.089	2.817	0.089	2.817	> 10000
			6:CASE I: VX	0.003	1.610	-0.008	2.415	0.008	2.415	> 10000
			7:1.1DL+1.0Wf	0.000	4.025	0.104	3.220	0.104	4.025	> 10000
			8:CASE I: VY	0.000	2.012	0.083	3.220	0.083	3.220	> 10000
			13:CASE III: V'	-0.000	0.402	0.052	2.817	0.052	2.817	> 10000
			14:CASE III: V _i	-0.000	4.427	0.007	2.012	0.007	2.012	> 10000
			15:CASE III:VX	0.002	1.610	-0.004	2.415	0.005	2.415	> 10000
33	12	4.830	2:DYNO DRUM	0.000	0.805	0.004	2.817	0.006	4.428	> 10000
			1:WEIGHT	0.000	2.415	0.036	4.427	0.044	2.415	> 10000
			10:WIND LOA	0.003	1.610	0.008	2.415	0.008	2.415	> 10000
			11:WIND LOA	-0.000	2.012	0.0625	2.415	0.088	2.415	> 10000
			12:DYNO DRU	-0.000	1.207	-0.002	2.415	0.002	2.415	> 10000
			16:WIND RES	0.003	2.012	0.007	4.025	0.007	4.025	> 10000
			9:COMPRESS	0	0	0	0	0.000	4.025	
			3:1.1DL+1.0Wf	0.003	2.012	-0.03125	2.415	0.070	2.415	> 10000
			4:1.25DL	-0.000	4.427	-0.0625	2.415	0.088	2.415	> 10000
			5:1.1DL+1.0Wf	0.003	1.610	0.0625	2.817	0.063	2.817	> 10000
			6:CASE I: VX	0.003	1.610	0.008	2.415	0.008	2.415	> 10000
			7:1.1DL+1.0Wf	0.000	2.817	0.046875	2.817	0.070	1.207	> 10000
			8:CASE I: VY	0.000	2.415	0.036	4.427	0.044	2.415	> 10000
			13:CASE III: V'	0.000	3.220	0.052	4.025	0.052	4.025	> 10000
			14:CASE III: V _i	0.000	3.220	0.003	4.025	0.003	4.025	> 10000
			15:CASE III:VX	0.002	1.610	0.004	2.415	0.005	2.415	> 10000

Beam End Displacement Summary

Displacements shown in *italic* indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	28	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6
Min X	28	26	4:1.25DL	-0.962	-556E+3	1.07E+6	1.21E+6
Max Y	30	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6
Min Y	30	28	4:1.25DL	0.086	-1.22E+6	-149E+3	1.23E+6
Max Z	28	26	4:1.25DL	-0.962	-556E+3	1.07E+6	1.21E+6
Min Z	28	26	11:WIND LOA	1.131	653E+3	-1.26E+6	1.42E+6
Max Rst	30	28	11:WIND LOA	-0.102	1.44E+6	175E+3	1.45E+6



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Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	28	26	9:COMPRESS	3.000	0.000	0.000	-0.000	-0.000	0.000
Min Fx	8	7	11:WIND LOA	-1.284	-0.340	-0.014	-7.549	0.126	-8.507
Max Fy	14	10	11:WIND LOA	0.460	1.290	0.000	-0.000	25.560	10.370
Min Fy	11	7	11:WIND LOA	0.460	-1.290	0.000	0.000	-13.800	-10.370
Max Fz	11	7	16:WIND RES	0.055	-0.104	0.206	-0.000	-1.123	1.339
Min Fz	27	25	2:DYNO DRUM	0.084	-0.001	-0.179	0.006	1.395	-0.005
Max Mx	5	3	11:WIND LOA	0.014	-0.105	0.006	8.964	-0.025	4.498
Min Mx	5	3	4:1.25DL	-0.013	0.116	-0.005	-7.923	0.024	-3.849
Max My	14	15	11:WIND LOA	0.460	1.290	0.000	-0.000	25.560	-0.000
Min My	14	15	7:1.1DL+1.0W	-0.301	-1.064	-0.157	0.000	-20.963	-0.000
Max Mz	29	17	4:1.25DL	-0	-0.432	0.000	-0.000	0.000	33.470
Min Mz	29	17	11:WIND LOA	-0	0.460	0.000	-0.000	-0.000	-39.360

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	28	9:COMPRESS	0	3.000	0.000	0.000	-0.000	-0.000	0.000
Min Fx	8	11:WIND LOA	0	-1.284	-0.340	-0.014	-7.549	0.126	-8.507
Max Fy	14	11:WIND LOA	0	0.460	1.290	0.000	-0.000	25.560	10.370
Min Fy	11	11:WIND LOA	0	0.460	-1.290	0.000	0.000	-13.800	-10.370
Max Fz	11	16:WIND RES	0	0.055	-0.104	0.206	-0.000	-1.123	1.339
Min Fz	27	2:DYNO DRUM	0	0.084	-0.001	-0.179	0.006	1.395	-0.005
Max Mx	5	11:WIND LOA	0	0.014	-0.105	0.006	8.964	-0.025	4.498
Min Mx	5	4:1.25DL	0	-0.013	0.116	-0.005	-7.923	0.024	-3.849
Max My	14	11:WIND LOA	0.670	0.460	1.290	0.000	-0.000	25.560	-0.000
Min My	14	7:1.1DL+1.0W	0.670	-0.301	-1.064	-0.157	0.000	-20.963	-0.000
Max Mz	29	4:1.25DL	2.500	-0	-0.432	0.000	-0.000	0.000	33.470
Min Mz	29	11:WIND LOA	2.500	-0	0.460	0.000	-0.000	-0.000	-39.360



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Beam Maximum Shear Forces

Distances to maxima are given from beam end A.

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
1	2	1.000	2:DYNO DRUM	Max +ve	0	0.179	0	0.000
				Max -ve				
			1:WEIGHT	Max +ve				
				Max -ve	0	-0.000	1.000	-0.029
			10:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.001
			11:WIND LOA	Max +ve	0	0.000	1.000	0.008
				Max -ve			0	-0.012
			12:DYNO DRU	Max +ve	0	0.000	0	0.000
				Max -ve				
			16:WIND RESI	Max +ve				
				Max -ve	0	-0.071	0	-0.000
			9:COMPRESSI	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.071	1.000	-0.032
			4:1.25DL	Max +ve				
				Max -ve	0	-0.000	1.000	-0.036
			5:1.1DL+1.0W	Max +ve	0	0.000		
				Max -ve			1.000	-0.033
			6:CASE I: VX	Max +ve	0	0.000		
				Max -ve			0	-0.001
			7:1.1DL+1.0W	Max +ve	0	0.179		
				Max -ve			1.000	-0.031
			8:CASE I: VY	Max +ve				
				Max -ve	0	-0.000	1.000	-0.029
			13:CASE III: V	Max +ve				
				Max -ve	0	-0.000	1.000	-0.022
			14:CASE III: V	Max +ve	0	0.134	0	0.000
				Max -ve				
			15:CASE III:VX	Max +ve	0	0.001		
				Max -ve			0	-0.001
2	3	1.500	2:DYNO DRUM	Max +ve	0	0.025403		
				Max -ve			0	-0.019
			1:WEIGHT	Max +ve				
				Max -ve	0	-0.010	1.500	-0.182
			10:WIND LOA	Max +ve			0	0.034
				Max -ve	0	-0.022		
			11:WIND LOA	Max +ve	0	0.014	1.500	0.290
				Max -ve				
			12:DYNO DRU	Max +ve				
				Max -ve	0	-0.021	0	-0.003
			16:WIND RESI	Max +ve			0	0.009
				Max -ve	0	-0.062		



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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			9:COMPRESSI	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.073	1.500	-0.192
			4:1.25DL	Max +ve				
				Max -ve	0	-0.013	1.500	-0.228
			5:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.054	1.500	-0.170
			6:CASE I: VX	Max +ve			0	0.034
				Max -ve	0	-0.022		
			7:1.1DL+1.0W	Max +ve	0	0.014		
				Max -ve			1.500	-0.220
			8:CASE I: VY	Max +ve				
				Max -ve	0	-0.010	1.500	-0.182
			13:CASE III: V	Max +ve				
				Max -ve	0	-0.008	1.500	-0.137
			14:CASE III: V	Max +ve	0	0.019		
				Max -ve			0	-0.015
			15:CASE III:VX	Max +ve			0	0.023
				Max -ve	0	-0.032		
3	4	0.500	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.0261	0	-0.019
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			0.500	-0.218
			10:WIND LOA	Max +ve	0	0.030	0	0.033
				Max -ve				
			11:WIND LOA	Max +ve			0.500	0.306
				Max -ve	0	-0.000		
			12:DYNO DRU	Max +ve	0	0.029		
				Max -ve			0	-0.003
			16:WIND RES	Max +ve	0	0.068	0	0.008
				Max -ve				
			9:COMPRESSI	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve	0	0.068		
				Max -ve			0.500	-0.231
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			0.500	-0.272
			5:1.1DL+1.0W	Max +ve	0	0.059		
				Max -ve			0.500	-0.209
			6:CASE I: VX	Max +ve	0	0.030	0	0.033
				Max -ve				
			7:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.026	0.500	-0.258
			8:CASE I: VY	Max +ve	0	0.000		



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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			0.500	-0.218
			13:CASE III: V'	Max +ve	0	0.000		
				Max -ve			0.500	-0.163
			14:CASE III: V _i	Max +ve				
				Max -ve	0	-0.020	0	-0.014
			15:CASE III:V _x	Max +ve	0	0.045	0	0.023
				Max -ve				
4	5	7.000	2:DYNO DRUM	Max +ve	0	0.052	0	0.001
				Max -ve				
			1:WEIGHT	Max +ve			0	0.092
				Max -ve	0	-0.000		
			10:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.002
			11:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.167
			12:DYNO DRU	Max +ve			0	0.000
				Max -ve	0	-0.000		
			16:WIND RES	Max +ve				
				Max -ve	0	-0.021	0	-0.000
			9:COMPRESS	Max +ve	0	0.000		
				Max -ve			0	-0.000
			3:1.1DL+1.0W	Max +ve			0	0.100
				Max -ve	0	-0.021		
			4:1.25DL	Max +ve			0	0.115
				Max -ve	0	-0.000		
			5:1.1DL+1.0W	Max +ve			0	0.099
				Max -ve	0	-0.000		
			6:CASE I: VX	Max +ve	0	0.000		
				Max -ve			0	-0.002
			7:1.1DL+1.0W	Max +ve	0	0.052	0	0.102
				Max -ve				
			8:CASE I: VY	Max +ve			0	0.092
				Max -ve	0	-0.000		
			13:CASE III: V'	Max +ve			0	0.069
				Max -ve	0	-0.000		
			14:CASE III: V _i	Max +ve	0	0.039	0	0.001
				Max -ve				
			15:CASE III:V _x	Max +ve	0	0.000		
				Max -ve			0	-0.001
5	3	2.000	2:DYNO DRUM	Max +ve	0	0.144	0	0.020
				Max -ve				
			1:WEIGHT	Max +ve			0	0.093
				Max -ve	0	-0.004		
			10:WIND LOA	Max +ve	2.000	0.033		
				Max -ve	0	-0.007	0	-0.036



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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			11:WIND LOA	Max +ve	0	0.006		
				Max -ve			0	-0.105
			12:DYNO DRU	Max +ve	0	0.016	0	0.003
				Max -ve				
			16:WIND RES	Max +ve				
				Max -ve	0	-0.026	0	-0.009
			9:COMPRESS	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0W	Max +ve			0	0.093
				Max -ve	0	-0.031		
			4:1.25DL	Max +ve			0	0.116
				Max -ve	0	-0.005		
			5:1.1DL+1.0W	Max +ve	2.000	0.045	0	0.069
				Max -ve				
			6:CASE I: VX	Max +ve	2.000	0.033		
				Max -ve	0	-0.007	0	-0.036
			7:1.1DL+1.0W	Max +ve	0	0.139	0	0.122
				Max -ve				
			8:CASE I: VY	Max +ve			0	0.093
				Max -ve	0	-0.004		
			13:CASE III: V	Max +ve			0	0.069
				Max -ve	0	-0.003		
			14:CASE III: V	Max +ve	0	0.108	0	0.015
				Max -ve				
			15:CASE III:VX	Max +ve	2.000	0.037		
				Max -ve			0	-0.024
6	5	2.000	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.144	0	-0.020
			1:WEIGHT	Max +ve	0	0.004		
				Max -ve			2.000	-0.362
			10:WIND LOA	Max +ve	2.000	0.033	0	0.036
				Max -ve	0	-0.007		
			11:WIND LOA	Max +ve			2.000	0.574
				Max -ve	0	-0.006		
			12:DYNO DRU	Max +ve	0	0.016		
				Max -ve			0	-0.003
			16:WIND RES	Max +ve	0	0.090	0	0.009
				Max -ve				
			9:COMPRESS	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve	0	0.095		
				Max -ve			2.000	-0.389
			4:1.25DL	Max +ve	0	0.005		
				Max -ve			2.000	-0.452
			5:1.1DL+1.0W	Max +ve	2.000	0.054		



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Job Title Pier Analysis

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Ref

By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			2.000	-0.366
			6:CASE I: VX	Max +ve	2.000	0.033	0	0.036
				Max -ve	0	-0.007		
			7:1.1DL+1.0Wz	Max +ve				
				Max -ve	0	-0.139	2.000	-0.418
			8:CASE I: VY	Max +ve	0	0.004		
				Max -ve			2.000	-0.362
			13:CASE III: V'	Max +ve	0	0.003		
				Max -ve			2.000	-0.271
			14:CASE III: Vz	Max +ve				
				Max -ve	0	-0.108	0	-0.015
			15:CASE III:Vx	Max +ve	2.000	0.037	0	0.024
				Max -ve				
7	8	1.000	2:DYNO DRUM	Max +ve	0	0.179		
				Max -ve			0	-0.000
			1:WEIGHT	Max +ve				
				Max -ve	0	-0.000	1.000	-0.046
			10:WIND LOA	Max +ve	0	0.000	0	0.001
				Max -ve				
			11:WIND LOA	Max +ve	0	0.000	1.000	0.032
				Max -ve				
			12:DYNO DRU	Max +ve	0	0.000		
				Max -ve			0	-0.000
			16:WIND RES	Max +ve			0	0.000
				Max -ve	0	-0.071		
			9:COMPRESS	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.071	1.000	-0.050
			4:1.25DL	Max +ve				
				Max -ve	0	-0.000	1.000	-0.057
			5:1.1DL+1.0W	Max +ve	0	0.001		
				Max -ve			1.000	-0.049
			6:CASE I: VX	Max +ve	0	0.000	0	0.001
				Max -ve				
			7:1.1DL+1.0Wz	Max +ve	0	0.179		
				Max -ve			1.000	-0.051
			8:CASE I: VY	Max +ve				
				Max -ve	0	-0.000	1.000	-0.046
			13:CASE III: V'	Max +ve				
				Max -ve	0	-0.000	1.000	-0.034
			14:CASE III: Vz	Max +ve	0	0.134		
				Max -ve			0	-0.000
			15:CASE III:Vx	Max +ve	0	0.001	0	0.001
				Max -ve				



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
8	7	1.500	2:DYNO DRUM	Max +ve	0	0.026797	0	0.019
				Max -ve				
			1:WEIGHT	Max +ve	0	0.010	0	0.234
				Max -ve				
			10:WIND LOA	Max +ve				
				Max -ve	0	-0.023	0	-0.128
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.014	0	-0.340
			12:DYNO DRU	Max +ve			0	0.031
				Max -ve	0	-0.021		
			16:WIND RES	Max +ve				
				Max -ve	0	-0.058	0	-0.063
			9:COMPRESS	Max +ve	0	0.000		
				Max -ve			0	-0.000
			3:1.1DL+1.0W	Max +ve			0	0.195
				Max -ve	0	-0.047		
			4:1.25DL	Max +ve	0	0.013	0	0.293
				Max -ve				
			5:1.1DL+1.0W	Max +ve			0	0.161
				Max -ve	0	-0.033		
			6:CASE I: VX	Max +ve				
				Max -ve	0	-0.023	0	-0.128
			7:1.1DL+1.0W	Max +ve	0	0.038	0	0.277
				Max -ve				
			8:CASE I: VY	Max +ve	0	0.010	0	0.234
				Max -ve				
			13:CASE III: V	Max +ve	0	0.008	0	0.176
				Max -ve				
			14:CASE III: V	Max +ve	0	0.020	0	0.015
				Max -ve				
			15:CASE III: VX	Max +ve				
				Max -ve	0	-0.033	0	-0.073
9	9	0.500	2:DYNO DRUM	Max +ve			0	0.020
				Max -ve	0	-0.0261		
			1:WEIGHT	Max +ve	0	0.000	0	0.196
				Max -ve				
			10:WIND LOA	Max +ve	0	0.031		
				Max -ve			0	-0.128
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.000	0	-0.308
			12:DYNO DRU	Max +ve	0	0.029	0	0.031
				Max -ve				
			16:WIND RES	Max +ve	0	0.068		
				Max -ve			0	-0.063
			9:COMPRESS	Max +ve				



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Job Title Pier Analysis

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Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0Wf	Max +ve	0	0.068	0	0.153
				Max -ve				
			4:1.25DL	Max +ve	0	0.000	0	0.245
				Max -ve				
			5:1.1DL+1.0W}	Max +ve	0	0.060	0	0.119
				Max -ve				
			6:CASE I: VX	Max +ve	0	0.031		
				Max -ve			0	-0.128
			7:1.1DL+1.0Wz	Max +ve			0	0.236
				Max -ve	0	-0.0261		
			8:CASE I: VY	Max +ve	0	0.000	0	0.196
				Max -ve				
			13:CASE III: V'	Max +ve	0	0.000	0	0.147
				Max -ve				
			14:CASE III: Vz	Max +ve			0	0.015
				Max -ve	0	-0.020		
			15:CASE III: VX	Max +ve	0	0.045		
				Max -ve			0	-0.073
10	10	7.000	2:DYNO DRUM	Max +ve	0	0.052		
				Max -ve			0	-0.001
			1:WEIGHT	Max +ve	0	0.000	0	0.084
				Max -ve				
			10:WIND LOAI	Max +ve			0	0.002
				Max -ve	0	-0.000		
			11:WIND LOAI	Max +ve				
				Max -ve	0	-0.000	0	-0.153
			12:DYNO DRU	Max +ve	0	0.000		
				Max -ve			0	-0.000
			16:WIND RESI	Max +ve			0	0.000
				Max -ve	0	-0.021		
			9:COMPRESSI	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0Wf	Max +ve			0	0.092
				Max -ve	0	-0.021		
			4:1.25DL	Max +ve	0	0.000	0	0.104
				Max -ve				
			5:1.1DL+1.0W}	Max +ve	0	0.000	0	0.094
				Max -ve				
			6:CASE I: VX	Max +ve			0	0.002
				Max -ve	0	-0.000		
			7:1.1DL+1.0Wz	Max +ve	0	0.052	0	0.091
				Max -ve				
			8:CASE I: VY	Max +ve	0	0.000	0	0.084
				Max -ve				



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Job Title Pier Analysis

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Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			13:CASE III: V'	Max +ve	0	0.000	0	0.063
				Max -ve				
			14:CASE III: V _z	Max +ve	0	0.039		
				Max -ve			0	-0.001
			15:CASE III:V _x	Max +ve			0	0.001
				Max -ve	0	-0.000		
11	7	0.670	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.157	0	-0.010
			1:WEIGHT	Max +ve			0	0.976
				Max -ve	0	-0.000		
			10:WIND LOAI	Max +ve	0	0.045		
				Max -ve			0.670	-0.0734
			11:WIND LOAI	Max +ve	0	0.000		
				Max -ve			0	-1.290
			12:DYNO DRU	Max +ve	0	0.041655		
				Max -ve			0	-0.083
			16:WIND RESI	Max +ve	0	0.206		
				Max -ve			0	-0.104
			9:COMPRESSI	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve	0	0.206	0	0.970
				Max -ve				
			4:1.25DL	Max +ve			0	1.220
				Max -ve	0	-0.000		
			5:1.1DL+1.0W	Max +ve	0	0.087	0	0.930
				Max -ve				
			6:CASE I: VX	Max +ve	0	0.045		
				Max -ve			0.670	-0.0734
			7:1.1DL+1.0W _z	Max +ve			0	1.064
				Max -ve	0	-0.157		
			8:CASE I: VY	Max +ve			0	0.976
				Max -ve	0	-0.000		
			13:CASE III: V'	Max +ve			0	0.732
				Max -ve	0	-0.000		
			14:CASE III: V _z	Max +ve				
				Max -ve	0	-0.117	0	-0.007
			15:CASE III:V _x	Max +ve	0	0.065		
				Max -ve			0.670	-0.118
14	10	0.670	2:DYNO DRUM	Max +ve			0	0.010
				Max -ve	0	-0.157		
			1:WEIGHT	Max +ve				
				Max -ve	0	-0.000	0	-0.976
			10:WIND LOAI	Max +ve				
				Max -ve	0	-0.045	0.670	-0.0734
			11:WIND LOAI	Max +ve	0	0.000	0	1.290



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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve				
			12:DYNO DRU	Max +ve				
				Max -ve	0	-0.042	0	-0.083
			16:WIND RESI	Max +ve	0	0.008		
				Max -ve			0	-0.111
			9:COMPRESSI	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0W	Max +ve	0	0.008		
				Max -ve			0	-1.184
			4:1.25DL	Max +ve				
				Max -ve	0	-0.000	0	-1.220
			5:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.087	0.670	-1.231
			6:CASE I: VX	Max +ve				
				Max -ve	0	-0.045	0.670	-0.0734
			7:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.157	0	-1.064
			8:CASE I: VY	Max +ve				
				Max -ve	0	-0.000	0	-0.976
			13:CASE III: V	Max +ve				
				Max -ve	0	-0.000	0	-0.732
			14:CASE III: V	Max +ve				
				Max -ve	0	-0.117	0	0.007
			15:CASE III:VX	Max +ve				
				Max -ve	0	-0.065	0.670	-0.118
20	18	7.000	2:DYNO DRUM	Max +ve			0	0.001
				Max -ve	0	-0.052		
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			7.000	-0.070
			10:WIND LOAI	Max +ve	0	0.000		
				Max -ve			0	-0.002
			11:WIND LOAI	Max +ve			7.000	0.135
				Max -ve	0	-0.000	0	-0.005
			12:DYNO DRU	Max +ve	0	0.000	0	0.000
				Max -ve				
			16:WIND RESI	Max +ve	0	0.021		
				Max -ve			0	-0.000
			9:COMPRESSI	Max +ve	0	0.000		
				Max -ve			0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.020817		
				Max -ve			7.000	-0.077
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			7.000	-0.088
			5:1.1DL+1.0W	Max +ve	0	0.000		
				Max -ve			7.000	-0.079



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			6:CASE I: VX	Max +ve	0	0.000		
				Max -ve			0	-0.002
			7:1.1DL+1.0Wz	Max +ve				
				Max -ve	0	-0.052	7.000	-0.076
			8:CASE I: VY	Max +ve	0	0.000		
				Max -ve			7.000	-0.070
			13:CASE III: V'	Max +ve	0	0.000		
				Max -ve			7.000	-0.053
			14:CASE III: Vz	Max +ve			0	0.001
				Max -ve	0	-0.039		
			15:CASE III:Vx	Max +ve	0	0.000		
				Max -ve			0	-0.001
21	19	7.000	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.052	0	-0.001
			1:WEIGHT	Max +ve				
				Max -ve	0	-0.000	7.000	-0.105
			10:WIND LOA	Max +ve			0	0.002
				Max -ve	0	-0.000		
			11:WIND LOA	Max +ve	0	0.000	7.000	0.185
				Max -ve				
			12:DYNO DRU	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			16:WIND RES	Max +ve	0	0.021	0	0.000
				Max -ve				
			9:COMPRESS	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve	0	0.020902		
				Max -ve			7.000	-0.115
			4:1.25DL	Max +ve				
				Max -ve	0	-0.000	7.000	-0.132
			5:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.000	7.000	-0.114
			6:CASE I: VX	Max +ve			0	0.002
				Max -ve	0	-0.000		
			7:1.1DL+1.0Wz	Max +ve				
				Max -ve	0	-0.052	7.000	-0.117
			8:CASE I: VY	Max +ve				
				Max -ve	0	-0.000	7.000	-0.105
			13:CASE III: V'	Max +ve				
				Max -ve	0	-0.000	7.000	-0.079
			14:CASE III: Vz	Max +ve				
				Max -ve	0	-0.039	0	-0.001
			15:CASE III:Vx	Max +ve			0	0.001
				Max -ve	0	-0.000		
22	20	0.500	2:DYNO DRUM	Max +ve	0	0.0261		



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			0	-0.019
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			0.500	-0.188
			10:WIND LOA	Max +ve	0	0.030	0	0.033
				Max -ve				
			11:WIND LOA	Max +ve			0.500	0.296
				Max -ve	0	-0.000		
			12:DYNO DRU	Max +ve	0	0.029		
				Max -ve			0	-0.003
			16:WIND RES	Max +ve	0	0.068	0	0.008
				Max -ve				
			9:COMPRESS	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve	0	0.068		
				Max -ve			0.500	-0.199
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			0.500	-0.235
			5:1.1DL+1.0W	Max +ve	0	0.059		
				Max -ve			0.500	-0.177
			6:CASE I: VX	Max +ve	0	0.030	0	0.033
				Max -ve				
			7:1.1DL+1.0W	Max +ve	0	0.026		
				Max -ve			0.500	-0.226
			8:CASE I: VY	Max +ve	0	0.000		
				Max -ve			0.500	-0.188
			13:CASE III: V	Max +ve	0	0.000		
				Max -ve			0.500	-0.141
			14:CASE III: V	Max +ve	0	0.019575		
				Max -ve			0	-0.014
			15:CASE III:VX	Max +ve	0	0.045	0	0.023
				Max -ve				
23	21	0.500	2:DYNO DRUM	Max +ve	0	0.0261	0	0.020
				Max -ve				
			1:WEIGHT	Max +ve	0	0.000	0	0.226
				Max -ve				
			10:WIND LOA	Max +ve	0	0.031		
				Max -ve			0	-0.128
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.000	0	-0.318
			12:DYNO DRU	Max +ve	0	0.029	0	0.031
				Max -ve				
			16:WIND RES	Max +ve	0	0.068		
				Max -ve			0	-0.063
			9:COMPRESS	Max +ve				
				Max -ve	0	-0.000	0	-0.000



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			3:1.1DL+1.0Wf	Max +ve	0	0.068	0	0.185
				Max -ve				
			4:1.25DL	Max +ve	0	0.000	0	0.282
				Max -ve				
			5:1.1DL+1.0W)	Max +ve	0	0.060	0	0.151
				Max -ve				
			6:CASE I: VX	Max +ve	0	0.031		
				Max -ve			0	-0.128
			7:1.1DL+1.0Wz	Max +ve	0	0.026	0	0.268
				Max -ve				
			8:CASE I: VY	Max +ve	0	0.000	0	0.226
				Max -ve				
			13:CASE III: V'	Max +ve	0	0.000	0	0.169
				Max -ve				
			14:CASE III: Vz	Max +ve	0	0.019575	0	0.015
				Max -ve				
			15:CASE III:Vx	Max +ve	0	0.045		
				Max -ve			0	-0.073
24	22	1.500	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.025	0	-0.019
			1:WEIGHT	Max +ve	0	0.010396		
				Max -ve			1.500	-0.241
			10:WIND LOA	Max +ve			0	0.034
				Max -ve	0	-0.022		
			11:WIND LOA	Max +ve			1.500	0.347
				Max -ve	0	-0.014		
			12:DYNO DRU	Max +ve				
				Max -ve	0	-0.021	0	-0.003
			16:WIND RES	Max +ve			0	0.009
				Max -ve	0	-0.042		
			9:COMPRESS	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0Wf	Max +ve				
				Max -ve	0	-0.030	1.500	-0.256
			4:1.25DL	Max +ve	0	0.013		
				Max -ve			1.500	-0.301
			5:1.1DL+1.0W)	Max +ve				
				Max -ve	0	-0.031	1.500	-0.234
			6:CASE I: VX	Max +ve			0	0.034
				Max -ve	0	-0.022		
			7:1.1DL+1.0Wz	Max +ve				
				Max -ve	0	-0.014	1.500	-0.284
			8:CASE I: VY	Max +ve	0	0.010396		
				Max -ve			1.500	-0.241
			13:CASE III: V'	Max +ve	0	0.008		



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Job Title Pier Analysis

Part

Ref

By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			1.500	-0.180
			14:CASE III: V _i	Max +ve				
				Max -ve	0	-0.019	0	-0.015
			15:CASE III:V _x	Max +ve			0	0.023
				Max -ve	0	-0.032		
25	23	1.500	2:DYNO DRUM	Max +ve			0	0.019
				Max -ve	0	-0.027		
			1:WEIGHT	Max +ve			0	0.188
				Max -ve	0	-0.010		
			10:WIND LOA	Max +ve				
				Max -ve	0	-0.023	0	-0.128
			11:WIND LOA	Max +ve				
				Max -ve			0	-0.297
			12:DYNO DRU	Max +ve			0	0.031
				Max -ve	0	-0.021		
			16:WIND RES	Max +ve				
				Max -ve	0	-0.036	0	-0.063
			9:COMPRESS	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0W	Max +ve			0	0.144
				Max -ve	0	-0.048		
			4:1.25DL	Max +ve			0	0.235
				Max -ve	0	-0.013		
			5:1.1DL+1.0W	Max +ve			0	0.110
				Max -ve	0	-0.056		
			6:CASE I: VX	Max +ve				
				Max -ve	0	-0.023	0	-0.128
			7:1.1DL+1.0W	Max +ve			0	0.226
				Max -ve	0	-0.038		
			8:CASE I: VY	Max +ve			0	0.188
				Max -ve	0	-0.010		
			13:CASE III: V'	Max +ve			0	0.141
				Max -ve	0	-0.008		
			14:CASE III: V _i	Max +ve			0	0.015
				Max -ve	0	-0.020		
			15:CASE III:V _x	Max +ve				
				Max -ve	0	-0.033	0	-0.073
26	24	1.000	2:DYNO DRUM	Max +ve			0	0.001
				Max -ve	0	-0.179		
			1:WEIGHT	Max +ve			0	0.039
				Max -ve				
			10:WIND LOA	Max +ve			0	0.000
				Max -ve			0	-0.001
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.000	0	-0.023



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			12:DYNO DRU	Max +ve	0	0.000	0	0.000
				Max -ve				
			16:WIND RESI	Max +ve	0	0.073		
				Max -ve			0	-0.000
			9:COMPRESSI	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.073	0	0.043
				Max -ve				
			4:1.25DL	Max +ve	0	0.000	0	0.049
				Max -ve				
			5:1.1DL+1.0W	Max +ve	0	0.001	0	0.042
				Max -ve				
			6:CASE I: VX	Max +ve	0	0.000		
				Max -ve			0	-0.001
			7:1.1DL+1.0W	Max +ve			0	0.044
				Max -ve	0	-0.179		
			8:CASE I: VY	Max +ve	0	0.000	0	0.039
				Max -ve				
			13:CASE III: V	Max +ve	0	0.000	0	0.029
				Max -ve				
			14:CASE III: V	Max +ve			0	0.000
				Max -ve	0	-0.134		
			15:CASE III:VX	Max +ve	0	0.001		
				Max -ve			0	-0.001
27	25	1.000	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.179	0	-0.001
			1:WEIGHT	Max +ve	0	0.000	0	0.035
				Max -ve				
			10:WIND LOAI	Max +ve	0	0.000	0	0.001
				Max -ve				
			11:WIND LOAI	Max +ve			1.000	0.004
				Max -ve	0	-0.000	0	-0.016
			12:DYNO DRU	Max +ve	0	0.000		
				Max -ve			0	-0.000
			16:WIND RESI	Max +ve	0	0.072	0	0.000
				Max -ve				
			9:COMPRESSI	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0W	Max +ve	0	0.072	0	0.039
				Max -ve				
			4:1.25DL	Max +ve	0	0.000	0	0.044
				Max -ve				
			5:1.1DL+1.0W	Max +ve	0	0.001	0	0.040
				Max -ve				
			6:CASE I: VX	Max +ve	0	0.000	0	0.001



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Job Title Pier Analysis

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By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve				
			7:1.1DL+1.0Wz	Max +ve			0	0.038
				Max -ve	0	-0.179		
			8:CASE I: VY	Max +ve	0	0.000	0	0.035
				Max -ve				
			13:CASE III: V'	Max +ve	0	0.000	0	0.026
				Max -ve				
			14:CASE III: Vz	Max +ve				
				Max -ve	0	-0.134	0	-0.000
			15:CASE III:Vx	Max +ve	0	0.001	0	0.001
				Max -ve				
28	26	2.500	2:DYNO DRUM	Max +ve	0	0.000		
				Max -ve			0	-0.000
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			2.500	-0.346
			10:WIND LOA	Max +ve			0	0.094
				Max -ve	0	-0.000		
			11:WIND LOA	Max +ve			0	0.460
				Max -ve	0	-0.000		
			12:DYNO DRU	Max +ve	0	0.000		
				Max -ve			0	-0.028
			16:WIND RES	Max +ve	0	0.000	0	0.055
				Max -ve				
			9:COMPRESS	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0Wf	Max +ve	0	0.000		
				Max -ve			2.500	-0.326
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			2.500	-0.432
			5:1.1DL+1.0W	Max +ve	0	0.000		
				Max -ve			2.500	-0.314
			6:CASE I: VX	Max +ve			0	0.094
				Max -ve	0	-0.000		
			7:1.1DL+1.0Wz	Max +ve	0	0.000		
				Max -ve			2.500	-0.381
			8:CASE I: VY	Max +ve	0	0.000		
				Max -ve			2.500	-0.346
			13:CASE III: V'	Max +ve	0	0.000		
				Max -ve			2.500	-0.259
			14:CASE III: Vz	Max +ve	0	0.000		
				Max -ve			0	-0.000
			15:CASE III:Vx	Max +ve			0	0.050
				Max -ve	0	-0.000		
29	27	2.500	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.000	0	-0.000



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Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			2.500	-0.346
			10:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.094
			11:WIND LOA	Max +ve	0	0.000	0	0.460
				Max -ve				
			12:DYNO DRU	Max +ve	0	0.000	0	0.028
				Max -ve				
			16:WIND RESI	Max +ve				
				Max -ve	0	-0.000	0	-0.055
			9:COMPRESSI	Max +ve			0	0.000
				Max -ve	0	-0.000		
			3:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.000	2.500	-0.435
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			2.500	-0.432
			5:1.1DL+1.0W	Max +ve	0	0.000		
				Max -ve			2.500	-0.447
			6:CASE I: VX	Max +ve	0	0.000		
				Max -ve			0	-0.094
			7:1.1DL+1.0W	Max +ve				
				Max -ve	0	-0.000	2.500	-0.381
			8:CASE I: VY	Max +ve	0	0.000		
				Max -ve			2.500	-0.346
			13:CASE III: V	Max +ve	0	0.000		
				Max -ve			2.500	-0.259
			14:CASE III: V	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			15:CASE III:VX	Max +ve	0	0.000		
				Max -ve			0	-0.050
30	3	1.000	2:DYNO DRUM	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			1:WEIGHT	Max +ve	0	0.000	0	0.010
				Max -ve			1.000	-0.000
			10:WIND LOA	Max +ve	0	0.02		
				Max -ve			0	-0.000
			11:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.020
			12:DYNO DRU	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			16:WIND RESI	Max +ve	0	0.015	0	0.000
				Max -ve				
			9:COMPRESSI	Max +ve	0	0.000		
				Max -ve			0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.015	0	0.011



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Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			1.000	-0.000
			4:1.25DL	Max +ve	0	0.000	0	0.012
				Max -ve			1.000	-0.000
			5:1.1DL+1.0W	Max +ve	0	0.02	0	0.011
				Max -ve			1.000	-0.000
			6:CASE I: VX	Max +ve	0	0.02		
				Max -ve			0	-0.000
			7:1.1DL+1.0W	Max +ve	0	0.000	0	0.011
				Max -ve			1.000	-0.000
			8:CASE I: VY	Max +ve	0	0.000	0	0.010
				Max -ve			1.000	-0.000
			13:CASE III: V	Max +ve	0	0.000	0	0.007
				Max -ve			1.000	-0.000
			14:CASE III: V	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			15:CASE III: VX	Max +ve	0	0.015		
				Max -ve			0	-0.000
31	5	1.000	2:DYNO DRUM	Max +ve			0	0.000
				Max -ve	0	-0.000		
			1:WEIGHT	Max +ve			0	0.010
				Max -ve	0	-0.000		
			10:WIND LOA	Max +ve	0	0.02		
				Max -ve	1.000	-0.000	0	-0.000
			11:WIND LOA	Max +ve	0	0.000		
				Max -ve			0	-0.020
			12:DYNO DRU	Max +ve	0	0.000	0	0.000
				Max -ve				
			16:WIND RES	Max +ve	0	0.015		
				Max -ve			0	-0.000
			9:COMPRESS	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.015	0	0.011
				Max -ve				
			4:1.25DL	Max +ve			0	0.012353
				Max -ve	0	-0.000		
			5:1.1DL+1.0W	Max +ve	0	0.02	0	0.011
				Max -ve	1.000	-0.000		
			6:CASE I: VX	Max +ve	0	0.02		
				Max -ve	1.000	-0.000	0	-0.000
			7:1.1DL+1.0W	Max +ve			0	0.011
				Max -ve	0	-0.000		
			8:CASE I: VY	Max +ve			0	0.010
				Max -ve	0	-0.000		
			13:CASE III: V	Max +ve			0	0.007
				Max -ve	0	-0.000		



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By IERM Date 2/12/2020 Chd

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
			14:CASE III: V _i	Max +ve			0	0.000
				Max -ve	0	-0.000		
			15:CASE III:V _x	Max +ve	0	0.015	0	0.000
				Max -ve	1.000	-0.000		
32	15	4.830	2:DYNO DRUM	Max +ve	0	0.000	0	0.000
				Max -ve				
			1:WEIGHT	Max +ve	0	0.000		
				Max -ve			0	-0.000
			10:WIND LOA	Max +ve			0	0.097
				Max -ve	0	-0.000		
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			12:DYNO DRU	Max +ve	0	0.000		
				Max -ve			0	-0.000
			16:WIND RES	Max +ve			0	0.037
				Max -ve	0	-0.037		
			9:COMPRESS	Max +ve	0	0.000	0	0.000
				Max -ve				
			3:1.1DL+1.0W	Max +ve			0	0.037
				Max -ve	0	-0.037		
			4:1.25DL	Max +ve	0	0.000		
				Max -ve			0	-0.000
			5:1.1DL+1.0W	Max +ve	0	0.000	0	0.097
				Max -ve			4.830	-0.000
			6:CASE I: VX	Max +ve			0	0.097
				Max -ve	0	-0.000		
			7:1.1DL+1.0W	Max +ve	0	0.000		
				Max -ve			0	-0.000
			8:CASE I: VY	Max +ve	0	0.000		
				Max -ve			0	-0.000
			13:CASE III: V'	Max +ve	0	0.000		
				Max -ve			0	-0.000
			14:CASE III: V _i	Max +ve	0	0.000	0	0.000
				Max -ve				
			15:CASE III:V _x	Max +ve			0	0.07245
				Max -ve	0	-0.000		
33	12	4.830	2:DYNO DRUM	Max +ve	0	0.000	0	0.000
				Max -ve				
			1:WEIGHT	Max +ve	0	0.000	0	0.000
				Max -ve				
			10:WIND LOA	Max +ve			0	0.097
				Max -ve	0	-0.000	4.830	-0.000
			11:WIND LOA	Max +ve				
				Max -ve	0	-0.000	0	-0.000
			12:DYNO DRU	Max +ve	0	0.000	0	0



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Client THEA

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Beam Maximum Shear Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fz (kip)	d (ft)	Max Fy (kip)
				Max -ve			0	0
			16:WIND RESI	Max +ve			0	0.037
				Max -ve	0	-0.037		
			9:COMPRESSI	Max +ve	0	0.000		
				Max -ve			0	-0.000
			3:1.1DL+1.0Wf	Max +ve			0	0.037
				Max -ve	0	-0.037		
			4:1.25DL	Max +ve	0	0.000	0	0.000
				Max -ve				
			5:1.1DL+1.0W)	Max +ve	0	0.000	0	0.097
				Max -ve				
			6:CASE I: VX	Max +ve			0	0.097
				Max -ve	0	-0.000	4.830	-0.000
			7:1.1DL+1.0Wz	Max +ve	0	0.000	0	0.000
				Max -ve				
			8:CASE I: VY	Max +ve	0	0.000	0	0.000
				Max -ve				
			13:CASE III: V'	Max +ve	0	0.000	0	0.000
				Max -ve				
			14:CASE III: Vz	Max +ve	0	0.000	0	0.000
				Max -ve				
			15:CASE III:Vx	Max +ve			0	0.07245
				Max -ve	0	-0.000	4.830	-0.000

Beam Maximum Axial Forces

Distances to maxima are given from beam end A.

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
1	2	1.000	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.084
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.000
			10:WIND LOAI	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOAI	Max +ve	0	0.001
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.025
				Max -ve		
			16:WIND RESI	Max +ve	0	0.053
				Max -ve		
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0Wf	Max +ve	0	0.053



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve		
			4:1.25DL	Max +ve		
				Max -ve	0	-0.001
			5:1.1DL+1.0W	Max +ve	0	0.025
				Max -ve		
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.084
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.000
			13:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.063
			15:CASE III: V	Max +ve		
				Max -ve	0	0.019
2	3	1.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.375
			1:WEIGHT	Max +ve	0	0.004
				Max -ve		
			10:WIND LOA	Max +ve	0	0.026
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.006
			12:DYNO DRU	Max +ve	0	0.011
				Max -ve		
			16:WIND RESI	Max +ve	0	0.183
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.188
				Max -ve		
			4:1.25DL	Max +ve	0	0.006
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.042439
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.026
				Max -ve		
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.370
			8:CASE I: VY	Max +ve	0	0.004
				Max -ve		
			13:CASE III: V	Max +ve	0	0.003
				Max -ve		



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Client THEA

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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			14:CASE III: V _i	Max +ve		
				Max -ve	0	-0.281
			15:CASE III:V _X	Max +ve	0	0.028
				Max -ve		
3	4	0.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.249
			1:WEIGHT	Max +ve	0	0.100
				Max -ve		
			10:WIND LOA	Max +ve	0	0
				Max -ve	0	0
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.133
			12:DYNO DRU	Max +ve	0	0.014
				Max -ve		
			16:WIND RES	Max +ve	0	0.103
				Max -ve		
			9:COMPRESS	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.213
				Max -ve		
			4:1.25DL	Max +ve	0	0.125
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.124
				Max -ve		
			6:CASE I: VX	Max +ve	0	0
				Max -ve	0	0
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.139
			8:CASE I: VY	Max +ve	0	0.100
				Max -ve		
			13:CASE III: V'	Max +ve	0	0.075235
				Max -ve		
			14:CASE III: V _i	Max +ve		
				Max -ve	0	-0.187
			15:CASE III:V _X	Max +ve	0	0.010
				Max -ve		
4	5	7.000	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.231
			1:WEIGHT	Max +ve	0	0.000
				Max -ve		
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			12:DYNO DRU	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0	-0.027
			16:WIND RESI	Max +ve	0	0.052
				Max -ve		
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0WI	Max +ve	0	0.052
				Max -ve		
			4:1.25DL	Max +ve	0	0.000
				Max -ve		
			5:1.1DL+1.0W)	Max +ve		
				Max -ve	0	-0.027
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0Wz	Max +ve		
				Max -ve	0	-0.231
			8:CASE I: VY	Max +ve	0	0.000
				Max -ve		
			13:CASE III: V'	Max +ve	0	0.000
				Max -ve		
			14:CASE III: Vz	Max +ve		
				Max -ve	0	-0.173
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.020
5	3	2.000	2:DYNO DRUM	Max +ve	0	0.078
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.011
			10:WIND LOAI	Max +ve		
				Max -ve	0	-0.022
			11:WIND LOAI	Max +ve	0	0.014
				Max -ve		
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.021
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.127
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0WI	Max +ve		
				Max -ve	0	-0.138
			4:1.25DL	Max +ve		
				Max -ve	0	-0.013
			5:1.1DL+1.0W)	Max +ve		
				Max -ve	0	-0.054
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.022



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			7:1.1DL+1.0Wz	Max +ve	0	0.065963
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.011
			13:CASE III: V'	Max +ve		
				Max -ve	0	-0.008
			14:CASE III: Vz	Max +ve	0	0.058
				Max -ve		
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.032
6	5	2.000	2:DYNO DRUM	Max +ve	0	0.078
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.011
			10:WIND LOA	Max +ve	0	0.022
				Max -ve		
			11:WIND LOA	Max +ve	0	0.014
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.021
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.024
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0Wf	Max +ve		
				Max -ve	0	-0.036
			4:1.25DL	Max +ve		
				Max -ve	0	-0.013
			5:1.1DL+1.0Wz	Max +ve	0	0.031
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.022
				Max -ve		
			7:1.1DL+1.0Wz	Max +ve	0	0.066
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.011
			13:CASE III: V'	Max +ve		
				Max -ve	0	-0.008
			14:CASE III: Vz	Max +ve	0	0.058
				Max -ve		
			15:CASE III:Vx	Max +ve	0	0.032
				Max -ve		
7	8	1.000	2:DYNO DRUM	Max +ve	0	0.084
				Max -ve		
			1:WEIGHT	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0	-0.001
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve	0	0.001
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.026
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.013
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.014
			4:1.25DL	Max +ve		
				Max -ve	0	-0.001
			5:1.1DL+1.0W	Max +ve	0	0.025
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve	0	0.083023
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.001
			13:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V	Max +ve	0	0.063
				Max -ve		
			15:CASE III:VX	Max +ve	0	0.019315
				Max -ve		
8	7	1.500	2:DYNO DRUM	Max +ve	0	0.366
				Max -ve		
			1:WEIGHT	Max +ve	0	0.972
				Max -ve		
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.026
			11:WIND LOA	Max +ve		
				Max -ve	0	-1.284
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.039
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.200
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.869
				Max -ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			4:1.25DL	Max +ve	0	1.215
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	1.004
				Max -ve		
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.026
			7:1.1DL+1.0W	Max +ve	0	1.434
				Max -ve		
			8:CASE I: VY	Max +ve	0	0.972
				Max -ve		
			13:CASE III: V	Max +ve	0	0.729
				Max -ve		
			14:CASE III: V	Max +ve	0	0.274
				Max -ve		
			15:CASE III: VX	Max +ve		
				Max -ve	0	-0.049
9	9	0.500	2:DYNO DRUM	Max +ve	0	0.236
				Max -ve		
			1:WEIGHT	Max +ve	0	0.732
				Max -ve		
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.967
			12:DYNO DRU	Max +ve	0	0.014
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.078
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.728
				Max -ve		
			4:1.25DL	Max +ve	0	0.915
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.819
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve	0	1.041
				Max -ve		
			8:CASE I: VY	Max +ve	0	0.732
				Max -ve		
			13:CASE III: V	Max +ve	0	0.549
				Max -ve		
			14:CASE III: V	Max +ve	0	0.177



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve		
			15:CASE III:Vx	Max +ve	0	0.010
				Max -ve		
10	10	7.000	2:DYNO DRUM	Max +ve	0	0.231
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.000
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOA	Max +ve	0	0.000
				Max -ve		
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.028
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.093
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.094
			4:1.25DL	Max +ve		
				Max -ve	0	-0.000
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.029
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve	0	0.231
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.000
			13:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V	Max +ve	0	0.173
				Max -ve		
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.021
11	7	0.670	2:DYNO DRUM	Max +ve	0	0.000
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0.670	-0.273
			10:WIND LOA	Max +ve	0	0.094
				Max -ve		
			11:WIND LOA	Max +ve	0	0.460
				Max -ve		
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.028



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			16:WIND RESI	Max +ve	0	0.055
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0.670	-0.246
			4:1.25DL	Max +ve		
				Max -ve	0.670	-0.342
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0.670	-0.234
			6:CASE I: VX	Max +ve	0	0.094
				Max -ve		
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0.670	-0.301
			8:CASE I: VY	Max +ve		
				Max -ve	0.670	-0.273
			13:CASE III: V	Max +ve		
				Max -ve	0.670	-0.205
			14:CASE III: V	Max +ve	0	0.000
				Max -ve		
			15:CASE III:VX	Max +ve	0	0.050
				Max -ve		
14	10	0.670	2:DYNO DRUM	Max +ve	0	0
				Max -ve	0	0
			1:WEIGHT	Max +ve		
				Max -ve	0.670	-0.273
			10:WIND LOAI	Max +ve		
				Max -ve	0	-0.094
			11:WIND LOAI	Max +ve	0	0.460
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.028
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.055
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0.670	-0.355
			4:1.25DL	Max +ve		
				Max -ve	0.670	-0.342
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0.670	-0.367
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.094
			7:1.1DL+1.0W	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0.670	-0.301
			8:CASE I: VY	Max +ve		
				Max -ve	0.670	-0.273
			13:CASE III: V'	Max +ve		
				Max -ve	0.670	-0.205
			14:CASE III: V _i	Max +ve	0	0
				Max -ve	0	0
			15:CASE III: V _x	Max +ve		
				Max -ve	0	-0.050
20	18	7.000	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.231
			1:WEIGHT	Max +ve	0	0.000
				Max -ve		
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			12:DYNO DRU	Max +ve	0	0.027
				Max -ve		
			16:WIND RESI	Max +ve	0	0.112
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.112
				Max -ve		
			4:1.25DL	Max +ve	0	0.000
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.027
				Max -ve		
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.231
			8:CASE I: VY	Max +ve	0	0.000
				Max -ve		
			13:CASE III: V'	Max +ve	0	0.000
				Max -ve		
			14:CASE III: V _i	Max +ve		
				Max -ve	0	-0.173
			15:CASE III: V _x	Max +ve	0	0.020
				Max -ve		
21	19	7.000	2:DYNO DRUM	Max +ve	0	0.231
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.000



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve	0	0.000
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.028
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.071
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.071
			4:1.25DL	Max +ve		
				Max -ve	0	-0.000
			5:1.1DL+1.0W	Max +ve	0	0.028
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve	0	0.231
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.000
			13:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V	Max +ve	0	0.173
				Max -ve		
			15:CASE III:VX	Max +ve	0	0.021
				Max -ve		
22	20	0.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.249
			1:WEIGHT	Max +ve	0	0.100
				Max -ve		
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.133
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.014
			16:WIND RESI	Max +ve	0	0.103
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.213
				Max -ve		
			4:1.25DL	Max +ve	0	0.125



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.096
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.139
			8:CASE I: VY	Max +ve	0	0.100
				Max -ve		
			13:CASE III: V	Max +ve	0	0.075235
				Max -ve		
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.187
			15:CASE III: VX	Max +ve		
				Max -ve	0	-0.010
23	21	0.500	2:DYNO DRUM	Max +ve	0	0.236
				Max -ve		
			1:WEIGHT	Max +ve	0	0.732
				Max -ve		
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.967
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.014
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.078
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.728
				Max -ve		
			4:1.25DL	Max +ve	0	0.915
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.791
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve	0	1.041
				Max -ve		
			8:CASE I: VY	Max +ve	0	0.732
				Max -ve		
			13:CASE III: V	Max +ve	0	0.549
				Max -ve		
			14:CASE III: V	Max +ve	0	0.177
				Max -ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.010
24	22	1.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.375
			1:WEIGHT	Max +ve	0	0.004
				Max -ve		
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.026
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.006
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.011
			16:WIND RES	Max +ve	0	0.097
				Max -ve		
			9:COMPRESS	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.102
				Max -ve		
			4:1.25DL	Max +ve	0	0.006
				Max -ve		
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.033
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.026
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.370
			8:CASE I: VY	Max +ve	0	0.004
				Max -ve		
			13:CASE III: V	Max +ve	0	0.003
				Max -ve		
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.281
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.028
25	23	1.500	2:DYNO DRUM	Max +ve	0	0.366
				Max -ve		
			1:WEIGHT	Max +ve	0	0.972
				Max -ve		
			10:WIND LOA	Max +ve	0	0.026
				Max -ve		
			11:WIND LOA	Max +ve		
				Max -ve	0	-1.284
			12:DYNO DRU	Max +ve	0	0.039
				Max -ve		
			16:WIND RES	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0	-0.072
			9:COMPRESSI	Max +ve		
				Max -ve	0	-0.000
			3:1.1DL+1.0W	Max +ve	0	0.996
				Max -ve		
			4:1.25DL	Max +ve	0	1.215
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	1.134
				Max -ve		
			6:CASE I: VX	Max +ve	0	0.026
				Max -ve		
			7:1.1DL+1.0W	Max +ve	0	1.434
				Max -ve		
			8:CASE I: VY	Max +ve	0	0.972
				Max -ve		
			13:CASE III: V	Max +ve	0	0.729
				Max -ve		
			14:CASE III: V	Max +ve	0	0.274
				Max -ve		
			15:CASE III:VX	Max +ve	0	0.049
				Max -ve		
26	24	1.000	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.084
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.000
			10:WIND LOA	Max +ve	0	0.000
				Max -ve		
			11:WIND LOA	Max +ve	0	0.001
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.000
				Max -ve		
			16:WIND RES	Max +ve	0	0.026
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.026
				Max -ve		
			4:1.25DL	Max +ve		
				Max -ve	0	-0.001
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.000
			6:CASE I: VX	Max +ve	0	0.000
				Max -ve		
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.084



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.000
			13:CASE III: V'	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V _i	Max +ve		
				Max -ve	0	-0.063
			15:CASE III:V _X	Max +ve	0	0.000
				Max -ve		
27	25	1.000	2:DYNO DRUM	Max +ve	0	0.084
				Max -ve		
			1:WEIGHT	Max +ve		
				Max -ve	0	-0.001
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOA	Max +ve	0	0.001
				Max -ve		
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.000
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.028
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.028
			4:1.25DL	Max +ve		
				Max -ve	0	-0.001
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.001
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve	0	0.083023
				Max -ve		
			8:CASE I: VY	Max +ve		
				Max -ve	0	-0.001
			13:CASE III: V'	Max +ve		
				Max -ve	0	-0.000
			14:CASE III: V _i	Max +ve	0	0.063
				Max -ve		
			15:CASE III:V _X	Max +ve		
				Max -ve	0	-0.000
28	26	2.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.000
			1:WEIGHT	Max +ve	0	0
				Max -ve	0	0
			10:WIND LOA	Max +ve	0	0



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0	0
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			12:DYNO DRU	Max +ve	0	0.000
				Max -ve		
			16:WIND RESI	Max +ve	0	0.000
				Max -ve		
			9:COMPRESSI	Max +ve	0	3.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0.000
				Max -ve		
			4:1.25DL	Max +ve	0	0
				Max -ve	0	0
			5:1.1DL+1.0W	Max +ve	0	0.000
				Max -ve		
			6:CASE I: VX	Max +ve	0	0
				Max -ve	0	0
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.000
			8:CASE I: VY	Max +ve	0	0
				Max -ve	0	0
			13:CASE III: V	Max +ve	0	0
				Max -ve	0	0
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			15:CASE III:VX	Max +ve	0	0.000
				Max -ve		
29	27	2.500	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.000
			1:WEIGHT	Max +ve	0	0
				Max -ve	0	0
			10:WIND LOA	Max +ve	0	0
				Max -ve	0	0
			11:WIND LOA	Max +ve	0	0
				Max -ve	0	0
			12:DYNO DRU	Max +ve	0	0
				Max -ve	0	0
			16:WIND RESI	Max +ve	0	0
				Max -ve	0	0
			9:COMPRESSI	Max +ve	0	3.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve	0	0
				Max -ve	0	0
			4:1.25DL	Max +ve	0	0
				Max -ve	0	0



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			5:1.1DL+1.0W	Max +ve	0	0
				Max -ve	0	0
			6:CASE I: VX	Max +ve	0	0
				Max -ve	0	0
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.000
			8:CASE I: VY	Max +ve	0	0
				Max -ve	0	0
			13:CASE III: V	Max +ve	0	0
				Max -ve	0	0
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			15:CASE III:VX	Max +ve	0	0
				Max -ve	0	0
30	3	1.000	2:DYNO DRUM	Max +ve	0	0
				Max -ve	0	0
			1:WEIGHT	Max +ve	0	0.000
				Max -ve		
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOA	Max +ve	0	0.000
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.000
				Max -ve		
			16:WIND RESI	Max +ve		
				Max -ve	0	-0.015
			9:COMPRESSI	Max +ve	0	0
				Max -ve	0	0
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.015
			4:1.25DL	Max +ve	0	0.000
				Max -ve		
			5:1.1DL+1.0W	Max +ve	0	0.000
				Max -ve		
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve	0	0.000
				Max -ve		
			8:CASE I: VY	Max +ve	0	0.000
				Max -ve		
			13:CASE III: V	Max +ve	0	0.000
				Max -ve		
			14:CASE III: V	Max +ve	0	0
				Max -ve	0	0
			15:CASE III:VX	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	0	-0.000
31	5	1.000	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.000
			1:WEIGHT	Max +ve	0	0
				Max -ve	0	0
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			11:WIND LOA	Max +ve		
				Max -ve	0	-0.000
			12:DYNO DRU	Max +ve	0	0
				Max -ve	0	0
			16:WIND RES	Max +ve		
				Max -ve	0	-0.015
			9:COMPRESS	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.015
			4:1.25DL	Max +ve	0	0
				Max -ve	0	0
			5:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.000
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.000
			7:1.1DL+1.0W	Max +ve		
				Max -ve	0	-0.000
			8:CASE I: VY	Max +ve	0	0
				Max -ve	0	0
			13:CASE III: V	Max +ve	0	0
				Max -ve	0	0
			14:CASE III: V	Max +ve		
				Max -ve	0	-0.000
			15:CASE III:VX	Max +ve		
				Max -ve	0	-0.000
32	15	4.830	2:DYNO DRUM	Max +ve		
				Max -ve	0	-0.000
			1:WEIGHT	Max +ve		
				Max -ve	4.830	-0.321
			10:WIND LOA	Max +ve		
				Max -ve	0	-0.094
			11:WIND LOA	Max +ve	0	0.460
				Max -ve		
			12:DYNO DRU	Max +ve	0	0.028
				Max -ve		
			16:WIND RES	Max +ve		
				Max -ve	0	-0.055



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0Wf	Max +ve		
				Max -ve	4.830	-0.408
			4:1.25DL	Max +ve		
				Max -ve	4.830	-0.402
			5:1.1DL+1.0W)	Max +ve		
				Max -ve	4.830	-0.420
			6:CASE I: VX	Max +ve		
				Max -ve	0	-0.094
			7:1.1DL+1.0Wz	Max +ve		
				Max -ve	4.830	-0.353
			8:CASE I: VY	Max +ve		
				Max -ve	4.830	-0.321
			13:CASE III: V'	Max +ve		
				Max -ve	4.830	-0.241
			14:CASE III: Vz	Max +ve		
				Max -ve	0	-0.000
			15:CASE III:Vx	Max +ve		
				Max -ve	0	-0.050
33	12	4.830	2:DYNO DRUM	Max +ve	0	0
				Max -ve	0	0
			1:WEIGHT	Max +ve		
				Max -ve	4.830	-0.321
			10:WIND LOAI	Max +ve	0	0.094
				Max -ve		
			11:WIND LOAI	Max +ve	0	0.460
				Max -ve		
			12:DYNO DRU	Max +ve		
				Max -ve	0	-0.028
			16:WIND RESI	Max +ve	0	0.055
				Max -ve		
			9:COMPRESSI	Max +ve	0	0.000
				Max -ve		
			3:1.1DL+1.0Wf	Max +ve		
				Max -ve	4.830	-0.299
			4:1.25DL	Max +ve		
				Max -ve	4.830	-0.402
			5:1.1DL+1.0W)	Max +ve		
				Max -ve	4.830	-0.287
			6:CASE I: VX	Max +ve	0	0.094
				Max -ve		
			7:1.1DL+1.0Wz	Max +ve		
				Max -ve	4.830	-0.353
			8:CASE I: VY	Max +ve		



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Beam Maximum Axial Forces Cont...

Beam	Node A	Length (ft)	L/C		d (ft)	Max Fx (kip)
				Max -ve	4.830	-0.321
			13:CASE III: V'	Max +ve		
				Max -ve	4.830	-0.241
			14:CASE III: V _i	Max +ve	0	0
				Max -ve	0	0
			15:CASE III: V _X	Max +ve	0	0.050
				Max -ve		

Beam Maximum Forces by Section Property

Section		Axial			Shear		Torsion	Bending	
		Max Fx (kip)	Max Fy (kip)	Max Fz (kip)	Max Mx (kip-in)	Max My (kip-in)	Max Mz (kip-in)		
HSST3X3X0.188	Max +ve	1.434	0.347	0.179	6.427	2.150	9.808		
	Max -ve	-1.284	-0.340	-0.179	-7.549	-2.252	-10.999		
HSST3.5X3.5X0.25	Max +ve	3.000	1.290	0.206	8.964	25.560	33.470		
	Max -ve	-0.420	-1.290	-0.157	-7.923	-20.963	-39.360		

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	2:DYNO DRUM	1.000	808.023	1.000	2	-896.777	1.000	1
	1:WEIGHT	1.000	213.567	1.000	3	-214.042	1.000	1
	10:WIND LOAL	1.000	4.584	1.000	3	-4.826	1.000	1
	11:WIND LOAL	1.000	35.503	0	1	-34.876	0	3
	12:DYNO DRU	1.000	20.377	1.000	2			
	16:WIND RESI	1.000	360.562	1.000	1	-304.328	1.000	2
	9:COMPRESSI	1.000	0.000	1.000	3	-0.000	1.000	1
	3:1.1DL+1.0W _i	1.000	595.486	1.000	4	-539.774	1.000	2
	4:1.25DL	1.000	266.959	1.000	3	-267.552	1.000	1
	5:1.1DL+1.0W _j	1.000	257.192	1.000	3	-231.068	1.000	1
	6:CASE I: V _X	1.000	4.584	1.000	3	-4.826	1.000	1
	7:1.1DL+1.0W _z	1.000	1.04E+3	1.000	3	-1.13E+3	1.000	1
	8:CASE I: V _Y	1.000	213.567	1.000	3	-214.042	1.000	1
	13:CASE III: V'	1.000	160.175	1.000	3	-160.531	1.000	1
	14:CASE III: V _i	1.000	606.017	1.000	2	-672.582	1.000	1
15:CASE III: V _X	1.000	18.344	1.000	3				
2	2:DYNO DRUM	1.500	372.927	0	1	-770.020	0	2
	1:WEIGHT	1.500	1.25E+3	0	1	-1.24E+3	0	3
	10:WIND LOAL	1.500	639.564	0	3	-611.547	0	1
	11:WIND LOAL	1.500	2.15E+3	0	3	-2.16E+3	0	1
	12:DYNO DRU	1.500	175.047	0	2	-163.347	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	16:WIND RESI	1.500	649.102	0	2	-455.636	0	1
	9:COMPRESSI	1.500	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0Wf	1.500	1.77E+3	0	1	-1.57E+3	0	3
	4:1.25DL	1.500	1.56E+3	0	1	-1.55E+3	0	3
	5:1.1DL+1.0Wj	1.500	1.26E+3	1.500	4	-1.22E+3	1.500	2
	6:CASE I: VX	1.500	639.564	0	3	-611.547	0	1
	7:1.1DL+1.0Wz	1.500	1.74E+3	0	1	-2.14E+3	0	3
	8:CASE I: VY	1.500	1.25E+3	0	1	-1.24E+3	0	3
	13:CASE III: V'	1.500	934.913	0	1	-931.373	0	3
	14:CASE III: Vz	1.500	279.695	0	1	-577.515	0	2
	15:CASE III: VX	1.500	539.802	0	3	-510.014	0	1
3	2:DYNO DRUM	0.500				-258.921	0.500	2
	1:WEIGHT	0.500	2.29E+3	0.500	3	-2.19E+3	0.500	1
	10:WIND LOAL	0.500	232.567	0.500	2	-232.567	0.500	4
	11:WIND LOAL	0.500	3.05E+3	0.500	1	-3.19E+3	0.500	3
	12:DYNO DRU	0.500	125.081	0.500	3	-110.417	0.500	1
	16:WIND RESI	0.500	343.758	0.500	2	-235.072	0.500	4
	9:COMPRESSI	0.500	0.000	0.500	1	-0.000	0.500	3
	3:1.1DL+1.0Wf	0.500	2.79E+3	0.500	3	-2.57E+3	0.500	1
	4:1.25DL	0.500	2.87E+3	0.500	3	-2.74E+3	0.500	1
	5:1.1DL+1.0Wj	0.500	2.64E+3	0.500	3	-2.51E+3	0.500	1
	6:CASE I: VX	0.500	232.567	0.500	2	-232.567	0.500	4
	7:1.1DL+1.0Wz	0.500	2.44E+3	0.500	3	-2.59E+3	0.500	1
	8:CASE I: VY	0.500	2.29E+3	0.500	3	-2.19E+3	0.500	1
	13:CASE III: V'	0.500	1.72E+3	0.500	3	-1.64E+3	0.500	1
	14:CASE III: Vz	0.500				-194.191	0.500	2
	15:CASE III: VX	0.500	250.746	0.500	2	-239.748	0.500	4
4	2:DYNO DRUM	7.000	1.3E+3	0	1	-1.55E+3	0	2
	1:WEIGHT	7.000	3.82E+3	0	3	-3.82E+3	0	1
	10:WIND LOAL	7.000	101.440	0	1	-101.076	0	3
	11:WIND LOAL	7.000	5.07E+3	0	1	-5.07E+3	0	3
	12:DYNO DRU	7.000				-26.640	0	1
	16:WIND RESI	7.000	597.088	0	2	-542.405	0	1
	9:COMPRESSI	7.000	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0Wf	7.000	4.74E+3	0	3	-4.69E+3	0	1
	4:1.25DL	7.000	4.77E+3	0	3	-4.77E+3	0	1
	5:1.1DL+1.0Wj	7.000	4.09E+3	0	3	-4.12E+3	0	1
	6:CASE I: VX	7.000	101.440	0	1	-101.076	0	3
	7:1.1DL+1.0Wz	7.000	5.49E+3	0	3	-5.73E+3	0	1
	8:CASE I: VY	7.000	3.82E+3	0	3	-3.82E+3	0	1
	13:CASE III: V'	7.000	2.86E+3	0	3	-2.86E+3	0	1
	14:CASE III: Vz	7.000	975.742	0	1	-1.16E+3	0	2
	15:CASE III: VX	7.000	60.371	0	1	-81.801	0	3
5	2:DYNO DRUM	2.000	899.971	2.000	2	-846.659	2.000	4



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	1:WEIGHT	2.000	1.78E+3	2.000	1	-1.79E+3	2.000	3
	10:WIND LOAL	2.000	700.758	2.000	3	-715.738	2.000	1
	11:WIND LOAL	2.000	2.31E+3	2.000	3	-2.3E+3	2.000	1
	12:DYNO DRU	2.000	151.032	2.000	2	-165.282	2.000	4
	16:WIND RESI	2.000	254.507	2.000	4	-341.616	2.000	2
	9:COMPRESSI	2.000	0.000	2.000	3	-0.000	2.000	1
	3:1.1DL+1.0Wf	2.000	1.81E+3	2.000	1	-1.9E+3	2.000	3
	4:1.25DL	2.000	2.23E+3	2.000	1	-2.24E+3	2.000	3
	5:1.1DL+1.0Wj	2.000	1.49E+3	2.000	2	-1.53E+3	2.000	4
	6:CASE I: VX	2.000	700.758	2.000	3	-715.738	2.000	1
	7:1.1DL+1.0Wz	2.000	2.8E+3	2.000	2	-2.75E+3	2.000	4
	8:CASE I: VY	2.000	1.78E+3	2.000	1	-1.79E+3	2.000	3
	13:CASE III: V'	2.000	1.34E+3	2.000	1	-1.34E+3	2.000	3
	14:CASE III: Vz	2.000	674.978	2.000	2	-634.994	2.000	4
	15:CASE III: VX	2.000	504.164	2.000	3	-526.086	2.000	1
6	2:DYNO DRUM	2.000	900.192	2.000	4	-846.880	2.000	2
	1:WEIGHT	2.000	4.09E+3	2.000	3	-4.1E+3	2.000	1
	10:WIND LOAL	2.000	715.738	2.000	2	-700.758	2.000	4
	11:WIND LOAL	2.000	6.34E+3	2.000	1	-6.33E+3	2.000	3
	12:DYNO DRU	2.000	165.089	2.000	3	-150.891	2.000	1
	16:WIND RESI	2.000	585.376	2.000	2	-601.798	2.000	4
	9:COMPRESSI	2.000	0.000	2.000	1	-0.000	2.000	3
	3:1.1DL+1.0Wf	2.000	4.68E+3	2.000	3	-4.7E+3	2.000	1
	4:1.25DL	2.000	5.12E+3	2.000	3	-5.13E+3	2.000	1
	5:1.1DL+1.0Wj	2.000	4.13E+3	2.000	3	-4.11E+3	2.000	1
	6:CASE I: VX	2.000	715.738	2.000	2	-700.758	2.000	4
	7:1.1DL+1.0Wz	2.000	5.34E+3	2.000	4	-5.29E+3	2.000	2
	8:CASE I: VY	2.000	4.09E+3	2.000	3	-4.1E+3	2.000	1
	13:CASE III: V'	2.000	3.07E+3	2.000	3	-3.08E+3	2.000	1
	14:CASE III: Vz	2.000	675.144	2.000	4	-635.160	2.000	2
	15:CASE III: VX	2.000	525.942	2.000	2	-504.058	2.000	4
7	2:DYNO DRUM	1.000	897.537	1.000	2	-809.062	1.000	1
	1:WEIGHT	1.000	290.880	1.000	3	-291.444	1.000	1
	10:WIND LOAL	1.000	6.556	1.000	2	-6.526	1.000	4
	11:WIND LOAL	1.000	131.822	1.000	1	-131.077	1.000	3
	12:DYNO DRU	1.000	19.731	0	1			
	16:WIND RESI	1.000	334.522	1.000	1	-348.459	1.000	2
	9:COMPRESSI	1.000	0.000	1.000	1	-0.000	1.000	3
	3:1.1DL+1.0Wf	1.000	652.020	1.000	4	-666.576	1.000	2
	4:1.25DL	1.000	363.601	1.000	3	-364.305	1.000	1
	5:1.1DL+1.0Wj	1.000	330.205	1.000	3	-303.573	1.000	1
	6:CASE I: VX	1.000	6.556	1.000	2	-6.526	1.000	4
	7:1.1DL+1.0Wz	1.000	1.22E+3	1.000	3	-1.13E+3	1.000	1
	8:CASE I: VY	1.000	290.880	1.000	3	-291.444	1.000	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	13:CASE III: V'	1.000	218.160	1.000	3	-218.583	1.000	1
	14:CASE III: V _z	1.000	673.153	1.000	2	-606.797	1.000	1
	15:CASE III: VX	1.000	16.464	0	1			
8	2:DYNO DRUM	1.500	819.536	0	1	-432.734	0	2
	1:WEIGHT	1.500	4.2E+3	0	3	-3.18E+3	0	1
	10:WIND LOAL	1.500	2E+3	0	1	-2.03E+3	0	3
	11:WIND LOAL	1.500	4.59E+3	0	1	-5.94E+3	0	3
	12:DYNO DRU	1.500	558.154	0	3	-599.239	0	1
	16:WIND RESI	1.500	1.23E+3	0	1	-1.44E+3	0	3
	9:COMPRESSI	1.500	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0W _i	1.500	3.85E+3	0	3	-2.93E+3	0	1
	4:1.25DL	1.500	5.25E+3	0	3	-3.97E+3	0	1
	5:1.1DL+1.0W _j	1.500	3.31E+3	0	3	-2.24E+3	0	1
	6:CASE I: VX	1.500	2E+3	0	1	-2.03E+3	0	3
	7:1.1DL+1.0W _z	1.500	5.44E+3	0	3	-3.93E+3	0	1
	8:CASE I: VY	1.500	4.2E+3	0	3	-3.18E+3	0	1
	13:CASE III: V'	1.500	3.15E+3	0	3	-2.38E+3	0	1
	14:CASE III: V _z	1.500	614.652	0	1	-324.550	0	2
	15:CASE III: VX	1.500	1.24E+3	0	1	-1.29E+3	0	3
9	2:DYNO DRUM	0.500	212.591	0	1			
	1:WEIGHT	0.500	866.667	0.500	1	-92.067	0.500	3
	10:WIND LOAL	0.500	581.498	0.500	3	-581.498	0.500	1
	11:WIND LOAL	0.500	192.594	0.500	3	-1.22E+3	0.500	1
	12:DYNO DRU	0.500	227.558	0.500	2	-212.894	0.500	4
	16:WIND RESI	0.500	425.346	0.500	3	-507.547	0.500	1
	9:COMPRESSI	0.500	0.000	0.500	3	-0.000	0.500	1
	3:1.1DL+1.0W _i	0.500	810.237	0	1	-40.378	0	2
	4:1.25DL	0.500	1.08E+3	0.500	1	-115.083	0.500	3
	5:1.1DL+1.0W _j	0.500	868.021	0	1	-1.297	0	2
	6:CASE I: VX	0.500	581.498	0.500	3	-581.498	0.500	1
	7:1.1DL+1.0W _z	0.500	1.16E+3	0.500	1	-56.186	0.500	3
	8:CASE I: VY	0.500	866.667	0.500	1	-92.067	0.500	3
	13:CASE III: V'	0.500	650.000	0.500	1	-69.050	0.500	3
	14:CASE III: V _z	0.500	159.443	0	1			
	15:CASE III: VX	0.500	436.207	0.500	3	-425.209	0.500	1
10	2:DYNO DRUM	7.000	1.55E+3	0	1	-1.3E+3	0	2
	1:WEIGHT	7.000	3.37E+3	0	3	-3.37E+3	0	1
	10:WIND LOAL	7.000	98.654	0	3	-99.018	0	1
	11:WIND LOAL	7.000	4.31E+3	0	1	-4.31E+3	0	3
	12:DYNO DRU	7.000				-27.613	0	1
	16:WIND RESI	7.000	507.675	0	2	-606.505	0	1
	9:COMPRESSI	7.000	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0W _i	7.000	4.21E+3	0	3	-4.3E+3	0	1
	4:1.25DL	7.000	4.22E+3	0	3	-4.22E+3	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	5:1.1DL+1.0W ₂	7.000	3.79E+3	0	3	-3.82E+3	0	1
	6:CASE I: VX	7.000	98.654	0	3	-99.018	0	1
	7:1.1DL+1.0W ₂	7.000	5.14E+3	0	3	-4.9E+3	0	1
	8:CASE I: VY	7.000	3.37E+3	0	3	-3.37E+3	0	1
	13:CASE III: V ₁	7.000	2.53E+3	0	3	-2.53E+3	0	1
	14:CASE III: V ₂	7.000	1.16E+3	0	1	-977.317	0	2
	15:CASE III: VX	7.000	58.337	0	3	-80.987	0	1
11	2:DYNO DRUM	0.670	464.323	0	2	-464.323	0	1
	1:WEIGHT	0.670	6.11E+3	0	2	-6.29E+3	0	1
	10:WIND LOAL	0.670	1.99E+3	0.670	4	-1.92E+3	0.670	2
	11:WIND LOAL	0.670	8.55E+3	0	1	-8.23E+3	0	2
	12:DYNO DRU	0.670	397.413	0	1	-416.594	0	3
	16:WIND RESI	0.670	958.260	0.670	3	-920.721	0.670	1
	9:COMPRESSI	0.670	0.000	0.670	1	-0.000	0.670	3
	3:1.1DL+1.0W ₁	0.670	6.81E+3	0	3	-6.98E+3	0	1
	4:1.25DL	0.670	7.64E+3	0	2	-7.86E+3	0	1
	5:1.1DL+1.0W ₂	0.670	6.36E+3	0	3	-6.52E+3	0	1
	6:CASE I: VX	0.670	1.99E+3	0.670	4	-1.92E+3	0.670	2
	7:1.1DL+1.0W ₂	0.670	7.13E+3	0	2	-7.33E+3	0	1
	8:CASE I: VY	0.670	6.11E+3	0	2	-6.29E+3	0	1
	13:CASE III: V ₁	0.670	4.58E+3	0	2	-4.72E+3	0	1
	14:CASE III: V ₂	0.670	348.242	0	2	-348.242	0	1
	15:CASE III: VX	0.670	1.26E+3	0.670	4	-1.23E+3	0.670	2
14	2:DYNO DRUM	0.670	874.350	0.670	1	-874.350	0.670	2
	1:WEIGHT	0.670	8.46E+3	0	1	-8.64E+3	0	2
	10:WIND LOAL	0.670	1.92E+3	0.670	3	-1.99E+3	0.670	1
	11:WIND LOAL	0.670	12.6E+3	0	2	-12.3E+3	0	1
	12:DYNO DRU	0.670	416.595	0	1	-397.414	0	3
	16:WIND RESI	0.670	1.15E+3	0.670	3	-1.19E+3	0.670	1
	9:COMPRESSI	0.670	0.000	0.670	2	-0.000	0.670	4
	3:1.1DL+1.0W ₁	0.670	8.45E+3	0	1	-8.69E+3	0	2
	4:1.25DL	0.670	10.6E+3	0	1	-10.8E+3	0	2
	5:1.1DL+1.0W ₂	0.670	7.79E+3	0	1	-8.04E+3	0	2
	6:CASE I: VX	0.670	1.92E+3	0.670	3	-1.99E+3	0.670	1
	7:1.1DL+1.0W ₂	0.670	9.71E+3	0	1	-9.91E+3	0	2
	8:CASE I: VY	0.670	8.46E+3	0	1	-8.64E+3	0	2
	13:CASE III: V ₁	0.670	6.34E+3	0	1	-6.48E+3	0	2
	14:CASE III: V ₂	0.670	655.762	0.670	1	-655.762	0.670	2
	15:CASE III: VX	0.670	1.23E+3	0.670	3	-1.26E+3	0.670	1
20	2:DYNO DRUM	7.000	1.29E+3	7.000	1	-1.54E+3	7.000	2
	1:WEIGHT	7.000	2.63E+3	7.000	3	-2.63E+3	7.000	1
	10:WIND LOAL	7.000	101.076	7.000	3	-101.440	7.000	1
	11:WIND LOAL	7.000	3.33E+3	7.000	1	-3.33E+3	7.000	3
	12:DYNO DRU	7.000	27.241	7.000	2			



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	16:WIND RESI	7.000	626.343	7.000	2	-507.442	7.000	1
	9:COMPRESSI	7.000	0.000	7.000	3	-0.000	7.000	1
	3:1.1DL+1.0Wf	7.000	3.52E+3	7.000	3	-3.4E+3	7.000	1
	4:1.25DL	7.000	3.29E+3	7.000	3	-3.29E+3	7.000	1
	5:1.1DL+1.0Wj	7.000	3.01E+3	7.000	3	-2.98E+3	7.000	1
	6:CASE I: VX	7.000	101.076	7.000	3	-101.440	7.000	1
	7:1.1DL+1.0Wz	7.000	4.08E+3	7.000	4	-4.32E+3	7.000	2
	8:CASE I: VY	7.000	2.63E+3	7.000	3	-2.63E+3	7.000	1
	13:CASE III: V'	7.000	1.97E+3	7.000	3	-1.97E+3	7.000	1
	14:CASE III: Vz	7.000	970.330	7.000	1	-1.15E+3	7.000	2
	15:CASE III: VX	7.000	82.251	7.000	3	-60.821	7.000	1
21	2:DYNO DRUM	7.000	1.54E+3	7.000	1	-1.3E+3	7.000	2
	1:WEIGHT	7.000	4.56E+3	7.000	3	-4.56E+3	7.000	1
	10:WIND LOAI	7.000	99.018	7.000	1	-98.654	7.000	3
	11:WIND LOAI	7.000	6.05E+3	7.000	1	-6.05E+3	7.000	3
	12:DYNO DRU	7.000	27.013	7.000	3			
	16:WIND RESI	7.000	545.005	7.000	2	-619.758	7.000	1
	9:COMPRESSI	7.000	0.000	7.000	1	-0.000	7.000	3
	3:1.1DL+1.0Wf	7.000	5.5E+3	7.000	3	-5.57E+3	7.000	1
	4:1.25DL	7.000	5.7E+3	7.000	3	-5.7E+3	7.000	1
	5:1.1DL+1.0Wj	7.000	4.94E+3	7.000	3	-4.91E+3	7.000	1
	6:CASE I: VX	7.000	99.018	7.000	1	-98.654	7.000	3
	7:1.1DL+1.0Wz	7.000	6.55E+3	7.000	4	-6.31E+3	7.000	2
	8:CASE I: VY	7.000	4.56E+3	7.000	3	-4.56E+3	7.000	1
	13:CASE III: V'	7.000	3.42E+3	7.000	3	-3.42E+3	7.000	1
	14:CASE III: Vz	7.000	1.16E+3	7.000	1	-971.905	7.000	2
	15:CASE III: VX	7.000	80.537	7.000	2	-57.887	7.000	4
22	2:DYNO DRUM	0.500				-222.179	0	1
	1:WEIGHT	0.500	1.5E+3	0.500	3	-1.4E+3	0.500	1
	10:WIND LOAI	0.500	232.567	0	3	-232.567	0	1
	11:WIND LOAI	0.500	1.95E+3	0.500	1	-2.09E+3	0.500	3
	12:DYNO DRU	0.500	110.404	0	1	-125.127	0	2
	16:WIND RESI	0.500	322.844	0	1	-214.157	0	2
	9:COMPRESSI	0.500	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0Wf	0.500	1.71E+3	0.500	3	-1.48E+3	0.500	1
	4:1.25DL	0.500	1.88E+3	0.500	3	-1.75E+3	0.500	1
	5:1.1DL+1.0Wj	0.500	1.65E+3	0.500	3	-1.55E+3	0.500	1
	6:CASE I: VX	0.500	232.567	0	3	-232.567	0	1
	7:1.1DL+1.0Wz	0.500	1.6E+3	0.500	3	-1.74E+3	0.500	1
	8:CASE I: VY	0.500	1.5E+3	0.500	3	-1.4E+3	0.500	1
	13:CASE III: V'	0.500	1.13E+3	0.500	3	-1.05E+3	0.500	1
	14:CASE III: Vz	0.500				-166.634	0	1
	15:CASE III: VX	0.500	239.737	0	1	-250.778	0	2
23	2:DYNO DRUM	0.500	262.766	0	1	-12.859	0	2



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	1:WEIGHT	0.500	1.6E+3	0	3	-827.225	0	1
	10:WIND LOA	0.500	581.498	0	1	-581.498	0	3
	11:WIND LOA	0.500	1.25E+3	0	1	-2.27E+3	0	3
	12:DYNO DRU	0.500	212.848	0	4	-227.571	0	1
	16:WIND RES	0.500	448.937	0	1	-531.138	0	2
	9:COMPRESS	0.500	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0W	0.500	1.73E+3	0	3	-958.821	0	1
	4:1.25DL	0.500	2E+3	0	3	-1.03E+3	0	1
	5:1.1DL+1.0W	0.500	1.62E+3	0	3	-779.673	0	1
	6:CASE I: VX	0.500	581.498	0	1	-581.498	0	3
	7:1.1DL+1.0W	0.500	2.02E+3	0	3	-922.807	0	1
	8:CASE I: VY	0.500	1.6E+3	0	3	-827.225	0	1
	13:CASE III: V	0.500	1.2E+3	0	3	-620.419	0	1
	14:CASE III: V	0.500	197.074	0	1	-9.644	0	2
	15:CASE III: VX	0.500	425.177	0	1	-436.219	0	3
24	2:DYNO DRUM	1.500	409.001	1.500	4	-806.095	1.500	2
	1:WEIGHT	1.500	4.79E+3	1.500	3	-4.79E+3	1.500	1
	10:WIND LOA	1.500	611.547	1.500	1	-639.564	1.500	3
	11:WIND LOA	1.500	6.71E+3	1.500	1	-6.72E+3	1.500	3
	12:DYNO DRU	1.500	163.040	1.500	4	-174.739	1.500	2
	16:WIND RES	1.500	379.521	1.500	1	-277.027	1.500	3
	9:COMPRESS	1.500	0.000	1.500	1	-0.000	1.500	3
	3:1.1DL+1.0W	1.500	5.39E+3	1.500	4	-5.28E+3	1.500	2
	4:1.25DL	1.500	5.99E+3	1.500	3	-5.99E+3	1.500	1
	5:1.1DL+1.0W	1.500	5.06E+3	1.500	4	-5.09E+3	1.500	2
	6:CASE I: VX	1.500	611.547	1.500	1	-639.564	1.500	3
	7:1.1DL+1.0W	1.500	5.68E+3	1.500	4	-6.07E+3	1.500	2
	8:CASE I: VY	1.500	4.79E+3	1.500	3	-4.79E+3	1.500	1
	13:CASE III: V	1.500	3.6E+3	1.500	3	-3.59E+3	1.500	1
	14:CASE III: V	1.500	306.751	1.500	4	-604.571	1.500	2
	15:CASE III: VX	1.500	509.785	1.500	1	-539.572	1.500	3
25	2:DYNO DRUM	1.500	760.263	1.500	1	-373.460	1.500	3
	1:WEIGHT	1.500	2.96E+3	1.500	1	-1.93E+3	1.500	3
	10:WIND LOA	1.500	2.03E+3	1.500	4	-2E+3	1.500	2
	11:WIND LOA	1.500	3.06E+3	1.500	3	-4.42E+3	1.500	1
	12:DYNO DRU	1.500	599.547	1.500	1	-558.461	1.500	3
	16:WIND RES	1.500	1.02E+3	1.500	4	-1.1E+3	1.500	2
	9:COMPRESS	1.500	0.000	1.500	3	-0.000	1.500	1
	3:1.1DL+1.0W	1.500	2.46E+3	1.500	1	-1.4E+3	1.500	3
	4:1.25DL	1.500	3.7E+3	1.500	1	-2.42E+3	1.500	3
	5:1.1DL+1.0W	1.500	2.14E+3	1.500	1	-938.302	1.500	3
	6:CASE I: VX	1.500	2.03E+3	1.500	4	-2E+3	1.500	2
	7:1.1DL+1.0W	1.500	4.02E+3	1.500	1	-2.5E+3	1.500	3
	8:CASE I: VY	1.500	2.96E+3	1.500	1	-1.93E+3	1.500	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	13:CASE III: V ₁	1.500	2.22E+3	1.500	1	-1.45E+3	1.500	3
	14:CASE III: V ₂	1.500	570.197	1.500	1	-280.095	1.500	3
	15:CASE III: VX	1.500	1.29E+3	1.500	4	-1.24E+3	1.500	2
26	2:DYNO DRUM	1.000	808.316	0	2	-897.070	0	1
	1:WEIGHT	1.000	255.049	0	3	-255.524	0	1
	10:WIND LOAL	1.000	4.826	0	1	-4.584	0	3
	11:WIND LOAL	1.000	83.151	0	1	-82.524	0	3
	12:DYNO DRU	1.000	2.370	0	1	-2.238	0	2
	16:WIND RESI	1.000	360.260	0	1	-332.245	0	2
	9:COMPRESSI	1.000	0.000	0	1	-0.000	0	3
	3:1.1DL+1.0W ₁	1.000	639.291	0	1	-611.797	0	2
	4:1.25DL	1.000	318.812	0	3	-319.405	0	1
	5:1.1DL+1.0W ₂	1.000	281.424	0	3	-281.572	0	1
	6:CASE I: VX	1.000	4.826	0	1	-4.584	0	3
	7:1.1DL+1.0W ₂	1.000	1.09E+3	0	2	-1.18E+3	0	1
	8:CASE I: VY	1.000	255.049	0	3	-255.524	0	1
	13:CASE III: V ₁	1.000	191.287	0	3	-191.643	0	1
	14:CASE III: V ₂	1.000	606.237	0	2	-672.802	0	1
	15:CASE III: VX	1.000	5.020	0	1	-4.739	0	2
27	2:DYNO DRUM	1.000	897.830	0	2	-809.355	0	1
	1:WEIGHT	1.000	235.561	0	3	-236.125	0	1
	10:WIND LOAL	1.000	6.526	0	3	-6.556	0	1
	11:WIND LOAL	1.000	50.503	0	1	-49.758	0	3
	12:DYNO DRU	1.000	2.399	0	1	-2.602	0	2
	16:WIND RESI	1.000	331.171	0	1	-360.384	0	2
	9:COMPRESSI	1.000	0.000	0	3	-0.000	0	1
	3:1.1DL+1.0W ₁	1.000	590.288	0	1	-620.122	0	2
	4:1.25DL	1.000	294.451	0	3	-295.156	0	1
	5:1.1DL+1.0W ₂	1.000	267.020	0	3	-267.873	0	1
	6:CASE I: VX	1.000	6.526	0	3	-6.556	0	1
	7:1.1DL+1.0W ₂	1.000	1.15E+3	0	2	-1.06E+3	0	1
	8:CASE I: VY	1.000	235.561	0	3	-236.125	0	1
	13:CASE III: V ₁	1.000	176.671	0	3	-177.094	0	1
	14:CASE III: V ₂	1.000	673.373	0	2	-607.016	0	1
	15:CASE III: VX	1.000	5.927	0	3	-6.101	0	1
28	2:DYNO DRUM	2.500				-0.000	2.292	1
	1:WEIGHT	2.500	3.47E+3	0	1	-3.47E+3	0	3
	10:WIND LOAL	2.500	982.292	0	3	-982.292	0	1
	11:WIND LOAL	2.500	4.79E+3	0	3	-4.79E+3	0	1
	12:DYNO DRU	2.500	290.717	0	1	-290.717	0	3
	16:WIND RESI	2.500	568.945	0	3	-568.945	0	1
	9:COMPRESSI	2.500	1.03E+3	0	1			
	3:1.1DL+1.0W ₁	2.500	3.25E+3	0	1	-3.25E+3	0	3
	4:1.25DL	2.500	4.34E+3	0	1	-4.34E+3	0	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	5:1.1DL+1.0W ₂	2.500	3.13E+3	0	1	-3.13E+3	0	3
	6:CASE I: VX	2.500	982.292	0	3	-982.292	0	1
	7:1.1DL+1.0W ₂	2.500	3.82E+3	0	1	-3.82E+3	0	3
	8:CASE I: VY	2.500	3.47E+3	0	1	-3.47E+3	0	3
	13:CASE III: V'	2.500	2.61E+3	0	1	-2.61E+3	0	3
	14:CASE III: V ₂	2.500				-0.000	2.292	1
	15:CASE III: VX	2.500	518.681	0	3	-518.681	0	1
29	2:DYNO DRUM	2.500	874.350	2.292	3	-874.350	2.292	1
	1:WEIGHT	2.500	9.3E+3	2.500	3	-9.3E+3	2.500	1
	10:WIND LOAL	2.500	982.292	0	1	-982.292	0	3
	11:WIND LOAL	2.500	13.7E+3	2.500	1	-13.7E+3	2.500	3
	12:DYNO DRU	2.500	290.717	0	3	-290.717	0	1
	16:WIND RESI	2.500	910.312	2.500	3	-910.312	2.500	1
	9:COMPRESSI	2.500	1.03E+3	0	1			
	3:1.1DL+1.0W ₁	2.500	11.1E+3	2.500	3	-11.1E+3	2.500	1
	4:1.25DL	2.500	11.6E+3	2.500	3	-11.6E+3	2.500	1
	5:1.1DL+1.0W ₂	2.500	10.2E+3	2.500	3	-10.2E+3	2.500	1
	6:CASE I: VX	2.500	982.292	0	1	-982.292	0	3
	7:1.1DL+1.0W ₂	2.500	11.1E+3	2.500	3	-11.1E+3	2.500	1
	8:CASE I: VY	2.500	9.3E+3	2.500	3	-9.3E+3	2.500	1
	13:CASE III: V'	2.500	6.97E+3	2.500	3	-6.97E+3	2.500	1
	14:CASE III: V ₂	2.500	655.763	2.292	3	-655.763	2.292	1
	15:CASE III: VX	2.500	518.681	0	1	-518.681	0	3
30	2:DYNO DRUM	1.000	0.000	1.000	1	-0.000	1.000	3
	1:WEIGHT	1.000	20.588	0	3	-20.588	0	1
	10:WIND LOAL	1.000	41.667	0	1	-41.667	0	2
	11:WIND LOAL	1.000	41.666	0	1	-41.666	0	3
	12:DYNO DRU	1.000	0.000	0	1	-0.000	0	3
	16:WIND RESI	1.000	56.769	0	1	-66.975	0	2
	9:COMPRESSI	1.000	0.000	1.000	3	-0.000	1.000	1
	3:1.1DL+1.0W ₁	1.000	79.416	0	1	-89.621	0	2
	4:1.25DL	1.000	25.735	0	3	-25.735	0	1
	5:1.1DL+1.0W ₂	1.000	64.313	0	1	-64.313	0	2
	6:CASE I: VX	1.000	41.667	0	1	-41.667	0	2
	7:1.1DL+1.0W ₂	1.000	22.647	0	3	-22.647	0	1
	8:CASE I: VY	1.000	20.588	0	3	-20.588	0	1
	13:CASE III: V'	1.000	15.441	0	3	-15.441	0	1
	14:CASE III: V ₂	1.000	0.000	1.000	1	-0.000	1.000	3
	15:CASE III: VX	1.000	31.250	0	1	-31.250	0	2
31	2:DYNO DRUM	1.000	0.000	0.917	1	-0.000	0.917	3
	1:WEIGHT	1.000	20.588	0	3	-20.588	0	1
	10:WIND LOAL	1.000	41.667	0	1	-41.667	0	2
	11:WIND LOAL	1.000	41.667	0	1	-41.667	0	3
	12:DYNO DRU	1.000	0.000	0	3	-0.000	0	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	16:WIND RESI	1.000	56.769	0	1	-66.975	0	2
	9:COMPRESSI	1.000	0.000	0	2	-0.000	0	1
	3:1.1DL+1.0Wf	1.000	79.416	0	1	-89.622	0	2
	4:1.25DL	1.000	25.735	0	3	-25.735	0	1
	5:1.1DL+1.0Wz	1.000	64.314	0	1	-64.314	0	2
	6:CASE I: VX	1.000	41.667	0	1	-41.667	0	2
	7:1.1DL+1.0Wz	1.000	22.647	0	3	-22.647	0	1
	8:CASE I: VY	1.000	20.588	0	3	-20.588	0	1
	13:CASE III: V'	1.000	15.441	0	3	-15.441	0	1
	14:CASE III: Vz	1.000	0.000	0.917	1	-0.000	0.917	3
	15:CASE III: VX	1.000	31.250	0	1	-31.250	0	2
32	2:DYNO DRUM	4.830	874.350	0	1	-874.350	0	2
	1:WEIGHT	4.830	5.73E+3	0	1	-5.93E+3	4.830	2
	10:WIND LOAI	4.830	1.92E+3	0	3	-1.99E+3	0	1
	11:WIND LOAI	4.830	9.03E+3	0	2	-8.72E+3	0	1
	12:DYNO DRU	4.830	300.308	0	1	-281.127	0	2
	16:WIND RESI	4.830	1.15E+3	0	3	-1.19E+3	0	1
	9:COMPRESSI	4.830	0.000	4.830	2	-0.000	4.830	1
	3:1.1DL+1.0Wf	4.830	6.62E+3	0	1	-6.89E+3	4.830	2
	4:1.25DL	4.830	7.16E+3	0	1	-7.42E+3	4.830	2
	5:1.1DL+1.0Wz	4.830	6.56E+3	0	1	-6.81E+3	0	2
	6:CASE I: VX	4.830	1.92E+3	0	3	-1.99E+3	0	1
	7:1.1DL+1.0Wz	4.830	7.18E+3	0	1	-7.4E+3	4.830	2
	8:CASE I: VY	4.830	5.73E+3	0	1	-5.93E+3	4.830	2
	13:CASE III: V'	4.830	4.3E+3	0	1	-4.45E+3	4.830	2
	14:CASE III: Vz	4.830	655.762	0	1	-655.762	0	2
	15:CASE III: VX	4.830	1.23E+3	0	3	-1.26E+3	0	1
33	2:DYNO DRUM	4.830	0.000	0	1	-0.000	0	2
	1:WEIGHT	4.830	3.38E+3	0	2	-3.59E+3	4.830	1
	10:WIND LOAI	4.830	1.99E+3	0	1	-1.92E+3	0	2
	11:WIND LOAI	4.830	4.95E+3	4.830	1	-4.63E+3	4.830	2
	12:DYNO DRU	4.830	281.127	0	2	-300.308	0	1
	16:WIND RESI	4.830	958.260	0	3	-920.721	0	1
	9:COMPRESSI	4.830	0.000	0	1	-0.000	0	2
	3:1.1DL+1.0Wf	4.830	4.68E+3	0	2	-4.85E+3	0	1
	4:1.25DL	4.830	4.23E+3	0	2	-4.48E+3	4.830	1
	5:1.1DL+1.0Wz	4.830	4.02E+3	0	2	-4.18E+3	0	1
	6:CASE I: VX	4.830	1.99E+3	0	1	-1.92E+3	0	2
	7:1.1DL+1.0Wz	4.830	3.72E+3	0	2	-3.94E+3	4.830	1
	8:CASE I: VY	4.830	3.38E+3	0	2	-3.59E+3	4.830	1
	13:CASE III: V'	4.830	2.54E+3	0	2	-2.69E+3	4.830	1
	14:CASE III: Vz	4.830	0.000	0	1	-0.000	0	2
	15:CASE III: VX	4.830	1.26E+3	0	3	-1.23E+3	0	1



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Plate Center Stress Summary

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Max Qx	17	4:1.25DL	7.324	-0.147	-0.065	-0.204	-0.047	-1.308	-0.259	0.219
Min Qx	17	11:WIND LOA	-8.297	0.024	0.068318	0.216	0.050	1.462	0.415	-0.250
Max Qy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Qy	18	4:1.25DL	-2.508	-1.659	-8.665	-29.979	0.000	0.898	1.218	-3.636
Max Sx	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Sx	18	4:1.25DL	-2.508	-1.659	-8.665	-29.979	0.000	0.898	1.218	-3.636
Max Sy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Sy	18	4:1.25DL	-2.508	-1.659	-8.665	-29.979	0.000	0.898	1.218	-3.636
Max Sxy	17	2:DYNO DRUM	0.317	0.001	-0.011	-0.044	77.028	-0.143	-0.043	0.008
Min Sxy	19	2:DYNO DRUM	-0.361	0.001	-0.011	-0.044	-77.028	0.143	0.042553	0.010
Max Mx	19	4:1.25DL	-1.688	0.181	-0.065	-0.204	0.047	2.487	0.873	0.025
Min Mx	19	11:WIND LOA	2.301	-0.064	0.068	0.216	-0.050	-3.000	-0.915	-0.037
Max My	18	4:1.25DL	-2.508	-1.659	-8.665	-29.979	0.000	0.898	1.218	-3.636
Min My	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Max Mxy	18	11:WIND LOA	2.482	1.951	9.159	31.689	-0.000	-1.165	-1.412	4.276
Min Mxy	18	4:1.25DL	-2.508	-1.659	-8.665	-29.979	0.000	0.898	1.218	-3.636

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	15	11:WIND LOA	1.290	0	-0.000	0	0	0
Min FX	15	3:1.1DL+1.0W	-1.332	0	-0.155	0	0	0
Max FY	17	5:1.1DL+1.0W	0	0.447	0	0	0	0
Min FY	17	11:WIND LOA	0	-0.460	0	0	0	0
Max FZ	15	7:1.1DL+1.0W	-1.064	0	0.157	0	0	0
Min FZ	12	16:WIND RES	-0.251	0	-0.353	0	0	0
Max MX	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MX	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Max MY	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MY	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Max MZ	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0
Min MZ	12	2:DYNO DRUM	-0.010	0	0.157	0	0	0



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Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.028	1.000	0.028	HSS FLEX+A	7	1.890	2.460	2.460	4.030
2	HSST3X3X0	HSST3X3X0	0.092	1.000	0.092	HSS TORSIO	11	1.890	2.460	2.460	4.030
3	HSST3X3X0	HSST3X3X0	0.104	1.000	0.104	HSS T+SH+F	11	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.156	1.000	0.156	HSS T+SH+F	11	1.890	2.460	2.460	4.030
5	HSST3.5X3.	HSST3.5X3.	0.094	1.000	0.094	HSS TORSIO	11	2.910	5.040	5.040	8.350
6	HSST3.5X3.	HSST3.5X3.	0.196	1.000	0.196	HSS T+SH+F	11	2.910	5.040	5.040	8.350
7	HSST3X3X0	HSST3X3X0	0.031	1.000	0.031	HSS FLEX+A	7	1.890	2.460	2.460	4.030
8	HSST3X3X0	HSST3X3X0	0.203	1.000	0.203	HSS T+SH+F	11	1.890	2.460	2.460	4.030
9	HSST3X3X0	HSST3X3X0	0.139	1.000	0.139	HSS TORSIO	11	1.890	2.460	2.460	4.030
10	HSST3X3X0	HSST3X3X0	0.133	1.000	0.133	HSS T+SH+F	11	1.890	2.460	2.460	4.030
11	HSST3.5X3.	HSST3.5X3.	0.216	1.000	0.216	HSS FLEX+A	11	2.910	5.040	5.040	8.350
14	HSST3.5X3.	HSST3.5X3.	0.319	1.000	0.319	HSS FLEX+A	11	2.910	5.040	5.040	8.350
20	HSST3X3X0	HSST3X3X0	0.110	1.000	0.110	HSS FLEX+A	7	1.890	2.460	2.460	4.030
21	HSST3X3X0	HSST3X3X0	0.187	1.000	0.187	HSS T+SH+F	11	1.890	2.460	2.460	4.030
22	HSST3X3X0	HSST3X3X0	0.091	1.000	0.091	HSS TORSIO	11	1.890	2.460	2.460	4.030
23	HSST3X3X0	HSST3X3X0	0.139	1.000	0.139	HSS TORSIO	11	1.890	2.460	2.460	4.030
24	HSST3X3X0	HSST3X3X0	0.215	1.000	0.215	HSS T+SH+F	11	1.890	2.460	2.460	4.030
25	HSST3X3X0	HSST3X3X0	0.155	1.000	0.155	HSS T+SH+F	11	1.890	2.460	2.460	4.030
26	HSST3X3X0	HSST3X3X0	29757	1.000	0.029757	HSS FLEX+A	7	1.890	2.460	2.460	4.030
27	HSST3X3X0	HSST3X3X0	0.029	1.000	0.029	HSS FLEX+A	7	1.890	2.460	2.460	4.030
28	HSST3.5X3.	HSST3.5X3.	0.122	1.000	0.122	HSS BEND Z	11	2.910	5.040	5.040	8.350
29	HSST3.5X3.	HSST3.5X3.	0.347	1.000	0.347	HSS BEND Z	11	2.910	5.040	5.040	8.350
30	HSST3.5X3.	HSST3.5X3.	0.002	1.000	0.002	HSS FLEX+A	3	2.910	5.040	5.040	8.350
31	HSST3.5X3.	HSST3.5X3.	0.002	1.000	0.002	HSS FLEX+A	3	2.910	5.040	5.040	8.350
32	HSST3.5X3.	N/A						2.910	5.040	5.040	8.350
33	HSST3.5X3.	N/A						2.910	5.040	5.040	8.350

Failed Members

There is no data of this type.



Software licensed to Kimley-Horn (Cary), N CAROLINA
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
69

Rev
4

Job Title Pier Analysis

Part

Ref

By IERM Date 2/12/2020 Chd

Client THEA

File THEA-Pier Model_CaseL Date/Time 13-Feb-2020 11:54

Base Pressure Summary

	Node	L/C	FX (psi)	FY (psi)	FZ (psi)
Max FX	12	2:DYNO DRUM	0	0	0
Min FX	12	2:DYNO DRUM	0	0	0
Max FY	12	2:DYNO DRUM	0	0	0
Min FY	12	2:DYNO DRUM	0	0	0
Max FZ	12	2:DYNO DRUM	0	0	0
Min FZ	12	2:DYNO DRUM	0	0	0

Statics Check Results

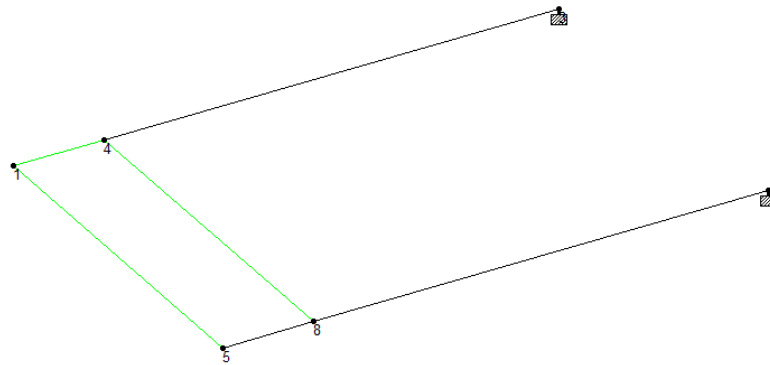
L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip-in)	MY (kip-in)	MZ (kip-in)
2:DYNO DRUM F	Loads	0	0	-0.313	0	37.584	0
2:DYNO DRUM F	Reactions	-0.000	0.000	0.313	2.518	-37.584	0.000
	Difference	-0.000	0.000	0.000	2.518	-0.000	0.000
1:WEIGHT	Loads	0	-0.692	0	-18.888	0	-83.024
1:WEIGHT	Reactions	-0.000	0.692	0.000	45.663	-0.000	83.024
	Difference	-0.000	0.000	0.000	26.776	-0.000	0.000
10:WIND LOAD C	Loads	0.340	0	0	0	-10.080	-7.260
10:WIND LOAD C	Reactions	-0.340	-0.000	-0.000	-0.000	10.080	7.260
	Difference	0.000	-0.000	-0.000	-0.000	-0.000	-0.000
11:WIND LOAD C	Loads	0	0.920	0	21.360	0	110.400
11:WIND LOAD C	Reactions	0.000	-0.920	-0.000	-60.720	0.000	-110.400
	Difference	0.000	-0.000	-0.000	-39.360	0.000	-0.000
12:DYNO DRUM	Loads	0.167	0	0	0	-3.999	0
12:DYNO DRUM	Reactions	-0.167	0.000	0.000	0.000	3.999	0.000
	Difference	-0.000	0.000	0.000	0.000	-0.000	0.000
16:WIND RESUL	Loads	0.508	0	0.508	6.709	-74.564	-6.709
16:WIND RESUL	Reactions	-0.508	0.000	-0.508	-4.088	74.564	6.709
	Difference	-0.000	0.000	0.000	2.622	-0.000	0.000
9:COMPRESSIOI	Loads	0	0	0	0	0	0
9:COMPRESSIOI	Reactions	0.000	-0.000	0.000	0.000	-0.000	-0.000
	Difference	0.000	-0.000	0.000	0.000	-0.000	-0.000



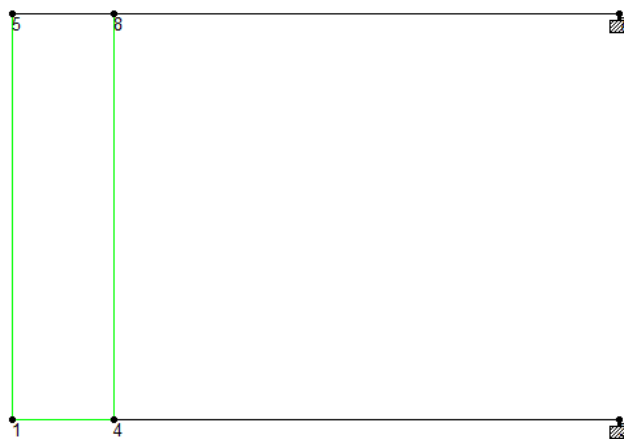
Straddle Bent-Sides

The following structure spacing was accommodated from analyzing the THEA contract plans reinforcement for the straddle bent. It was concluded that the HSS arm would be welded to the plate and bolted onto the straddle bent column. The 2ft width of the arms can vary based on field rebar measurements. The distance was chosen for a worst case scenario.

3D View-Length:



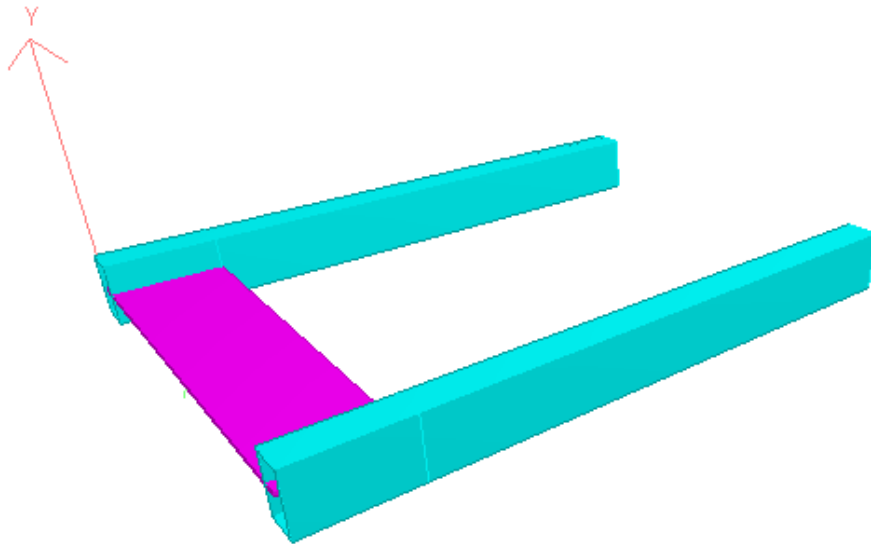
Plan View:



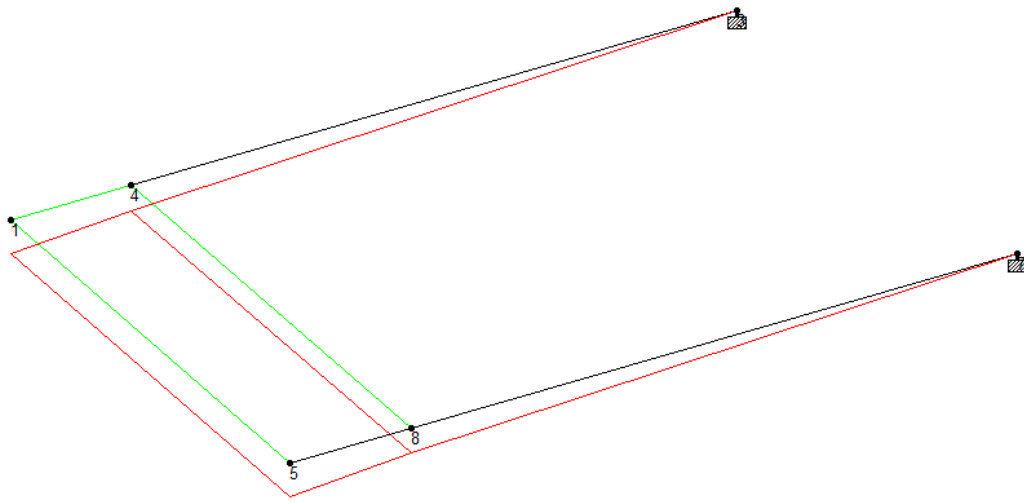
Side View:



3D View:



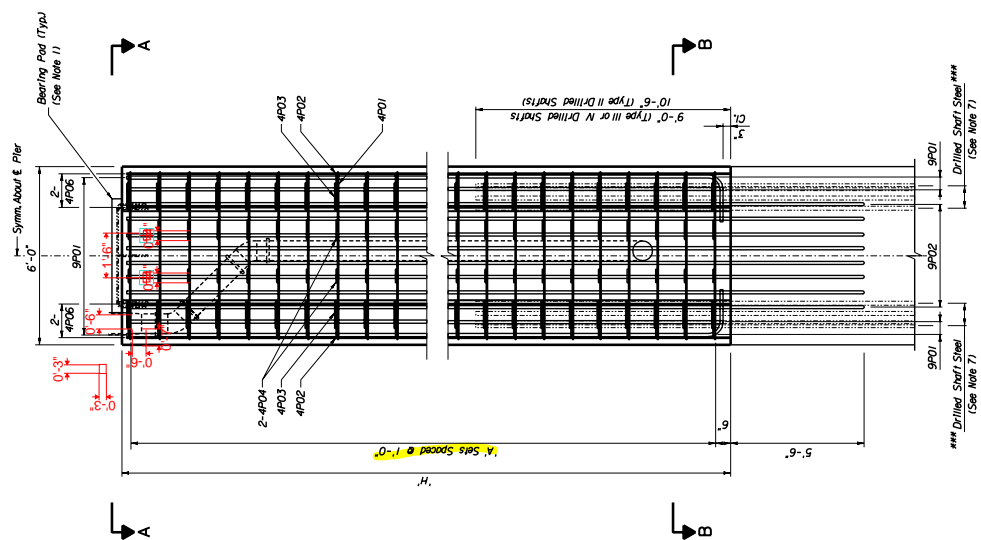
Deflection View:





Existing Structural Plans

***Note:**
 Based on the location of the drainage pipe 1'-9" into the bent. The plate will be able to be drilled without any obstruction.



Pier	'A' S66
165 L	57
165 R	58
164 L	60
164 R	62
163 L	60
163 R	63
162 L	61
162 R	64
46 L	35
46 R	32
45 L	37
45 R	34
44 L	36
44 R	36
43 L	40
43 R	39
42 L	42
42 R	42
29 L	38
29 R	35
28 L	36
28 R	35
27 L	38
27 R	36
26 L	41
26 R	38

ELEVATION

*** 11SD1,11S02 & 11S03 Bars Terminating at Top of Drilled Shaft Not Shown

SIDE VIEW

*** 11SD1,11S02 & 11S03 Bars Terminating at Top of Drilled Shaft Not Shown

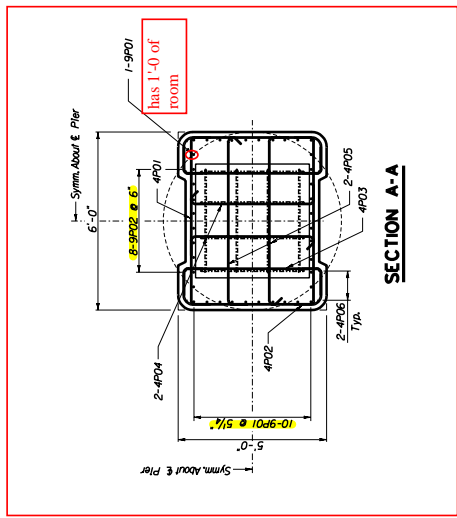
NOTE:

1. For Bearing Details, See Bearing Details sheets.
2. For Straddle Bar Details, See Straddle Bar Dimensions and Reinforcement sheets.
3. For Drainage Details, See Drainage Details sheets.
4. For Drilled Shaft Details, See Drilled Shaft Dimensions and Reinforcement sheets.
5. E.F. Denotes Each Face
6. O.F. Denotes Outside Face
7. I.F. Denotes Inside Face
8. Minimum Concrete Cover - 2" Unless Otherwise Noted
9. For Placement of Drilled Shaft Reinforcement, See Sheets T-156 and T-157.

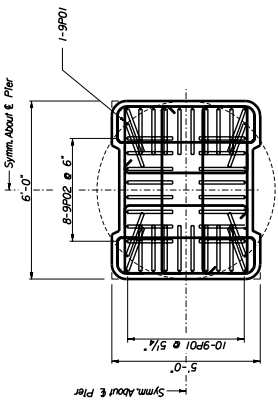
STRUCTURE NOS. 100800, 100806 & 100812 STRADDLE BENT COLUMN REINFORCEMENT 1		SHEET TITLE DRAWING NO. T-174
TAMPBA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		PROJECT NAME SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE
FORM NO. S.R. 618	COUNTY HILLSBOROUGH	CONSTRUCTION PROJECT NO. THCEA 5140.01
REVISIONS		
DATE	BY	DESCRIPTION
12-13-02	JMF	ENGINEER OF RECORD
12-13-02	CF	DATE 12-13-02
12-13-02	CF	CHECKED BY 124 No. Carlson Street Tampa, FL 33604 Phone: 813-288-8800 Fax: 813-288-8801 E-Mail: j.rodriguez@twp.com
12-13-02	ADH	DESIGNED BY 2800 N. Westchase Blvd., Suite 500 Tampa, FL 33607 Phone: 813-288-8800 Fax: 813-288-8801 E-Mail: j.rodriguez@twp.com
12-13-02	J.R. Rodriguez	APPROVED BY

DATE	1/12/01
REVISION	1
DESCRIPTION	FLA 50-001 & 51-001

BAR BENDING DIAGRAMS
(All dimensions are cut to cut)



SECTION A-A



SECTION B-B

(Drilled Shaft Reinforcing Not Shown)
(See Section A-A for callouts of #4 bars)

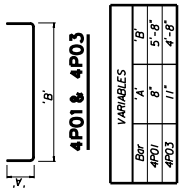
BAR LIST - PER

Bar No.	Length	Bent	Str.
4P01	Varies	7'-0"	•
4P02	Varies	8'-6"	•
4P03	Varies	6'-6"	•
4P04	Varies	5'-4"	•
4P05	Varies	6'-10"	•
4P06	8	Varies	•
9P01	24	Varies	•
9P02	16	Varies	•

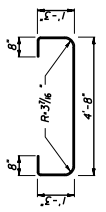
*Number preceding letter denotes Bar size.
All bars shall be in accordance with A.C.I. Standards.



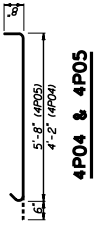
9P01 & 9P02



4P01 & 4P03



4P02



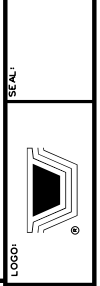
4P04 & 4P05

ESTIMATED QUANTITIES

Pier	Variable Length						Class IV Concrete (5500 psi)(Cu./Yds.)	Reinforcing Steel (lbs.)	
	4P01	4P02	4P03	4P04	4P05	9P01			
165 L	114	114	114	114	114	55'-10"	61'-1"	5802	10718
165 R	116	116	116	116	116	55'-10"	61'-1"	5806	10805
164 L	120	120	120	120	120	58'-10"	64'-1"	6113	11219
164 R	124	124	124	124	124	61'-4"	66'-7"	6372	11254
163 L	120	120	120	120	120	59'-4"	64'-7"	6165	11350
163 R	126	126	126	126	126	62'-4"	67'-7"	6476	11911
162 L	122	122	122	122	122	59'-10"	65'-1"	6217	11466
162 R	128	128	128	128	128	62'-10"	68'-1"	6528	12027
46 L	70	70	70	70	70	34'-4"	33'-7"	3575	6675
46 R	64	64	64	64	64	30'-10"	30'-1"	3212	6043
45 L	74	74	74	74	74	35'-10"	35'-1"	3730	6978
45 R	68	68	68	68	68	32'-10"	32'-1"	3419	6417
44 L	76	76	76	76	76	36'-10"	36'-1"	3834	7165
44 R	72	72	72	72	72	34'-10"	34'-1"	3627	6931
43 L	80	80	80	80	80	39'-4"	38'-7"	4093	7610
43 R	78	78	78	78	78	38'-4"	37'-7"	3989	7423
42 L	84	84	84	84	84	41'-4"	40'-7"	4300	7984
42 R	84	84	84	84	84	41'-4"	40'-7"	4300	7984
29 L	76	76	76	76	76	36'-10"	36'-1"	3834	7165
29 R	70	70	70	70	70	33'-10"	33'-1"	3523	6604
28 L	76	76	76	76	76	36'-10"	36'-1"	3834	7165
28 R	70	70	70	70	70	34'-4"	33'-7"	3575	6675
27 L	76	76	76	76	76	37'-4"	36'-7"	3986	7236
27 R	72	72	72	72	72	35'-4"	34'-7"	3678	6962
26 L	82	82	82	82	82	39'-10"	39'-1"	4165	7785
26 R	76	76	76	76	76	36'-10"	36'-1"	3834	7165

STRUCTURE NOS. 100800, 100806 & 100812
STRADDLE BENT COLUMN REINFORCEMENT 2
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE

TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY
CONSTRUCTION PROJECT NO. THCEA 5140.01
COUNTY: HILLSBOROUGH
FORM NO. S.R. 618



ENGINEER OF RECORD:
J. Rodriguez
124 N. Central Street
Tampa, Florida 33601
Professional Engineer No. 5332

DATE	BY	DESCRIPTION
12-13-02	J. Rodriguez	Checked by
12-13-02	J. Rodriguez	Designed by
12-13-02	J. Rodriguez	Checked by

DATE	BY	DESCRIPTION

REVISIONS
DATE BY DESCRIPTION

STAAD Analysis


```

*****
*
*          STAAD.Pro V8i SELECTseries6          *
*          Version  20.07.11.70                 *
*          Proprietary Program of               *
*          Bentley Systems, Inc.                *
*          Date=    JUL 19, 2018                *
*          Time=    15:51:29                   *
*
*          USER ID: Kimley-Horn and Associates  *
*****

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```

1. STAAD SPACE
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2. START JOB INFORMATION
3. ENGINEER DATE 19-JUN-18
4. JOB NAME STRADDLE BENT - SIDES
5. JOB CLIENT THEA
6. JOB NO 148872000
7. JOB REV 3
8. ENGINEER NAME IERM
9. END JOB INFORMATION
10. INPUT WIDTH 79
11. UNIT FEET KIP
12. JOINT COORDINATES
13. 1 0 0 0; 3 3 0 0; 4 0.5 0 0; 5 0 0 2; 7 3 0 2; 8 0.5 0 2
14. MEMBER INCIDENCES
15. 1 1 4; 4 5 8; 8 4 3; 9 8 7
16. ELEMENT INCIDENCES SHELL
17. 7 5 1 4 8
18. ELEMENT PROPERTY
19. 7 THICKNESS 0.020833
20. DEFINE MATERIAL START
21. ISOTROPIC STEEL
22. E 4.176E+006
23. POISSON 0.3
24. DENSITY 0.489024
25. ALPHA 6E-006
26. DAMP 0.03
27. TYPE STEEL
28. STRENGTH FY 5184 FU 8352 RY 1.5 RT 1.2
29. ISOTROPIC A500-GR.
30. E 4.176E+006
31. POISSON 0.3
32. DENSITY 0.49
33. ALPHA 6E-006
34. DAMP 0.03
35. G 1.6128E-006
36. TYPE STEEL
37. STRENGTH FY 6624 FU 8352 RY 1.1 RT 1.2
38. END DEFINE MATERIAL

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39. MEMBER PROPERTY AMERICAN
 40. 1 4 8 9 TABLE ST HSST3.5X2X0.188
 41. CONSTANTS
 42. MATERIAL STEEL MEMB 7
 43. MATERIAL A500-GR. MEMB 1 4 8 9
 44. SUPPORTS
 45. 3 7 FIXED
 46. LOAD 1 LOADTYPE DEAD TITLE DL
 47. SELFWEIGHT Y -1 LIST ALL
 48. JOINT LOAD
 49. 1 5 FY -0.0528
 50. LOAD 2 LOADTYPE WIND TITLE W1
 51. JOINT LOAD
 52. 1 5 FZ -0.0277
 53. 1 5 MX -0.0159
 54. 1 5 FX 0.0293
 55. 1 5 MZ -0.0173
 56. LOAD 3 LOADTYPE WIND TITLE 0.75W2
 57. JOINT LOAD
 58. 1 5 FZ -0.021
 59. 1 5 MX -0.012
 60. 1 5 FX 0.022
 61. 1 5 MZ -0.013
 62. LOAD COMB 4 1.25DL
 63. 1 1.25
 64. LOAD COMB 5 1.1DL+1.0W1
 65. 1 1.1 2 1.0
 66. LOAD COMB 6 1.1DL+1.0W2
 67. 1 1.1 3 1.0
 68. PERFORM ANALYSIS PRINT ALL

P R O B L E M S T A T I S T I C S

NUMBER OF JOINTS	6	NUMBER OF MEMBERS	4
NUMBER OF PLATES	1	NUMBER OF SOLIDS	0
NUMBER OF SURFACES	0	NUMBER OF SUPPORTS	2

SOLVER USED IS THE OUT-OF-CORE BASIC SOLVER

ORIGINAL/FINAL BAND-WIDTH= 5/ 5/ 24 DOF
 TOTAL PRIMARY LOAD CASES = 3, TOTAL DEGREES OF FREEDOM = 24
 TOTAL LOAD COMBINATION CASES = 3 SO FAR.
 SIZE OF STIFFNESS MATRIX = 1 DOUBLE KILO-WORDS
 REQD/AVAIL. DISK SPACE = 12.0/ 0.0 MB

STAAD SPACE

-- PAGE NO. 3

LOADING 1 LOADTYPE DEAD TITLE DL

SELFWEIGHT Y -1.000

ACTUAL WEIGHT OF THE STRUCTURE = 0.045 KIP

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	-0.05	0.00	0.00	0.00	0.00
5	0.00	-0.05	0.00	0.00	0.00	0.00

LOADING 2 LOADTYPE WIND TITLE W1

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.03	0.00	0.00	0.00
5	0.00	0.00	-0.03	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.02	0.00	0.00
5	0.00	0.00	0.00	-0.02	0.00	0.00
1	0.03	0.00	0.00	0.00	0.00	0.00
5	0.03	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	-0.02
5	0.00	0.00	0.00	0.00	0.00	-0.02

LOADING 3 LOADTYPE WIND TITLE 0.75W2

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.02	0.00	0.00	0.00
5	0.00	0.00	-0.02	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.01	0.00	0.00
5	0.00	0.00	0.00	-0.01	0.00	0.00
1	0.02	0.00	0.00	0.00	0.00	0.00
5	0.02	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	-0.01
5	0.00	0.00	0.00	0.00	0.00	-0.01

FOR LOADING - 1
APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
-------	---------	---------	---------	-------	-------	-------

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00000E+00	-5.68016E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.21224E-04
3	0.00000E+00	-7.27344E-03	0.00000E+00	0.00000E+00	0.00000E+00	3.03060E-03
4	0.00000E+00	-1.12751E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.90938E-03
5	0.00000E+00	-5.68016E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.21224E-04
7	0.00000E+00	-7.27344E-03	0.00000E+00	0.00000E+00	0.00000E+00	3.03060E-03
8	0.00000E+00	-1.12751E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.90938E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.364403388E+00
Y = 0.000000000E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.00
SUMMATION FORCE-Y = -0.15
SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 0.15 MY= 0.00 MZ= -0.05

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.00
SUMMATION FORCE-Y = 0.15
SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -0.15 MY= 0.00 MZ= 0.05

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)
MAXIMUMS AT NODE
X = 0.00000E+00 0
Y = -1.31106E-02 5
Z = 0.00000E+00 0
RX= 9.57666E-06 4
RY= 0.00000E+00 0
RZ= 5.38717E-04 5

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
						SUPPORT=1
3	0.00 0.00	-0.01 -0.07	0.00 0.00	0.00 0.00	0.00 0.00	0.00 0.20 111111

STAAD SPACE -- PAGE NO. 5

7	0.00	-0.01	0.00	0.00	0.00	0.00	
	0.00	-0.07	0.00	-0.00	0.00	0.20	111111

FOR LOADING - 2

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	2.93000E-02	0.00000E+00	-2.77000E-02	-1.59000E-02	0.00000E+00	-1.73000E-02
5	2.93000E-02	0.00000E+00	-2.77000E-02	-1.59000E-02	0.00000E+00	-1.73000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.590443686E+00
Z = 0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.574007281E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = 5.8600001E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -5.5399999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -3.1800003E-02 MY= 5.8600003E-02 MZ= -3.4600001E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = -5.8600001E-02
SUMMATION FORCE-Y = 8.5625951E-15
SUMMATION FORCE-Z = 5.5399999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 3.1800003E-02 MY= -5.8600003E-02 MZ= 3.4600001E-02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)

MAXIMUMS	AT NODE
X = 5.24405E-05	1
Y = 4.35162E-03	5
Z = -2.38559E-03	1
RX= -2.04126E-03	1
RY= -2.45045E-05	8
RZ= -1.97655E-04	5

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
----	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUPPORT=1

FOR LOADING - 3

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	2.20000E-02	0.00000E+00	-2.10000E-02	-1.20000E-02	0.00000E+00	-1.30000E-02
5	2.20000E-02	0.00000E+00	-2.10000E-02	-1.20000E-02	0.00000E+00	-1.30000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
LOADTYPE WIND TITLE 0.75W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.590909124E+00
Z = 0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.571428572E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 4.4000000E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -4.1999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -2.4000000E-02 MY= 4.4000001E-02 MZ= -2.6000001E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -4.4000000E-02
SUMMATION FORCE-Y = 6.4392935E-15
SUMMATION FORCE-Z = 4.1999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 2.4000000E-02 MY= -4.4000001E-02 MZ= 2.6000001E-02

STAAD SPACE

-- PAGE NO. 7

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)
 MAXIMUMS AT NODE
 X = 3.96028E-05 1
 Y = 3.27843E-03 5
 Z = -1.80856E-03 1
 RX= -1.54054E-03 1
 RY= -1.85754E-05 8
 RZ= -1.48851E-04 5

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
----	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUPPORT=1

LOAD COMBINATION NO. 4
 1.25DL

LOADING- 1.
 FACTOR - 1.25

LOAD COMBINATION NO. 5
 1.1DL+1.0W1

LOADING- 1. 2.
 FACTOR - 1.10 1.00

LOAD COMBINATION NO. 6
 1.1DL+1.0W2

LOADING- 1. 3.
 FACTOR - 1.10 1.00

***** END OF DATA FROM INTERNAL STORAGE *****

69. PARAMETER 2
 70. CODE LRFD
 71. CHECK CODE ALL

STAAD.Pro CODE CHECKING - (LRFD 3RD EDITION) v1.0

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE Noted)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
1	ST	HSST3.5X2X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.012	5
		0.06 C	0.03	0.02	0.50
4	ST	HSST3.5X2X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.012	2
		0.00 C	0.03	-0.02	0.50
8	ST	HSST3.5X2X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.059	5
		0.08 C	-0.04	0.24	2.50
9	ST	HSST3.5X2X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.049	4
		0.00 C	0.00	0.25	2.50

***** END OF TABULATED RESULT OF DESIGN *****

72. PERFORM ANALYSIS PRINT STATICS CHECK

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.364403388E+00
Y = 0.000000000E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.00
SUMMATION FORCE-Y = -0.15
SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 0.15 MY= 0.00 MZ= -0.05

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.00
SUMMATION FORCE-Y = 0.15
SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -0.15 MY= 0.00 MZ= 0.05

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)
MAXIMUMS AT NODE
X = 0.00000E+00 0
Y = -1.31106E-02 5
Z = 0.00000E+00 0
RX= 9.57666E-06 4
RY= 0.00000E+00 0
RZ= 5.38717E-04 5

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.590443686E+00
Z = 0.100000003E+01

STAAD SPACE

-- PAGE NO. 10

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.574007281E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = 5.8600001E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -5.5399999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -3.1800003E-02 MY= 5.8600003E-02 MZ= -3.4600001E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = -5.8600001E-02
SUMMATION FORCE-Y = 8.5625951E-15
SUMMATION FORCE-Z = 5.5399999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 3.1800003E-02 MY= -5.8600003E-02 MZ= 3.4600001E-02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)

	MAXIMUMS	AT NODE
X =	5.24405E-05	1
Y =	4.35162E-03	5
Z =	-2.38559E-03	1
RX=	-2.04126E-03	1
RY=	-2.45045E-05	8
RZ=	-1.97655E-04	5

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
LOADTYPE WIND TITLE 0.75W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.590909124E+00
Z = 0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.571428572E+00
Z = 0.100000003E+01

STAAD SPACE

-- PAGE NO. 11

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 4.4000000E-02

SUMMATION FORCE-Y = 0.0000000E+00

SUMMATION FORCE-Z = -4.1999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -2.4000000E-02 MY= 4.4000001E-02 MZ= -2.6000001E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -4.4000000E-02

SUMMATION FORCE-Y = 6.4392935E-15

SUMMATION FORCE-Z = 4.1999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 2.4000000E-02 MY= -4.4000001E-02 MZ= 2.6000001E-02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)

MAXIMUMS AT NODE

X = 3.96028E-05 1

Y = 3.27843E-03 5

Z = -1.80856E-03 1

RX= -1.54054E-03 1

RY= -1.85754E-05 8

RZ= -1.48851E-04 5

***** END OF DATA FROM INTERNAL STORAGE *****

73. FINISH

***** END OF THE STAAD.Pro RUN *****

**** DATE= JUL 19,2018 TIME= 15:51:31 ****

* For technical assistance on STAAD.Pro, please visit *
* <http://selectservices.bentley.com/en-US/> *
* * * * *
* Details about additional assistance from *
* Bentley and Partners can be found at program menu *
* Help->Technical Support *
* * * * *
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Job No
148872000

Sheet No
1

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	19-Jun-18		

Project ID	
Project Name	

Structure Type	SPACE FRAME
-----------------------	-------------

Number of Nodes	6	Highest Node	8
Number of Elements	4	Highest Beam	9
Number of Plates	1	Highest Plate	7

Number of Basic Load Cases	3
Number of Combination Load Cases	3

Included in this printout are data for:

All	The Whole Structure
------------	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	W1
Primary	3	0.75W2
Combination	4	1.25DL
Combination	5	1.1DL+1.0W1
Combination	6	1.1DL+1.0W2

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	4	0.500	2	0
4	5	8	0.500	2	0
8	4	3	2.500	2	0
9	8	7	2.500	2	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
7	5	1	4	8	1



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Job No
148872000

Sheet No
2

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (/°F)
1	STEEL	29E+3	0.300	0.000	6E-6
2	STAINLESSSTEEL	28E+3	0.300	0.000	10E-6
3	ALUMINUM	10E+3	0.330	0.000	13E-6
4	A500-GR.	29E+3	0.300	0.000	6E-6
5	CONCRETE	3.15E+3	0.170	0.000	5E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
3	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	W1	Wind
3	0.75W2	Wind

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	1.25DL	1	DL	1.25
5	1.1DL+1.0W1	1	DL	1.10
		2	W1	1.00
6	1.1DL+1.0W2	1	DL	1.10
		3	0.75W2	1.00



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Job No
148872000

Sheet No
3

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	1	2:W1	0.000	-0.001	-0.002	0.003	-0.002	0.000	0.000
Min X	8	2:W1	-0.000	0.003	-0.002	0.004	0.001	-0.000	-0.000
Max Y	5	2:W1	-0.000	0.004	-0.002	0.005	-0.002	0.000	-0.000
Min Y	1	4:1.25DL	0.000	-0.016	0.000	0.016	0.000	0.000	0.001
Max Z	1	1:DL	0.000	-0.013	0.000	0.013	0.000	0.000	0.001
Min Z	1	2:W1	0.000	-0.001	-0.002	0.003	-0.002	0.000	0.000
Max rX	8	2:W1	-0.000	0.003	-0.002	0.004	0.001	-0.000	-0.000
Min rX	1	2:W1	0.000	-0.001	-0.002	0.003	-0.002	0.000	0.000
Max rY	5	2:W1	-0.000	0.004	-0.002	0.005	-0.002	0.000	-0.000
Min rY	8	2:W1	-0.000	0.003	-0.002	0.004	0.001	-0.000	-0.000
Max rZ	1	4:1.25DL	0.000	-0.016	0.000	0.016	0.000	0.000	0.001
Min rZ	5	2:W1	-0.000	0.004	-0.002	0.005	-0.002	0.000	-0.000
Max Rst	1	4:1.25DL	0.000	-0.016	0.000	0.016	0.000	0.000	0.001

Beam Displacement Detail Summary

Displacements shown in italic indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	1	2:W1	0.000	0.000	-0.001	-0.002	0.003
Min X	4	2:W1	0.350	-0.000	0.004	-0.002	0.004
Max Y	4	2:W1	0.000	-0.000	0.004	-0.002	0.005
Min Y	1	4:1.25DL	0.000	0.000	-0.016	0.000	0.016
Max Z	1	1:DL	0.000	0.000	-0.013	0.000	0.013
Min Z	4	2:W1	0.150	-0.000	0.004	-0.002	0.005
Max Rst	1	4:1.25DL	0.000	0.000	-0.016	0.000	0.016

Beam End Displacement Summary

Displacements shown in italic indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	1	1	2:W1	0.000	-0.001	-0.002	0.003
Min X	4	8	2:W1	-0.000	0.003	-0.002	0.004
Max Y	4	5	2:W1	-0.000	0.004	-0.002	0.005
Min Y	1	1	4:1.25DL	0.000	-0.016	0.000	0.016
Max Z	1	1	1:DL	0.000	-0.013	0.000	0.013
Min Z	1	1	2:W1	0.000	-0.001	-0.002	0.003
Max Rst	1	1	4:1.25DL	0.000	-0.016	0.000	0.016



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Job No 148872000	Sheet No 4	Rev 3
Part		
Ref		
By IERM	Date 19-Jun-18	Chd
Client THEA	File THEA2.1-StraddleBent-Si	Date/Time 19-Jul-2018 11:27

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	8	4	2:W1	0.076	-0.016	-0.028	0.000	0.391	-0.194
Min Fx	9	8	2:W1	-0.017	0.016	-0.028	0.000	0.389	-0.222
Max Fy	9	8	2:W1	-0.017	0.016	-0.028	0.000	0.389	-0.222
Min Fy	8	3	5:1.1DL+1.0W1	0.076	-0.099	-0.028	0.000	-0.441	2.905
Max Fz	1	1	2:W1	0.055	-0.015	0.065	-0.000	-0.067	-0.264
Min Fz	8	4	2:W1	0.076	-0.016	-0.028	0.000	0.391	-0.194
Max Mx	9	8	2:W1	-0.017	0.016	-0.028	0.000	0.389	-0.222
Min Mx	1	1	5:1.1DL+1.0W1	0.055	-0.076	0.065	-0.000	-0.067	-0.265
Max My	8	4	2:W1	0.076	-0.016	-0.028	0.000	0.391	-0.194
Min My	8	3	2:W1	0.076	-0.016	-0.028	0.000	-0.441	0.283
Max Mz	8	3	4:1.25DL	-0.000	-0.094	-0.000	0.000	-0.000	2.979
Min Mz	9	7	2:W1	-0.017	0.016	-0.028	0.000	-0.440	-0.699

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	8	2:W1	0.000	0.076	-0.016	-0.028	0.000	0.391	-0.194
Min Fx	9	2:W1	0.000	-0.017	0.016	-0.028	0.000	0.389	-0.222
Max Fy	9	2:W1	0.000	-0.017	0.016	-0.028	0.000	0.389	-0.222
Min Fy	8	5:1.1DL+1.0W1	2.500	0.076	-0.099	-0.028	0.000	-0.441	2.905
Max Fz	1	2:W1	0.000	0.055	-0.015	0.065	-0.000	-0.067	-0.264
Min Fz	8	2:W1	0.000	0.076	-0.016	-0.028	0.000	0.391	-0.194
Max Mx	9	2:W1	0.000	-0.017	0.016	-0.028	0.000	0.389	-0.222
Min Mx	1	5:1.1DL+1.0W1	0.000	0.055	-0.076	0.065	-0.000	-0.067	-0.265
Max My	8	2:W1	0.000	0.076	-0.016	-0.028	0.000	0.391	-0.194
Min My	8	2:W1	2.500	0.076	-0.016	-0.028	0.000	-0.441	0.283
Max Mz	8	4:1.25DL	2.500	-0.000	-0.094	-0.000	0.000	-0.000	2.979
Min Mz	9	2:W1	2.500	-0.017	0.016	-0.028	0.000	-0.440	-0.699



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Job No
148872000

Sheet No
5

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	1:DL	0.500	227.822	0.500	3	-227.822	0.500	1
	2:W1	0.500	450.225	0.500	2	-385.801	0.500	4
	3:0.75W2	0.500	340.380	0.500	2	-291.777	0.500	4
	4:1.25DL	0.500	284.777	0.500	3	-284.777	0.500	1
	5:1.1DL+1.0W1	0.500	465.047	0.500	3	-400.623	0.500	1
	6:1.1DL+1.0W2	0.500	413.940	0.500	3	-365.338	0.500	1
4	1:DL	0.500	227.822	0.500	3	-227.822	0.500	1
	2:W1	0.500	467.111	0.500	2	-465.891	0.500	4
	3:0.75W2	0.500	352.987	0.500	2	-352.301	0.500	4
	4:1.25DL	0.500	284.777	0.500	3	-284.777	0.500	1
	5:1.1DL+1.0W1	0.500	400.029	0.500	3	-398.809	0.500	1
	6:1.1DL+1.0W2	0.500	364.734	0.500	3	-364.047	0.500	1
8	1:DL	2.500	1.6E+3	2.500	3	-1.6E+3	2.500	1
	2:W1	2.500	642.965	2.500	4	-554.465	2.500	2
	3:0.75W2	2.500	487.126	2.500	4	-420.282	2.500	2
	4:1.25DL	2.500	2E+3	2.500	3	-2E+3	2.500	1
	5:1.1DL+1.0W1	2.500	2.4E+3	2.500	4	-2.31E+3	2.500	2
	6:1.1DL+1.0W2	2.500	2.24E+3	2.500	4	-2.18E+3	2.500	2
9	1:DL	2.500	1.6E+3	2.500	3	-1.6E+3	2.500	1
	2:W1	2.500	866.009	2.500	1	-885.971	2.500	3
	3:0.75W2	2.500	654.370	2.500	1	-669.753	2.500	3
	4:1.25DL	2.500	2E+3	2.500	3	-2E+3	2.500	1
	5:1.1DL+1.0W1	2.500	1.69E+3	2.500	4	-1.71E+3	2.500	2
	6:1.1DL+1.0W2	2.500	1.71E+3	2.500	4	-1.72E+3	2.500	2

Plate Center Principal Stress Summary

	Plate	L/C	Principal		Von Mis		Tresca	
			Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)
Max (t)	7	2:W1	625.041	676.984	1.07E+3	1.18E+3	1.24E+3	1.36E+3
Max (b)	7	5:1.1DL+1.0W1	620.600	681.389	1.07E+3	1.18E+3	1.24E+3	1.36E+3
Max VM (t)	7	2:W1	625.041	676.984	1.07E+3	1.18E+3	1.24E+3	1.36E+3
Max VM (b)	7	2:W1	625.041	676.984	1.07E+3	1.18E+3	1.24E+3	1.36E+3
Tresca (t)	7	2:W1	625.041	676.984	1.07E+3	1.18E+3	1.24E+3	1.36E+3
Tresca (b)	7	2:W1	625.041	676.984	1.07E+3	1.18E+3	1.24E+3	1.36E+3



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
6

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	7	2:W1	0.017	-0.016	0.028	-0.000	0.440	0.699
Min FX	3	2:W1	-0.076	0.016	0.028	-0.000	0.441	-0.283
Max FY	3	5:1.1DL+1.0W1	-0.076	0.099	0.028	-0.000	0.441	-2.905
Min FY	7	2:W1	0.017	-0.016	0.028	-0.000	0.440	0.699
Max FZ	3	2:W1	-0.076	0.016	0.028	-0.000	0.441	-0.283
Min FZ	3	1:DL	0.000	0.075	0.000	-0.000	0.000	-2.383
Max MX	7	4:1.25DL	0.000	0.094	0.000	0.000	0.000	-2.979
Min MX	7	2:W1	0.017	-0.016	0.028	-0.000	0.440	0.699
Max MY	3	2:W1	-0.076	0.016	0.028	-0.000	0.441	-0.283
Min MY	3	1:DL	0.000	0.075	0.000	-0.000	0.000	-2.383
Max MZ	7	2:W1	0.017	-0.016	0.028	-0.000	0.440	0.699
Min MZ	3	4:1.25DL	0.000	0.094	0.000	-0.000	0.000	-2.979



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
7

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Steel Design (Track 2) Beam 1 Check 1

```

*****
MEMBER 1 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1710E+1
AY=0.1218E+1
AZ=0.4640E+0
PY=0.1270E+1
PZ=0.1890E+1
RY=0.7947E+0
RZ=0.1235E+1
*****
PARAMETER 0.0 (KIP-FOOT)
IN KIP INCH
*****
L4 CAPACITIES
IN KIP INCH
KL/R-Y= 7.55
KL/R-Z= 4.86
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.1 0.0 0.0
LOCATION 0.0 0.5 0.0 0.5 0.5
LOADING 2 5 2 2 4
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.012 5
0.06 C 0.03 0.02 0.50
*****
1 ST HSST3.5X2X0.188 (AISC SECTIONS)

```



Software licensed to Kimley-Horn and Associates
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
8

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Steel Design (Track 2) Beam 4 Check 1

```

*****
MEMBER 4 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1710E+1
AY=0.1218E+1
AZ=0.4640E+0
PY=0.1270E+1
PZ=0.1890E+1
RY=0.7947E+0
RZ=0.1235E+1

PARAMETER 0.0 (KIP-FOOT)
IN KIP INCH
-----
KL/R-Y= 7.55
KL/R-Z= 4.86
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00

L4
L4
L4
L2 L2
L5 L2 L2
-----
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.1 0.1 0.0 0.0
LOCATION 0.0 0.5 0.0 0.5 0.5
LOADING 2 4 2 2 4

*****
*
* DESIGN SUMMARY (KIP-FOOT)
*
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
-----
PASS HSS FLEX+AXL 0.012 2
0.00 C 0.03 -0.02 0.50
*
*****
4 ST HSST3.5X2X0.188 (AISC SECTIONS)

```



Software licensed to Kimley-Horn and Associates
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
9

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Steel Design (Track 2) Beam 8 Check 1

```

*****
MEMBER 8 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 2.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1710E+1
AY=0.1218E+1
AZ=0.4640E+0
PY=0.1270E+1
PZ=0.1890E+1
RY=0.7947E+0
RZ=0.1235E+1
*****
PARAMETER 0.2 (KIP-FEET)
IN KIP INCH
KL/R-Y= 37.75
KL/R-Z= 24.28
UNL = 30.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.0 0.0 0.2
LOCATION 0.0 2.5 0.0 2.5 2.5
LOADING 2 5 2 2 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.059 5
0.08 C -0.04 0.24 2.50
*****
8 ST HSST3.5X2X0.188 (AISC SECTIONS)

```



Software licensed to Kimley-Horn and Associates
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
10

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Steel Design (Track 2) Beam 9 Check 1

```

*****
MEMBER 9 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 2.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1710E+1
AY=0.1218E+1
AZ=0.4640E+0
PY=0.1270E+1
PZ=0.1890E+1
RY=0.7947E+0
RZ=0.1235E+1
*****
PARAMETER 0.2 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 37.75
KL/R-Z= 24.28
UNL = 30.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.0 0.1 0.0 0.0 0.2
LOCATION 0.0 2.5 0.0 2.5 2.5
LOADING 2 4 2 2 4
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS BEND Z 0.049 4
0.00 C 0.00 0.25 2.50
*****
9 ST HSST3.5X2X0.188 (AISC SECTIONS)

```



Software licensed to Kimley-Horn and Associates
CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
11

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3.5X2)	HSST3.5X2)	0.012	1.000	0.012	HSS FLEX+A	5	1.710	2.610	1.080	2.550
4	HSST3.5X2)	HSST3.5X2)	0.012	1.000	0.012	HSS FLEX+A	2	1.710	2.610	1.080	2.550
8	HSST3.5X2)	HSST3.5X2)	0.059	1.000	0.059	HSS FLEX+A	5	1.710	2.610	1.080	2.550
9	HSST3.5X2)	HSST3.5X2)	0.049	1.000	0.049	HSS BEND Z	4	1.710	2.610	1.080	2.550

Failed Members

There is no data of this type.

Statics Check Results

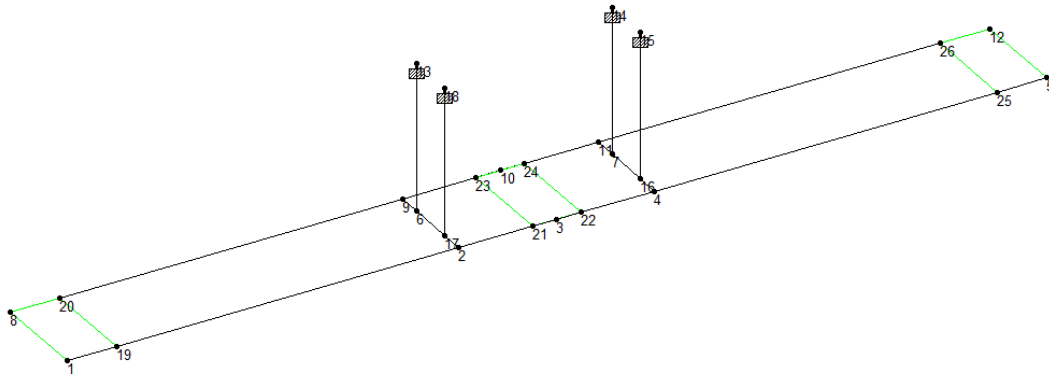
L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1:DL	Loads	0.000	-0.151	0.000	1.808	0.000	-0.659
1:DL	Reactions	0.000	0.151	0.000	-1.808	0.000	0.659
	Difference	0.000	-0.000	0.000	0.000	0.000	-0.000
2:W1	Loads	0.059	0.000	-0.055	-0.382	0.703	-0.415
2:W1	Reactions	-0.059	0.000	0.055	0.382	-0.703	0.415
	Difference	0.000	0.000	-0.000	-0.000	0.000	0.000
3:0.75W2	Loads	0.044	0.000	-0.042	-0.288	0.528	-0.312
3:0.75W2	Reactions	-0.044	0.000	0.042	0.288	-0.528	0.312
	Difference	0.000	0.000	-0.000	-0.000	0.000	0.000



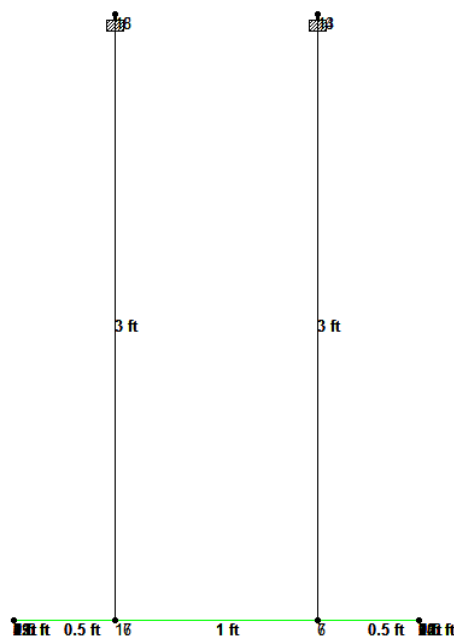
Straddle Bent- Middle

The following structure spacing was accommodated from analyzing the THEA contract plans reinforcement for the straddle bent middle. Based on which superstructure the structure is placed the distances will vary. An analysis of 4 feet width for the middle section was used.

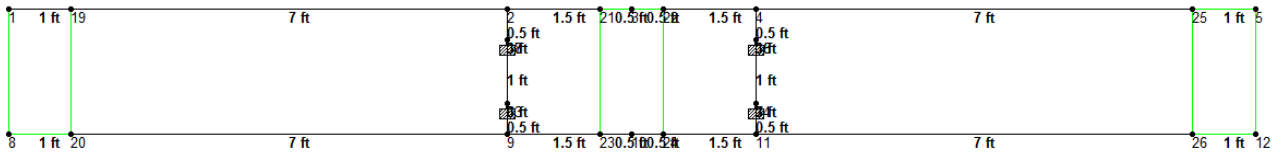
3D View-Length:



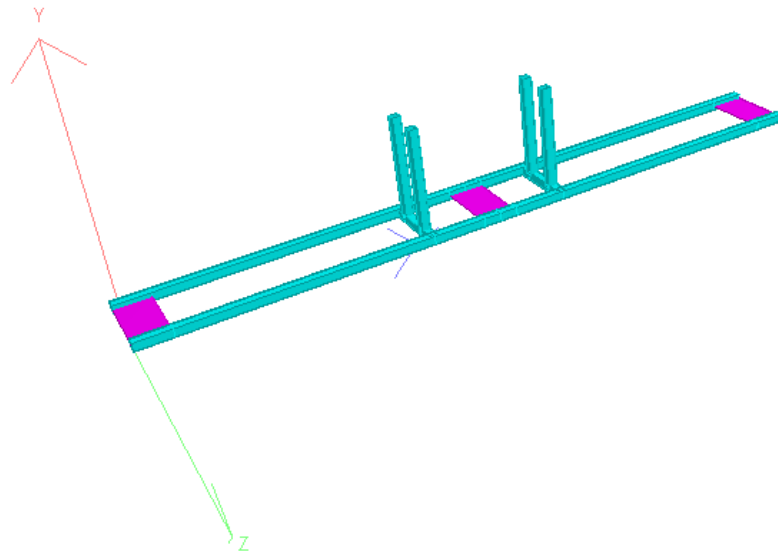
Side View:



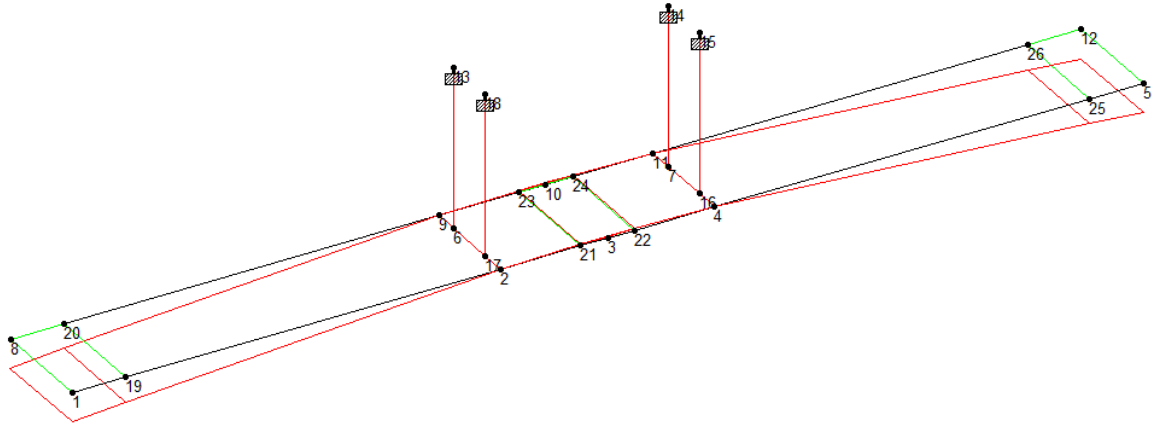
Plan View:



3D View:



Deflection View:





Existing Structural Plans

DATE	SCALE	REVISION NUMBER
X	FLA 50-30-001 & 51-30-01	1562

PROJECT NO.	CONSTRUCTION PROJECT NO.
S.R. 618	THCEA 5140.01

OWNER	ENGINEER OF RECORD
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	Florida Bridge Engineers

PROJECT NAME	STRUCTURE NOS. 100800, 100806 & 100812
CONTRACT NO.	9'-4" TYPICAL SEGMENT DIMENSIONS (47'-0" BOX)

COUNTY	CONTRACT PROJECT NO.
HILLSBOROUGH	THCEA 5140.01

SECTION	NO.
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE	1-368

DATE	BY	DESCRIPTION

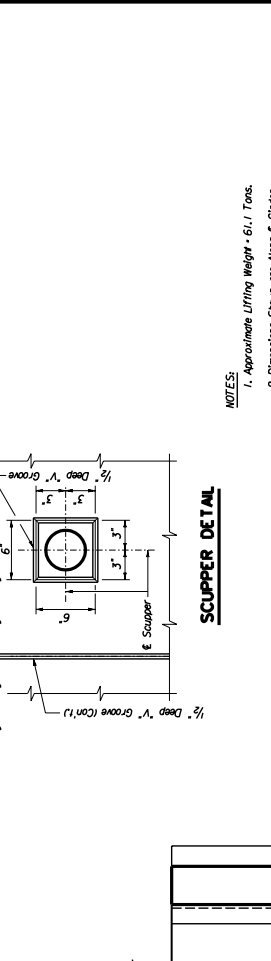
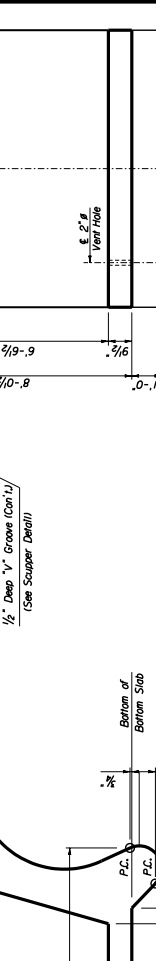
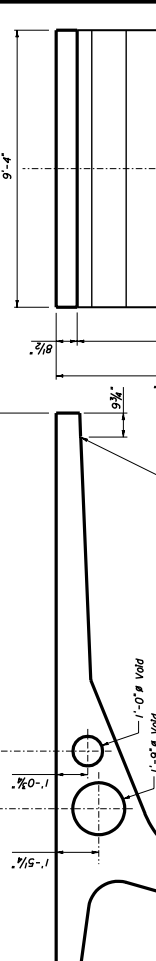
NO.	DATE	REVISIONS

Drawn by	12-13-02	JKF
Checked by	12-13-02	AKK
Designed by	12-13-02	WJP
Checked by	12-13-02	JMR
Approved by	J. Rodriguez	

PROJECT NAME	STRUCTURE NOS. 100800, 100806 & 100812
CONTRACT NO.	9'-4" TYPICAL SEGMENT DIMENSIONS (47'-0" BOX)

COUNTY	CONTRACT PROJECT NO.
HILLSBOROUGH	THCEA 5140.01

OWNER	ENGINEER OF RECORD
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	Florida Bridge Engineers



NOTES:

1. Approximate Lifting Weight - 61.1 Tons.
2. Dimensions Shown are Along E Girder.
3. For Bottom Slab Access Details, See Miscellaneous Superstructure Details Sheet.
4. For Variable Segment Dimensions, see Variable Segment Dimensions Sheets.
5. Scupper to be provided in Segments Indicated in Variable Segment Dimensions Sheet. Contractor must address milling of deck when placing top of scupper pipe location. For Segments with Drain Inlets Specified, see Drainage Details Sheet and refer to Drain Segment Construction and Reinforcement Sheets for 25'-0" Box for Details.
6. For Vent Hole Location, See Variable Segment Dimensions Sheets.

DATE	BY	DESCRIPTION

NO.	DATE	REVISIONS

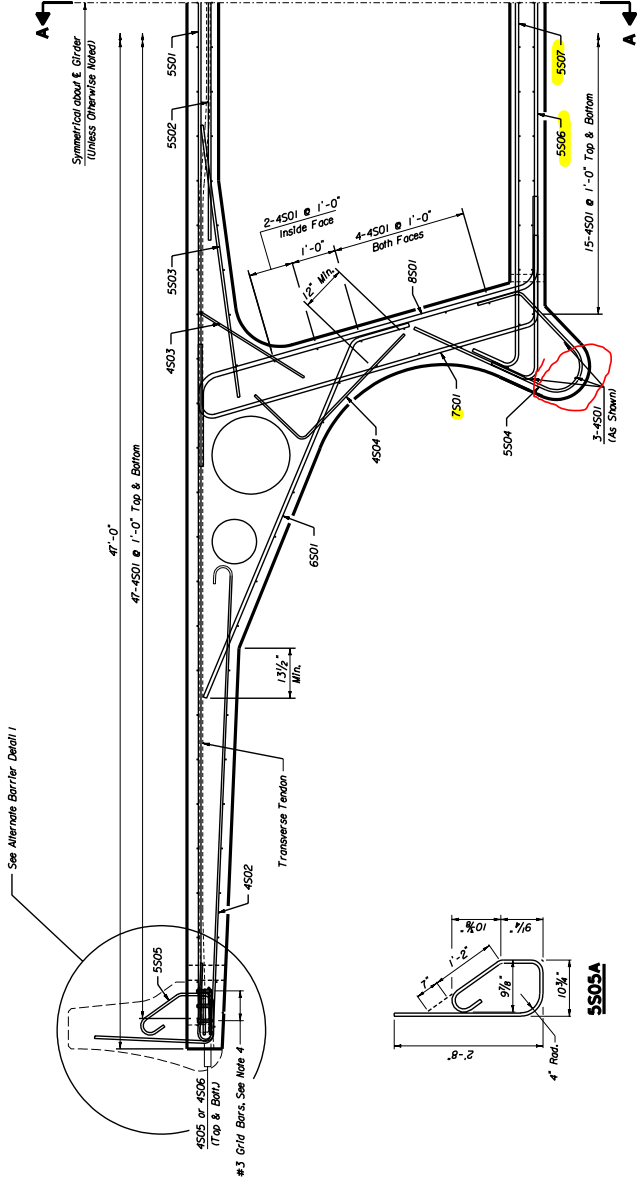
Drawn by	12-13-02	JKF
Checked by	12-13-02	AKK
Designed by	12-13-02	WJP
Checked by	12-13-02	JMR
Approved by	J. Rodriguez	

PROJECT NAME	STRUCTURE NOS. 100800, 100806 & 100812
CONTRACT NO.	9'-4" TYPICAL SEGMENT DIMENSIONS (47'-0" BOX)

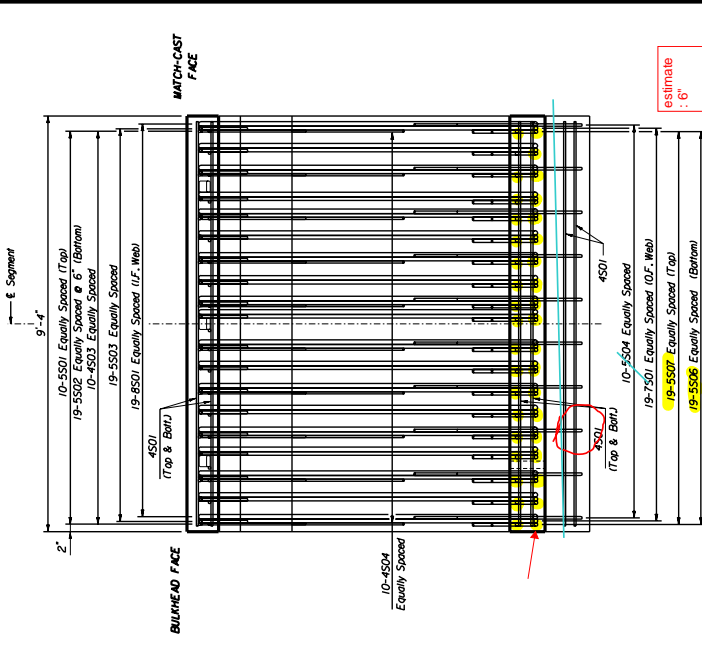
COUNTY	CONTRACT PROJECT NO.
HILLSBOROUGH	THCEA 5140.01

OWNER	ENGINEER OF RECORD
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	Florida Bridge Engineers

PROJECT NO.	DATE	REVISION NO.
X FLA 50-30-001 & 51-30-01	10/2	10/2



HALF-ELEVATION



SECTION A-A

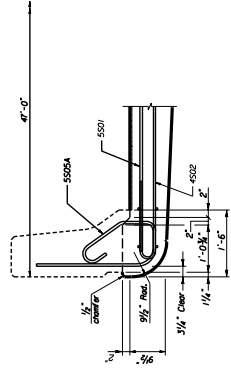
NOTE:

- Concrete Cover: 3/4" • Top of Top Slab
1 1/2" • All Interior Faces
2" • All Exterior Faces
- Space All Reinforcing Steel In Top Slab To Clear Transverse Tendons and Drains.
- For Transverse P.T. Details, See Sheet T-440.
- #3 Grid Bars and Bar #101 are Detailed on Sheet T-440.
- The Contractor May Use Either the Typical or Alternate Barrier Shown on Sheet T-6. Contractor Shall make Adjustments to Slab Dimensions and local labor as Shown to Accommodate the Alternate Barrier Shape.

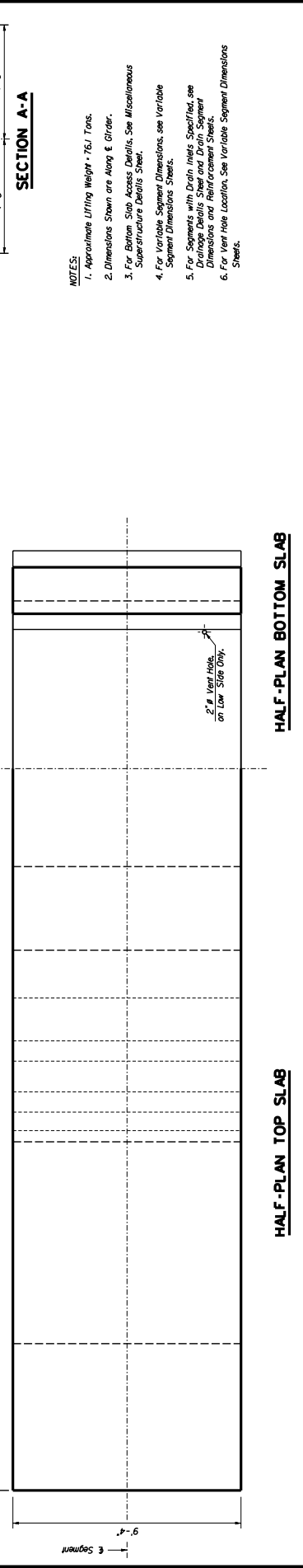
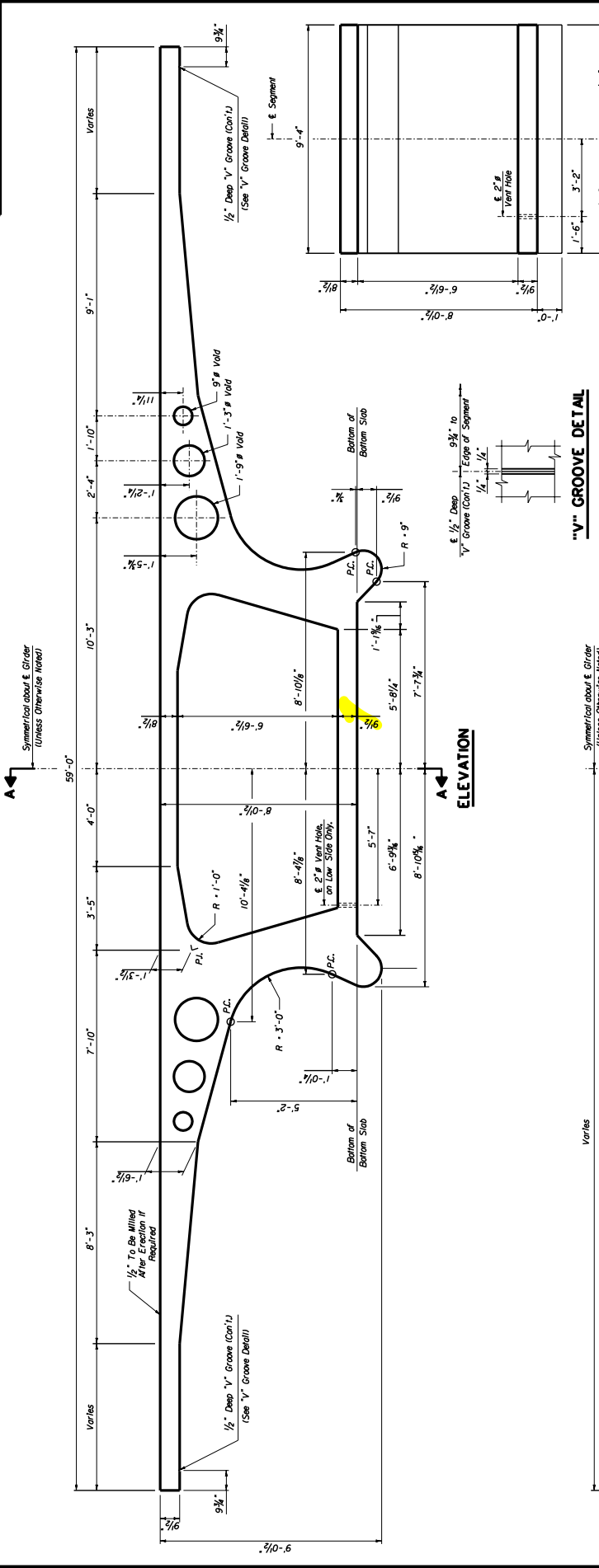
DATE		DESCRIPTION		REVISIONS		ENGINEER OF RECORD		LOGO		SEAL		PROJECT NAME		DRAWING NO.	
													TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		T-369
													SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE		
													STRUCTURE NOS. 100800, 100806 & 100812		
													9'-4" TYPICAL SEGMENT REINFORCEMENT (147'-0" BOX)		
													SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE		
													CONSTRUCTION PROJECT NO.		
													THCEA 5140.01		
													COUNTY		
													HILLSBOROUGH		
													SHEET NO.		
													T-369		

ALTERNATE BARRIER DETAIL 1

(SEE NOTE 5)



DATE	SCALE	REVISION
12/13/02	1/4" = 1'-0"	1. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.
12/13/02	1/4" = 1'-0"	2. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.
12/13/02	1/4" = 1'-0"	3. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.
12/13/02	1/4" = 1'-0"	4. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.
12/13/02	1/4" = 1'-0"	5. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.
12/13/02	1/4" = 1'-0"	6. REVISED TO ADD 2" DIA. VENT HOLES ON LOW SIDE ONLY.



NOTES:

1. Approximate Lifting Weight - 76.1 Tons.
2. Dimensions Shown are Along ϵ Girder.
3. For Bottom Slab Access Details, See Miscellaneous Superstructure Details Sheet.
4. For Variable Segment Dimensions, see Variable Segment Dimensions Sheets.
5. For Segments with Depth Inside Specified, see Drainage Details Sheet and Drain Segment Dimensions and Reinforcement Sheets.
6. For Vent Hole Location, See Variable Segment Dimensions Sheets.

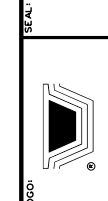
DATE	BY	DESCRIPTION

REVISIONS	DATE	BY	DESCRIPTION

DATE	BY	DESCRIPTION
12-13-02	JSR	DESIGNED
12-13-02	MJP	CHECKED
12-13-02	MJP	DESIGNED
12-13-02	MJP	CHECKED
12-13-02	J. Rodriguez	APPROVED

ENGINEER OF RECORD:

 Five Bridges Engineers, Inc.
 124 W. Collier Street
 Tallahassee, Florida 32301
 Florida Professional Engineer No. 5332
 J. Rodriguez, P.E., Member, P.E., Professional P.E.



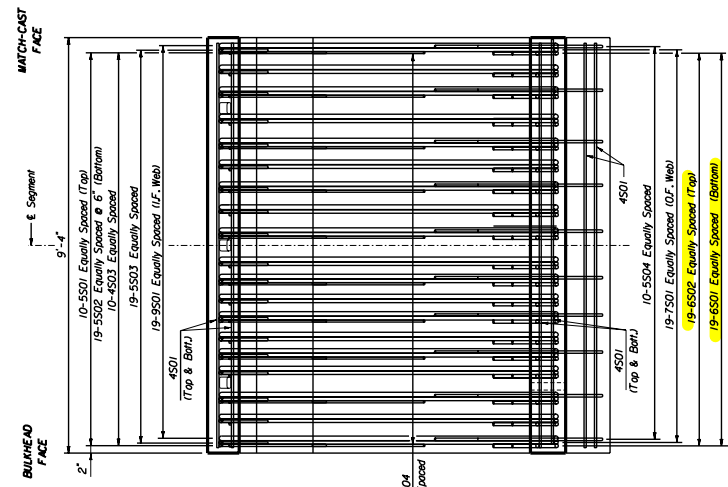
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY
 COUNTY: HILLSBOROUGH
 PROJECT NO.: THCEA 5140.01

STRUCTURE NOS. 100800, 100806 & 100812
9'-4" TYPICAL SEGMENT DIMENSIONS (59'-0" BOX)
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE

HALF-PLAN TOP SLAB

HALF-PLAN BOTTOM SLAB

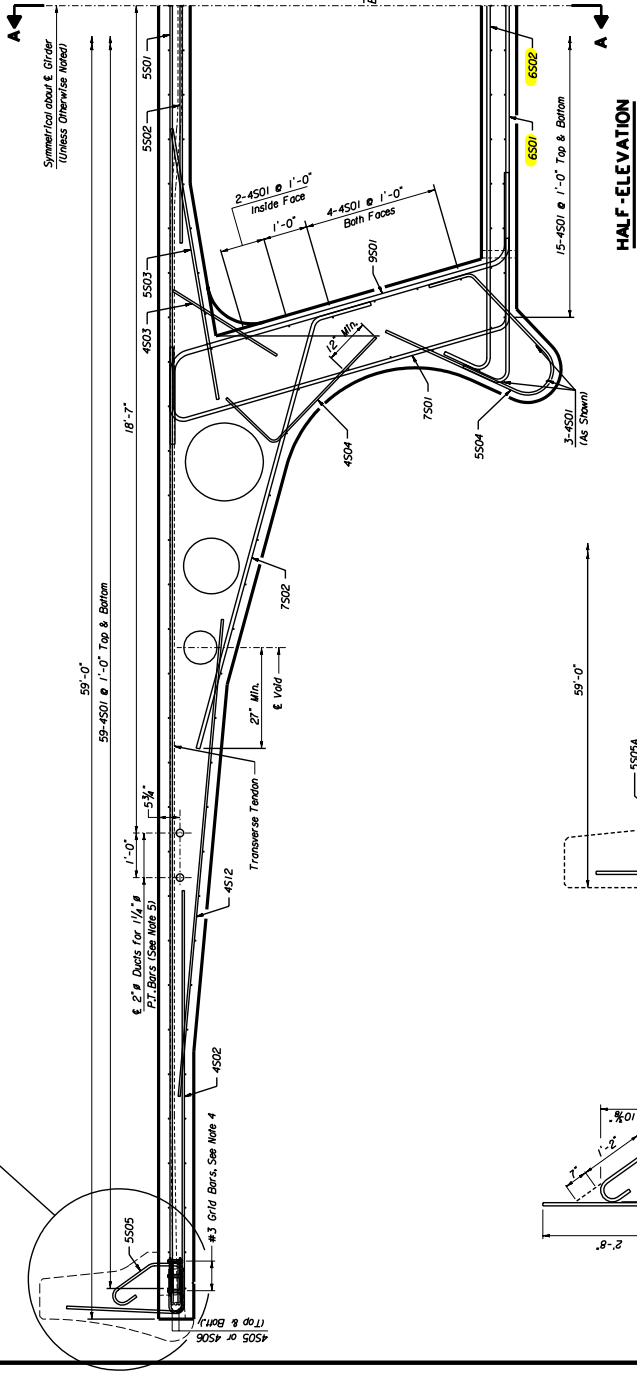
DATE	SCALE	REVISION
12/13/02	1/4" = 1'-0"	1
12/13/02	1/4" = 1'-0"	2
12/13/02	1/4" = 1'-0"	3
12/13/02	1/4" = 1'-0"	4
12/13/02	1/4" = 1'-0"	5
12/13/02	1/4" = 1'-0"	6
12/13/02	1/4" = 1'-0"	7
12/13/02	1/4" = 1'-0"	8
12/13/02	1/4" = 1'-0"	9
12/13/02	1/4" = 1'-0"	10
12/13/02	1/4" = 1'-0"	11
12/13/02	1/4" = 1'-0"	12
12/13/02	1/4" = 1'-0"	13
12/13/02	1/4" = 1'-0"	14
12/13/02	1/4" = 1'-0"	15
12/13/02	1/4" = 1'-0"	16
12/13/02	1/4" = 1'-0"	17
12/13/02	1/4" = 1'-0"	18
12/13/02	1/4" = 1'-0"	19
12/13/02	1/4" = 1'-0"	20
12/13/02	1/4" = 1'-0"	21
12/13/02	1/4" = 1'-0"	22
12/13/02	1/4" = 1'-0"	23
12/13/02	1/4" = 1'-0"	24
12/13/02	1/4" = 1'-0"	25
12/13/02	1/4" = 1'-0"	26
12/13/02	1/4" = 1'-0"	27
12/13/02	1/4" = 1'-0"	28
12/13/02	1/4" = 1'-0"	29
12/13/02	1/4" = 1'-0"	30
12/13/02	1/4" = 1'-0"	31
12/13/02	1/4" = 1'-0"	32
12/13/02	1/4" = 1'-0"	33
12/13/02	1/4" = 1'-0"	34
12/13/02	1/4" = 1'-0"	35
12/13/02	1/4" = 1'-0"	36
12/13/02	1/4" = 1'-0"	37
12/13/02	1/4" = 1'-0"	38
12/13/02	1/4" = 1'-0"	39
12/13/02	1/4" = 1'-0"	40
12/13/02	1/4" = 1'-0"	41
12/13/02	1/4" = 1'-0"	42
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12/13/02	1/4" = 1'-0"	45
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12/13/02	1/4" = 1'-0"	47
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12/13/02	1/4" = 1'-0"	50
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12/13/02	1/4" = 1'-0"	54
12/13/02	1/4" = 1'-0"	55
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12/13/02	1/4" = 1'-0"	97
12/13/02	1/4" = 1'-0"	98
12/13/02	1/4" = 1'-0"	99
12/13/02	1/4" = 1'-0"	100



SECTION A-A

NOTE:

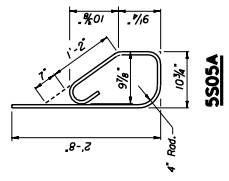
- Concrete Cover: 2 1/2" - Top of Top Slab
1 1/2" - Interior Faces
2" - All Exterior Faces
- Space All Reinforcing Steel in Top Slab To Clear Transverse Tendons and Drains.
- For Transverse P.T. Details, See Sheet T-441.
- #3 Grid Bars and Bar 4T01 are Detailed on Sheet T-441.
- For Segments with 2" # Ducts for 1/4" Wing P.T. Bars, See Variable Segment Dimensions Sheets.
- The Contractor May Use Either the Typical or Alternate Barrier Shown on Sheet T-6. Contractor Shall make Adjustments to Slab Dimensions and Local Floor as Shown to Accommodate the Alternate Barrier Shape.



HALF-ELEVATION

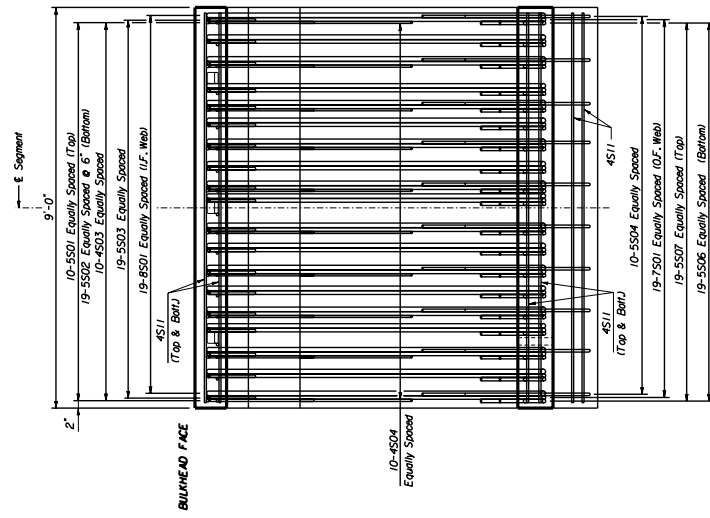
ALTERNATE BARRIER DETAIL 1

(SEE NOTE 6)



DATE		DESCRIPTION		BY		DATE		DESCRIPTION		BY	
<p>ENGINEER OF RECORD: FLORIAN BRIDGE EXPERTS 124 N. CAROL STREET TAMPA, FLORIDA 33601 PHONE: 813.288.1100 FAX: 813.288.1101 P.E. No. 5332</p>											
<p>LOGO: </p>											
<p>SEAL: </p>											
<p>PROJECT NAME: TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY</p>											
<p>CONSTRUCTION PROJECT NO.: THCEA 5140.01</p>											
<p>FORM NO.: S.R. 618</p>											
<p>COUNTY: HILLSBOROUGH</p>											
<p>PROJECT NO.: 1-373</p>											
<p>DATE: 12/13/02</p>											
<p>BY: J. Rodriguez</p>											
<p>APPROVED BY: J. Rodriguez</p>											
<p>STRUCTURE NOS. 100800, 100806 & 100812</p>											
<p>9'-4" TYPICAL SEGMENT REINFORCEMENT (159'-0" BOX)</p>											
<p>SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE</p>											

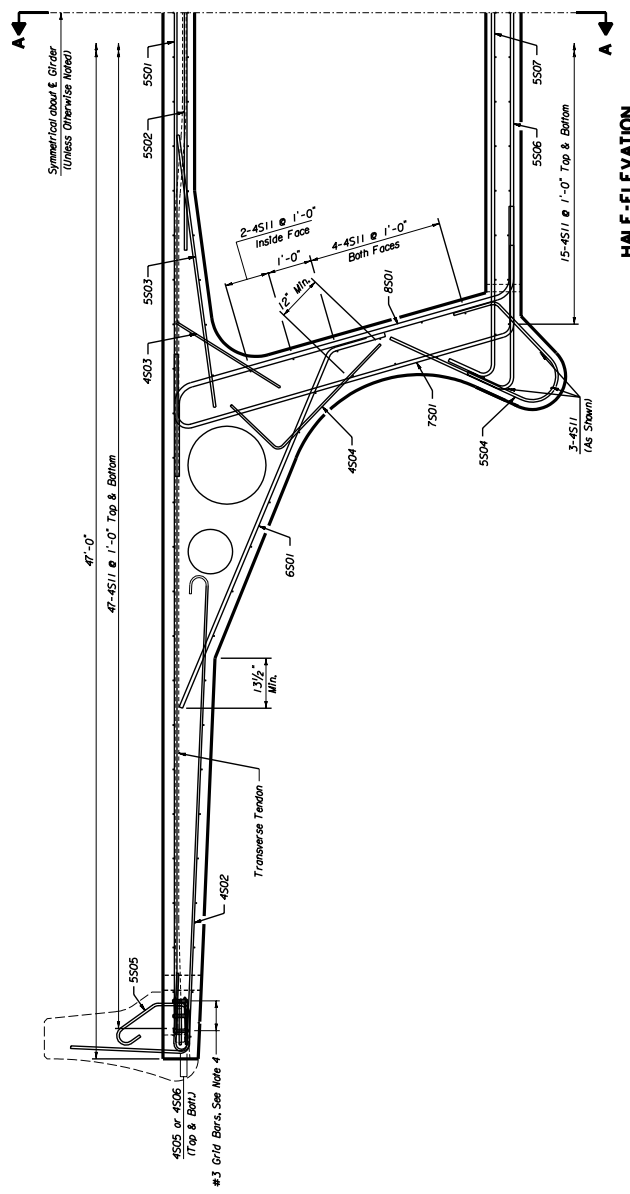
DATE	SCALE	REVISION NUMBER	BY
X	FLA 50-30-001 & 51-30-01		



SECTION A-A

NOTE:

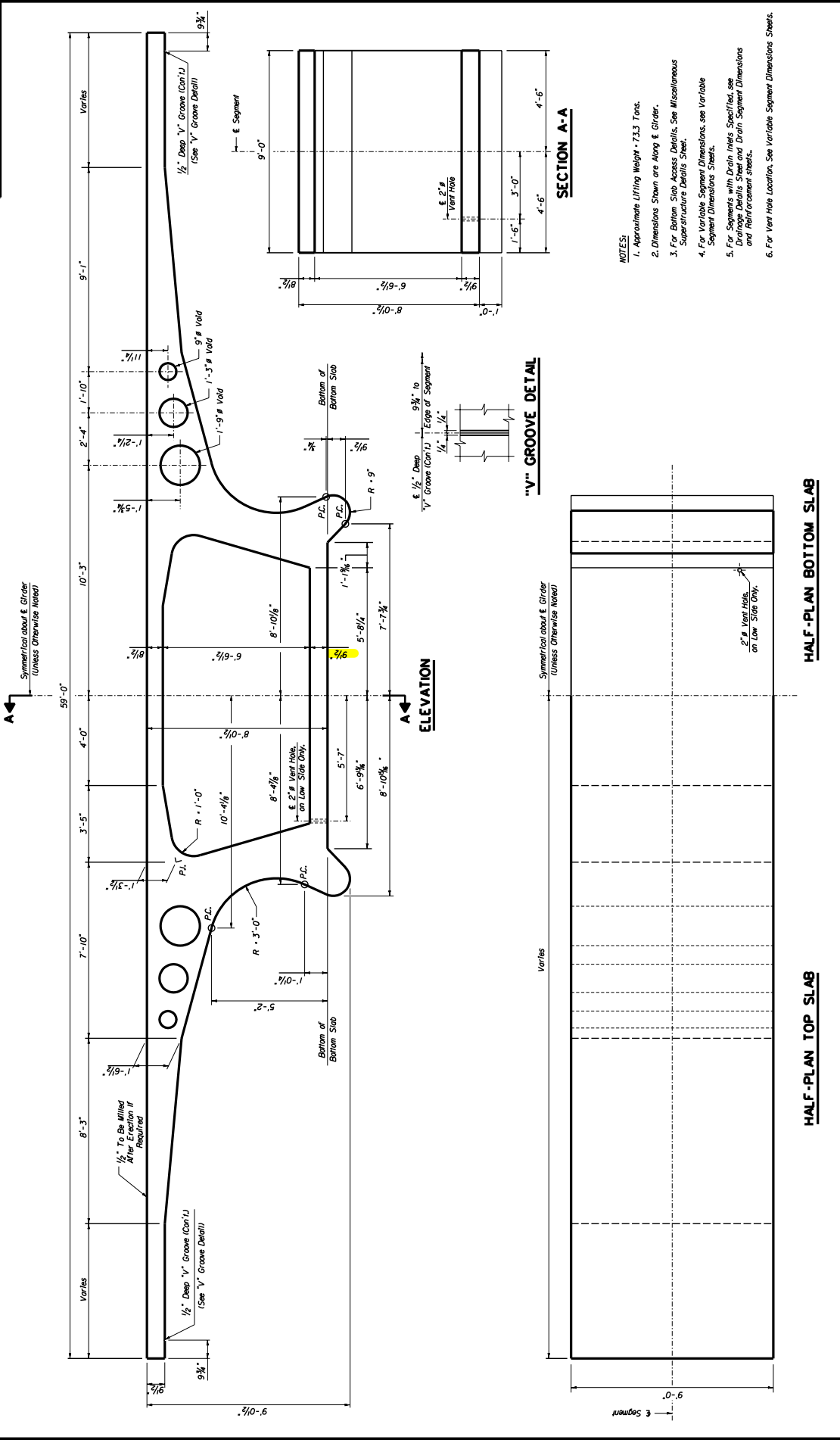
1. Concrete Cover: 2 1/2" - Top of Top Slab
1 1/2" - All Interior Faces
2" - All Exterior Faces
2. Space All Reinforcing Steel in Top Slab To Clear Transverse Tendons and Drains.
3. For Transverse P.T. Details, See Sheet T-440.
4. #3 Grid Bars and Bar #101 are Detailed on Sheet T-440.
5. For Wing Details with Alternate Barriers, see Sheet T-369.



DATE		DESCRIPTION		BY	
REVISIONS					
DRAWN BY		CHECKED BY		APPROVED BY	
J.S.F.		M.P.R.		J. Rodriguez	
DESIGNED BY		DATE		PROJECT NO.	
R.G.T.		12-13-02		100800, 100806 & 100812	
DATE		DESCRIPTION		PROJECT NAME	
12-13-02				TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	
12-13-02				9'-0" TYPICAL SEGMENT REINFORCEMENT (147'-0" BOX)	
12-13-02				SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE	
				CONSTRUCTION PROJECT NO.	
				THCEA 51401.01	
				COUNTY	
				HILLSBOROUGH	
				SHEET TITLE	
				STRUCTURE NOS. 100800, 100806 & 100812	
				DRAWING NO.	
				T-381	
				SCALE	
				LOGO	
				ENGINEER OF RECORD	
				J. Rodriguez	
				DATE	
				12-13-02	
				PROJECT NO.	
				100800, 100806 & 100812	
				PROJECT NAME	
				TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	
				SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE	
				CONSTRUCTION PROJECT NO.	
				THCEA 51401.01	
				COUNTY	
				HILLSBOROUGH	
				SHEET TITLE	
				STRUCTURE NOS. 100800, 100806 & 100812	
				DRAWING NO.	
				T-381	

12 DEC 2002 19:43:01

DATE	SCALE	DESIGN PROJECT NO.
X	FLA 50-30-001 & 51-30-01	1082



DATE	BY	DESCRIPTION

DESIGNED BY	DATE	ENGINEER OF RECORD
MJP	12-13-02	Five Bridge Engineers

PROJECT NAME	CONSTRUCTION PROJECT NO.
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE	THCEA 5140.01

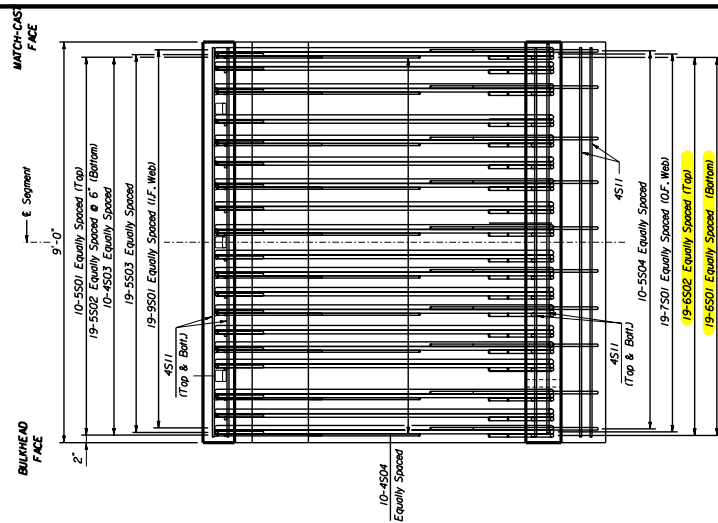
FORM NO.	COUNTY	SEAL
S.R. 618	HILLSBOROUGH	

PROJECT NO.	PROJECT NO.
1-384	100812

STRUCTURE NOS. 100800, 100806 & 100812

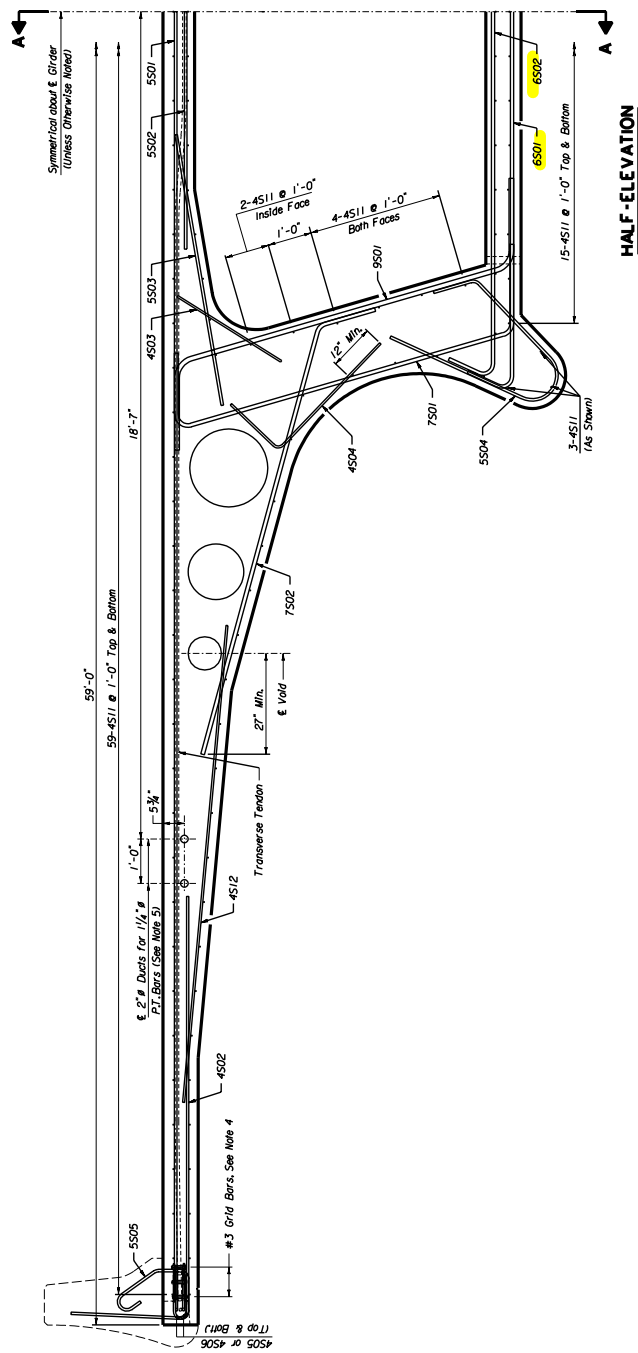
9'-0" TYPICAL SEGMENT DIMENSIONS (59'-0" BOX)

DATE	12/13/02
BY	J.R.
PROJECT NO.	FLA 50-30-001 & 51-30-01



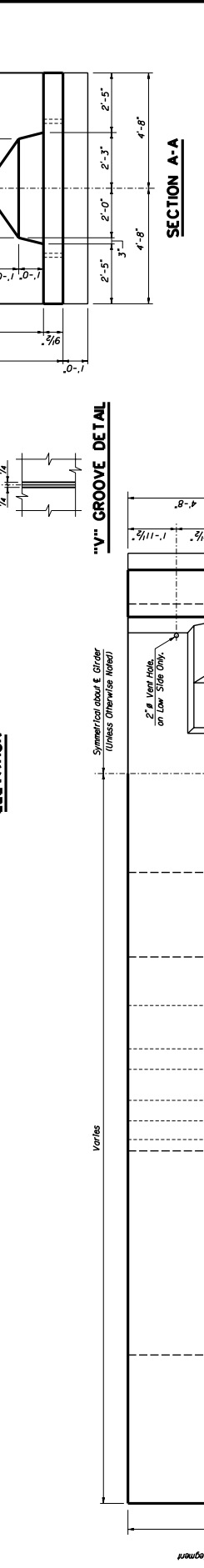
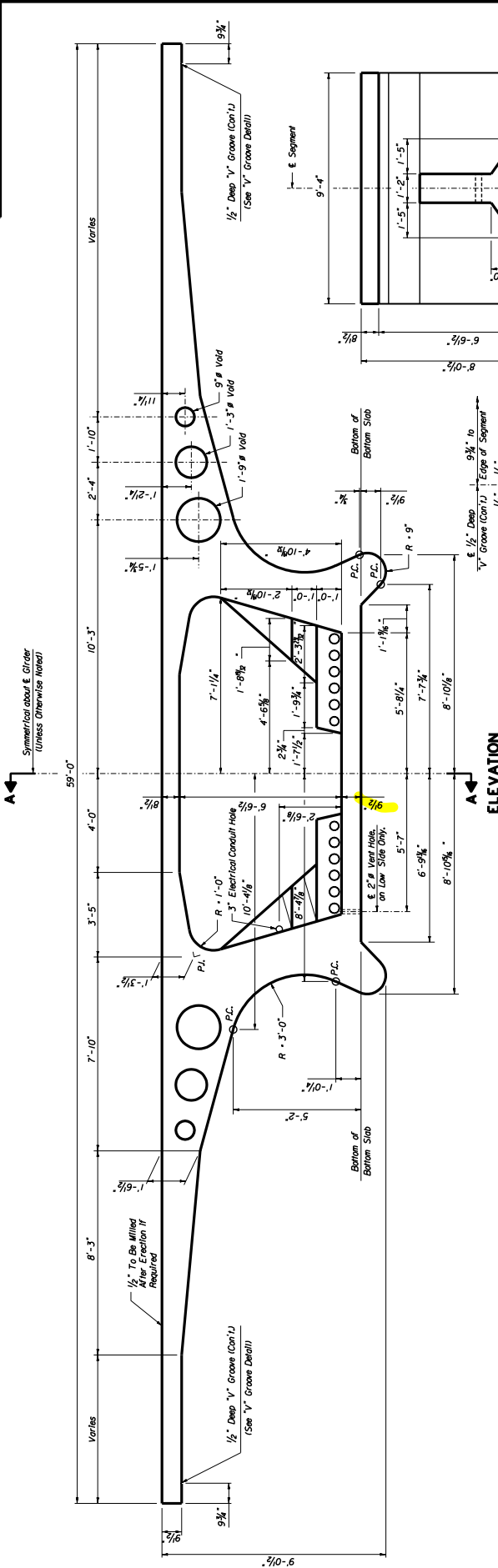
NOTE

1. Concrete Cover: 2 1/2" - Top of Top Slab
1 1/2" - All Interior Faces
2" - All Exterior Faces
2. Space All Reinforcing Steel in Top Slab To Clear Transverse Tendons and Drains.
3. For Transverse P.T. Details, See Sheet T-441.
4. #3 Grid Bars and Bar 4T01 are Detailed on Sheet T-441.
5. For Segments with 2" # Ducts for 1/4" P.T. Bars, See Variable Segment Dimensions Sheets.
6. For Wing Details with Alternate Barrier, see Sheet T-373.



DATE		DESCRIPTION		BY		DATE		DESCRIPTION	
REVISIONS									
Drawn by	JSF	12-13-02	ENGINEER OF RECORD						
Checked by	MR	12-13-02	DATE						
Designed by	MR	12-13-02	PROJECT NO.						
Checked by	MR	12-13-02	COUNTY						
Approved by	J. Rodriguez		CONSTRUCTION PROJECT NO.						
			FORM NO.						
			S.R. 618						
			HILLSBOROUGH COUNTY						
			HILLSBOROUGH						
			THCEA 5140.01						
			TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY						
			STRUCTURE NOS. 100800, 100806 & 100812						
			9'-0" TYPICAL SEGMENT REINFORCEMENT (159'-0" BOX)						
			SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE						
			T-385						

DATE	SCALE	REVISION
12/13/02	1/4" = 1'-0"	1
12/13/02	1/4" = 1'-0"	2
12/13/02	1/4" = 1'-0"	3
12/13/02	1/4" = 1'-0"	4
12/13/02	1/4" = 1'-0"	5
12/13/02	1/4" = 1'-0"	6
12/13/02	1/4" = 1'-0"	7
12/13/02	1/4" = 1'-0"	8
12/13/02	1/4" = 1'-0"	9
12/13/02	1/4" = 1'-0"	10
12/13/02	1/4" = 1'-0"	11
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12/13/02	1/4" = 1'-0"	14
12/13/02	1/4" = 1'-0"	15
12/13/02	1/4" = 1'-0"	16
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12/13/02	1/4" = 1'-0"	32
12/13/02	1/4" = 1'-0"	33
12/13/02	1/4" = 1'-0"	34
12/13/02	1/4" = 1'-0"	35
12/13/02	1/4" = 1'-0"	36
12/13/02	1/4" = 1'-0"	37
12/13/02	1/4" = 1'-0"	38
12/13/02	1/4" = 1'-0"	39
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12/13/02	1/4" = 1'-0"	41
12/13/02	1/4" = 1'-0"	42
12/13/02	1/4" = 1'-0"	43
12/13/02	1/4" = 1'-0"	44
12/13/02	1/4" = 1'-0"	45
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12/13/02	1/4" = 1'-0"	47
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12/13/02	1/4" = 1'-0"	49
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12/13/02	1/4" = 1'-0"	51
12/13/02	1/4" = 1'-0"	52
12/13/02	1/4" = 1'-0"	53
12/13/02	1/4" = 1'-0"	54
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12/13/02	1/4" = 1'-0"	62
12/13/02	1/4" = 1'-0"	63
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12/13/02	1/4" = 1'-0"	65
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12/13/02	1/4" = 1'-0"	79
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12/13/02	1/4" = 1'-0"	81
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12/13/02	1/4" = 1'-0"	95
12/13/02	1/4" = 1'-0"	96
12/13/02	1/4" = 1'-0"	97
12/13/02	1/4" = 1'-0"	98
12/13/02	1/4" = 1'-0"	99
12/13/02	1/4" = 1'-0"	100



NOTES:

1. Approximate Lifting Weight - 781 Tons.
2. Dimensions Shown are Along ϵ Girder.
3. For Variable Segment Dimensions, see Variable Segment Dimensions Sheets.
4. For Vent Hole Location, see Variable Segment Dimensions Sheets.
5. For Epoxy Joint Details, see Epoxy Joint Details Sheets.

HALF-PLAN TOP SLAB

HALF-PLAN BOTTOM SLAB

STRUCTURE NOS. 100800, 100806 & 100812		SHEET TITLE	
9'-4" DEVIATION SEGMENT DIMENSIONS (59'-0" BOX)		DRAWING NO.	
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE		T-395	
PROJECT NAME		CONSTRUCTION PROJECT NO.	
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		THCEA 5140.01	
COUNTY		S.R. 618	
HILLSBOROUGH		HILLSBOROUGH	
LOGO		ENGINEER OF RECORD	
		J. Rodriguez & Associates, P.A. 124 W. Carson Street Tallahassee, Florida 32301 Phone: 904.438.2222 Fax: 904.438.2222 www.jrodriguez.com	
DATE		DATE	
12 DEC 2002		12-13-02	
DRAWN BY		CHECKED BY	
J. Rodriguez		J. Rodriguez	
DESIGNED BY		APPROVED BY	
M. Rodriguez		J. Rodriguez	
DESCRIPTION		DESCRIPTION	
9'-4" ϵ Segment		9'-4" ϵ Segment	

NO.	DATE	BY	DESCRIPTION
1	12-13-02	JRF	Drawn by
2	12-13-02	MDR	Checked by
3	12-13-02	MFC	Designed by
4	12-13-02	GGH	Checked by
5	12-13-02	J.Rodriguez	Approved by

ENGINEER OF RECORD:
Five Bridge Engineers
 424 W. Carson Street
 Tallahassee, Florida 32301
 P.E. No. 5332
 J. Rodriguez, P.E., Member, C.E., Professional, P.A.

LOGO

SEAL

CONSTRUCTION PROJECT NO.
 THCEA 5140.01

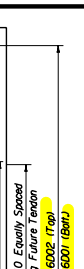
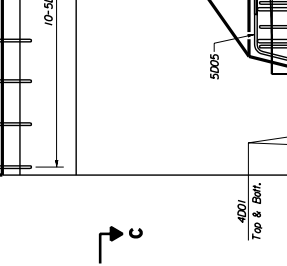
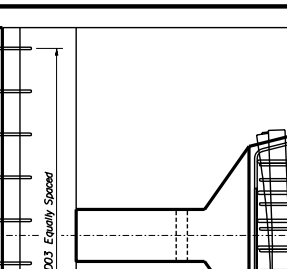
COUNTY
 HILLSBOROUGH

PROJECT NAME
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY

STRUCTURE NOS. 100800, 100806 & 100812

9'-4" DEVIATION SEGMENT REINFORCEMENT 7 - BLOCKS H & J

SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE



NOTES:
 # 1 - Type 'H' Block Shown.
 For Type 'J' Block, Remove Tendon T3 and the 8-5008 Along It.
 2. Concrete Cover: 2 1/2" - Top of Top Slab
 1 1/2" - All Interior Faces
 2" - All Exterior Faces
 3. For Deviation Block Types & Locations, See P.T. Layouts.
 4. For Longitudinal P.T. Details, See P.T. Layouts.
 5. For Transverse P.T. Details, See Steel T-441.
 6. #3 Grid Bars and Bar 4F01 are Detailed on Steel T-441.
 7. Space All Reinforcing Steel To Clear P.T. Tendons.
 8. For Sections E-B & C-C, See Steel T-397.
 9. For Epoxy Joint Details, See Epoxy Joint Details sheets.
 10. For Wing Details with Alternate Barrier, See Steel T-373.

1943-08 12 DEC 2002

REVISIONS

DATE BY DESCRIPTION

1-4006 (Top & Bottom)

1-4007 (Top & Bottom)

1-4008 (Top & Bottom)

1-4009 (Top & Bottom)

1-4010 (Top & Bottom)

1-4011 (Top & Bottom)

1-4012 (Top & Bottom)

1-4013 (Top & Bottom)

NO.	DATE	BY	DESCRIPTION
1	12-13-02	JRF	Drawn by
2	12-13-02	MDR	Checked by
3	12-13-02	MFC	Designed by
4	12-13-02	GGH	Checked by
5	12-13-02	J.Rodriguez	Approved by

ENGINEER OF RECORD:
Five Bridge Engineers
 424 W. Carson Street
 Tallahassee, Florida 32301
 P.E. No. 5332
 J. Rodriguez, P.E., Member, C.E., Professional, P.A.

LOGO

SEAL

CONSTRUCTION PROJECT NO.
 THCEA 5140.01

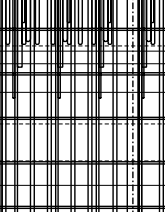
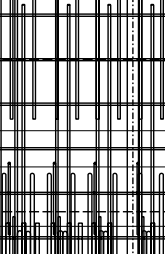
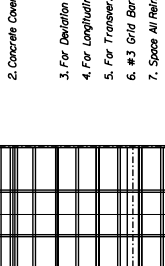
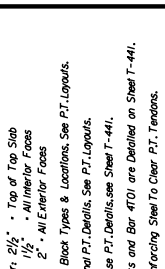
COUNTY
 HILLSBOROUGH

PROJECT NAME
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY

STRUCTURE NOS. 100800, 100806 & 100812

9'-4" DEVIATION SEGMENT REINFORCEMENT 7 - BLOCKS H & J

SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE



NOTES:
 # 1 - Type 'H' Block Shown.
 For Type 'J' Block, Remove Tendon T3 and the 8-5008 Along It.
 2. Concrete Cover: 2 1/2" - Top of Top Slab
 1 1/2" - All Interior Faces
 2" - All Exterior Faces
 3. For Deviation Block Types & Locations, See P.T. Layouts.
 4. For Longitudinal P.T. Details, See P.T. Layouts.
 5. For Transverse P.T. Details, See Steel T-441.
 6. #3 Grid Bars and Bar 4F01 are Detailed on Steel T-441.
 7. Space All Reinforcing Steel To Clear P.T. Tendons.
 8. For Sections E-B & C-C, See Steel T-397.
 9. For Epoxy Joint Details, See Epoxy Joint Details sheets.
 10. For Wing Details with Alternate Barrier, See Steel T-373.

1943-08 12 DEC 2002

REVISIONS

DATE BY DESCRIPTION

1-4006 (Top & Bottom)

1-4007 (Top & Bottom)

1-4008 (Top & Bottom)

1-4009 (Top & Bottom)

1-4010 (Top & Bottom)

1-4011 (Top & Bottom)

1-4012 (Top & Bottom)

NO.	DATE	BY	DESCRIPTION
1	12-13-02	JRF	Drawn by
2	12-13-02	MDR	Checked by
3	12-13-02	MFC	Designed by
4	12-13-02	GGH	Checked by
5	12-13-02	J.Rodriguez	Approved by

ENGINEER OF RECORD:
Five Bridge Engineers
 424 W. Carson Street
 Tallahassee, Florida 32301
 P.E. No. 5332
 J. Rodriguez, P.E., Member, C.E., Professional, P.A.

LOGO

SEAL

CONSTRUCTION PROJECT NO.
 THCEA 5140.01

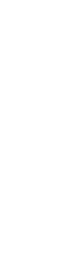
COUNTY
 HILLSBOROUGH

PROJECT NAME
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY

STRUCTURE NOS. 100800, 100806 & 100812

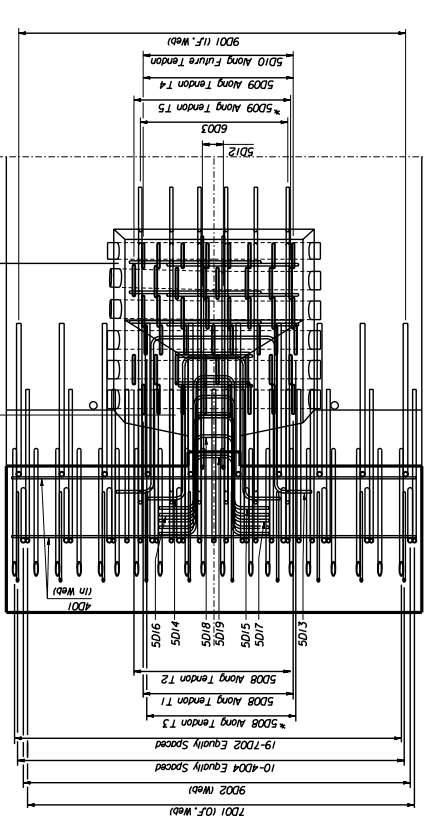
9'-4" DEVIATION SEGMENT REINFORCEMENT 7 - BLOCKS H & J

SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE

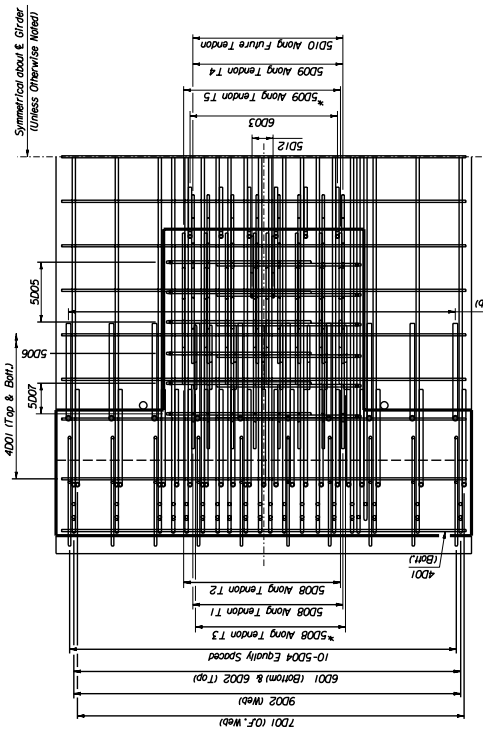


DATE	SCALE	REVISION NUMBER	BY
12/13/02	X	FLA 50-30-001 & 51-30-01	1042

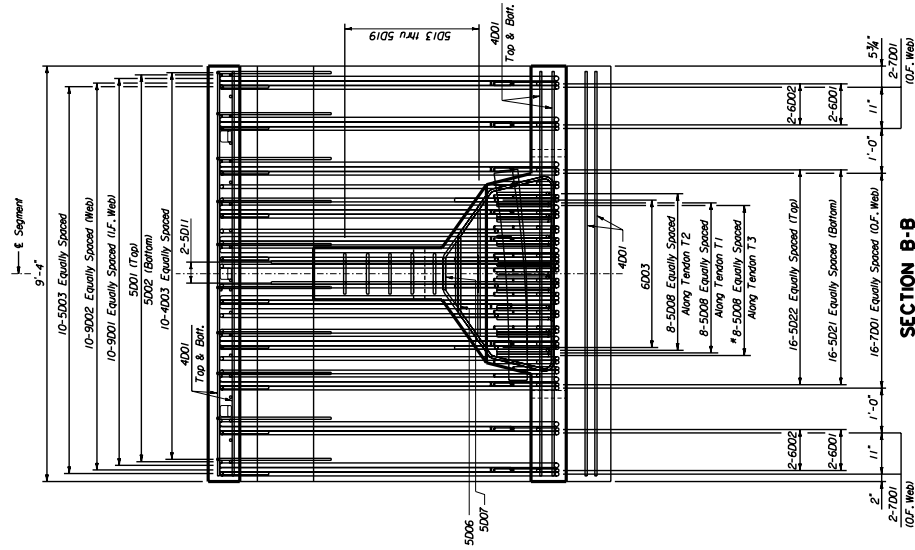
DATE	SCALE	REVISION NUMBER	BY
12/13/02	X	FLA 50-30-001 & 51-30-01	1042



SECTION C-C



SECTION B-B



SECTION B-B

NOTES:

- * 1. Type 'J' Block Shown For Type 'K' Block. Remove Tendon T3 and the 8-5008 Along It.
- * For Type 'O' Block, Remove Tendon T5 and the 8-5009 along It.
- * For Type 'O' Block, Remove Tendon T1 and the 8-5008 along It, and Remove Tendon T5 and the 8-5009 along It.
- 2. Concrete Cover: 2 1/2" - Top of Top Sub 1 1/2" - All Interior Faces 2" - All Exterior Faces
- 3. For Deviation Block Types & Locations, See P.T. Layouts.
- 4. For Longitudinal P.T. Details, See P.T. Layouts.
- 5. Space All Reinforcing Steel To Clear P.T. Tendons.
- 6. For Epoxy Joint Details, see Epoxy Joint Details sheets.

DATE		DESCRIPTION		BY		DATE		DESCRIPTION	
REVISIONS									
DRAWN BY		CHECKED BY		DESIGNED BY		APPROVED BY		DATE	
J.S.F.		M.F.C.		M.F.C.		J. Rodriguez		12/13/02	
<p>ENGINEER OF RECORD: Five Bridge Engineers 424 N. Central Street Tallahassee, Florida 32301 Phone: 904.438.2222 Fax: 904.438.2222 P.E. No. 5332 * Tallahassee, FL * Miami, FL * Jacksonville, FL *</p>									
FORM NO.		COUNT		CONSTRUCTION PROJECT NO.		PROJECT NAME		DRAWING NO.	
S.R. 618		HILLSBOROUGH		THCEA 5140.01		TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		1-399	
STRUCTURE NOS. 100800, 100806 & 100812									
9'-4" DEVIATION SEGMENT REINFORCEMENT - BLOCKS L, K, O & Q									
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE									



ENGINEER OF RECORD: Five Bridge Engineers

DATE: 12-13-02
 DRAWN BY: J.S.F.
 CHECKED BY: M.F.C.
 DESIGNED BY: M.F.C.
 APPROVED BY: J. Rodriguez

PROJECT NAME: TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY
 CONSTRUCTION PROJECT NO.: THCEA 5140.01
 FORM NO.: S.R. 618
 COUNT: HILLSBOROUGH
 DRAWING NO.: 1-399

STRUCTURE NOS. 100800, 100806 & 100812
 9'-4" DEVIATION SEGMENT REINFORCEMENT - BLOCKS L, K, O & Q
 SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE



STAAD Analysis

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*****
*
*          STAAD.Pro V8i SELECTseries6          *
*          Version  20.07.11.70                 *
*          Proprietary Program of              *
*          Bentley Systems, Inc.               *
*          Date=    JUL 19, 2018               *
*          Time=    12:29: 7                   *
*
*          USER ID: Kimley-Horn and Associates  *
*****

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1. STAAD SPACE
INPUT FILE: \\kimley-horn.com\FL_ORL\ORL_Structures\_Projects-Structures\148872000 THEA Lighting Proje.. .STD
2. START JOB INFORMATION
3. ENGINEER DATE 19-JUN-18
4. JOB NAME STRADDLE BENT - MIDDLE
5. JOB CLIENT THEA
6. JOB NO 148872000
7. JOB REV 3
8. ENGINEER NAME IERM
9. END JOB INFORMATION
10. INPUT WIDTH 79
11. UNIT FEET KIP
12. JOINT COORDINATES
13. 1 0 0 0; 2 8 0 0; 3 10 0 0; 4 12 0 0; 5 20 0 0; 6 8 0 -1.5; 7 12 0 -1.5
14. 8 0 0 -2; 9 8 0 -2; 10 10 0 -2; 11 12 0 -2; 12 20 0 -2; 13 8 3 -1.5
15. 14 12 3 -1.5; 15 12 3 -0.5; 16 12 0 -0.5; 17 8 0 -0.5; 18 8 3 -0.5; 19 1 0 0
16. 20 1 0 -2; 21 9.5 0 0; 22 10.5 0 0; 23 9.5 0 -2; 24 10.5 0 -2; 25 19 0 0
17. 26 19 0 -2
18. MEMBER INCIDENCES
19. 1 1 19; 2 2 21; 3 3 22; 4 4 25; 5 2 17; 6 6 9; 7 4 16; 8 7 11; 9 8 20; 10 9 23
20. 11 10 24; 12 11 26; 13 6 13; 14 7 14; 15 18 17; 16 15 16; 17 16 7; 18 17 6
21. 19 19 2; 20 20 9; 21 21 3; 22 22 4; 23 23 10; 24 24 11; 25 25 5; 26 26 12
22. ELEMENT INCIDENCES SHELL
23. 27 1 8 20 19; 28 21 23 24 22; 29 25 26 12 5
24. ELEMENT PROPERTY
25. 27 TO 29 THICKNESS 0.0208333
26. DEFINE MATERIAL START
27. ISOTROPIC STEEL
28. E 4.176E+006
29. POISSON 0.3
30. DENSITY 0.489024
31. ALPHA 6E-006
32. DAMP 0.03
33. TYPE STEEL
34. STRENGTH FY 5184 FU 8352 RY 1.5 RT 1.2
35. ISOTROPIC A500-GR.
36. E 4.176E+006
37. POISSON 0.3
38. DENSITY 0.49

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STAAD SPACE

-- PAGE NO. 2

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39. ALPHA 6E-006
40. DAMP 0.03
41. G 1.6128E-006
42. TYPE STEEL
43. STRENGTH FY 6624 FU 8352 RY 1.1 RT 1.2
44. END DEFINE MATERIAL
45. MEMBER PROPERTY AMERICAN
46. 1 TO 26 TABLE ST HSST3X3X0.188
47. CONSTANTS
48. MATERIAL STEEL MEMB 27 TO 29
49. MATERIAL A500-GR. MEMB 1 TO 26
50. SUPPORTS
51. 13 TO 15 18 FIXED
52. LOAD 1 LOADTYPE DEAD TITLE DL
53. SELFWEIGHT Y -1
54. JOINT LOAD
55. 1 5 8 12 FY -0.015
56. 21 TO 24 FY -0.006
57. LOAD 2 LOADTYPE WIND TITLE W1
58. JOINT LOAD
59. 1 5 8 12 FZ -0.0522
60. 1 5 8 12 MX -0.0324
61. 1 5 8 12 FX 0.0277
62. 1 5 8 12 MZ -0.017
63. LOAD 3 LOADTYPE WIND TITLE W2
64. JOINT LOAD
65. 21 TO 24 FZ -0.007325
66. 21 TO 24 MX -0.004325
67. 21 TO 24 FX 0.006925
68. 21 TO 24 MZ -0.003975
69. LOAD 4 LOADTYPE WIND TITLE 0.75W3
70. JOINT LOAD
71. 1 5 8 12 FZ -0.039
72. 1 5 8 12 MX -0.024
73. 1 5 8 12 FX 0.021
74. 1 5 8 12 MZ -0.013
75. 21 TO 24 FZ -0.00549
76. 21 TO 24 MX -0.00324
77. 21 TO 24 FX 0.00519
78. 21 TO 24 MZ 0.00298
79. LOAD COMB 5 1.25DL
80. 1 1.25
81. LOAD COMB 6 1.1DL+1.0W1
82. 1 1.1 2 1.0
83. LOAD COMB 7 1.1DL+1.0W2
84. 1 1.1 3 1.0
85. PERFORM ANALYSIS PRINT ALL
```

P R O B L E M S T A T I S T I C S

NUMBER OF JOINTS	26	NUMBER OF MEMBERS	26
NUMBER OF PLATES	3	NUMBER OF SOLIDS	0
NUMBER OF SURFACES	0	NUMBER OF SUPPORTS	4

SOLVER USED IS THE OUT-OF-CORE BASIC SOLVER

ORIGINAL/FINAL BAND-WIDTH=	21/	6/	42 DOF	
TOTAL PRIMARY LOAD CASES =	4,	TOTAL DEGREES OF FREEDOM =		132
TOTAL LOAD COMBINATION CASES =	3	SO FAR.		
SIZE OF STIFFNESS MATRIX =	6	DOUBLE KILO-WORDS		
REQRD/AVAIL. DISK SPACE =	12.1/	0.0 MB		

STAAD SPACE

-- PAGE NO. 4

LOADING 1 LOADTYPE DEAD TITLE DL

SELFWEIGHT Y -1.000

ACTUAL WEIGHT OF THE STRUCTURE = 0.421 KIP

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	-0.01	0.00	0.00	0.00	0.00
5	0.00	-0.01	0.00	0.00	0.00	0.00
8	0.00	-0.01	0.00	0.00	0.00	0.00
12	0.00	-0.01	0.00	0.00	0.00	0.00
21	0.00	-0.01	0.00	0.00	0.00	0.00
22	0.00	-0.01	0.00	0.00	0.00	0.00
23	0.00	-0.01	0.00	0.00	0.00	0.00
24	0.00	-0.01	0.00	0.00	0.00	0.00

LOADING 2 LOADTYPE WIND TITLE W1

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.05	0.00	0.00	0.00
5	0.00	0.00	-0.05	0.00	0.00	0.00
8	0.00	0.00	-0.05	0.00	0.00	0.00
12	0.00	0.00	-0.05	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.03	0.00	0.00
5	0.00	0.00	0.00	-0.03	0.00	0.00
8	0.00	0.00	0.00	-0.03	0.00	0.00
12	0.00	0.00	0.00	-0.03	0.00	0.00
1	0.03	0.00	0.00	0.00	0.00	0.00
5	0.03	0.00	0.00	0.00	0.00	0.00
8	0.03	0.00	0.00	0.00	0.00	0.00
12	0.03	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	-0.02
5	0.00	0.00	0.00	0.00	0.00	-0.02
8	0.00	0.00	0.00	0.00	0.00	-0.02
12	0.00	0.00	0.00	0.00	0.00	-0.02

LOADING 3 LOADTYPE WIND TITLE W2

STAAD SPACE

-- PAGE NO. 5

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
21	0.00	0.00	-0.01	0.00	0.00	0.00
22	0.00	0.00	-0.01	0.00	0.00	0.00
23	0.00	0.00	-0.01	0.00	0.00	0.00
24	0.00	0.00	-0.01	0.00	0.00	0.00
21	0.00	0.00	0.00	-0.00	0.00	0.00
22	0.00	0.00	0.00	-0.00	0.00	0.00
23	0.00	0.00	0.00	-0.00	0.00	0.00
24	0.00	0.00	0.00	-0.00	0.00	0.00
21	0.01	0.00	0.00	0.00	0.00	0.00
22	0.01	0.00	0.00	0.00	0.00	0.00
23	0.01	0.00	0.00	0.00	0.00	0.00
24	0.01	0.00	0.00	0.00	0.00	0.00
21	0.00	0.00	0.00	0.00	0.00	-0.00
22	0.00	0.00	0.00	0.00	0.00	-0.00
23	0.00	0.00	0.00	0.00	0.00	-0.00
24	0.00	0.00	0.00	0.00	0.00	-0.00

LOADING 4 LOADTYPE WIND TITLE 0.75W3

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.04	0.00	0.00	0.00
5	0.00	0.00	-0.04	0.00	0.00	0.00
8	0.00	0.00	-0.04	0.00	0.00	0.00
12	0.00	0.00	-0.04	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.02	0.00	0.00
5	0.00	0.00	0.00	-0.02	0.00	0.00
8	0.00	0.00	0.00	-0.02	0.00	0.00
12	0.00	0.00	0.00	-0.02	0.00	0.00
1	0.02	0.00	0.00	0.00	0.00	0.00
5	0.02	0.00	0.00	0.00	0.00	0.00
8	0.02	0.00	0.00	0.00	0.00	0.00
12	0.02	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	-0.01
5	0.00	0.00	0.00	0.00	0.00	-0.01
8	0.00	0.00	0.00	0.00	0.00	-0.01
12	0.00	0.00	0.00	0.00	0.00	-0.01
21	0.00	0.00	-0.01	0.00	0.00	0.00
22	0.00	0.00	-0.01	0.00	0.00	0.00
23	0.00	0.00	-0.01	0.00	0.00	0.00
24	0.00	0.00	-0.01	0.00	0.00	0.00
21	0.00	0.00	0.00	-0.00	0.00	0.00
22	0.00	0.00	0.00	-0.00	0.00	0.00
23	0.00	0.00	0.00	-0.00	0.00	0.00
24	0.00	0.00	0.00	-0.00	0.00	0.00

21	0.01	0.00	0.00	0.00	0.00	0.00
22	0.01	0.00	0.00	0.00	0.00	0.00
23	0.01	0.00	0.00	0.00	0.00	0.00
24	0.01	0.00	0.00	0.00	0.00	0.00
21	0.00	0.00	0.00	0.00	0.00	0.00
22	0.00	0.00	0.00	0.00	0.00	0.00
23	0.00	0.00	0.00	0.00	0.00	0.00
24	0.00	0.00	0.00	0.00	0.00	0.00

*WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 3 EQN.NO. 64
 LOADS APPLIED OR DISTRIBUTED HERE FROM ELEMENTS WILL BE IGNORED.
 THIS MAY BE DUE TO ALL MEMBERS AT THIS JOINT BEING RELEASED OR
 EFFECTIVELY RELEASED IN THIS DIRECTION.
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 10 EQN.NO. 82

Stiffness at the connections is expected since the plates are the major contributing factor. The warning is considered but not a cause for concern in the design.

FOR LOADING - 1
 APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00000E+00	-2.33096E-02	0.00000E+00	0.00000E+00	0.00000E+00	-5.35938E-04
2	0.00000E+00	-2.89406E-02	0.00000E+00	-1.33984E-04	0.00000E+00	2.50551E-02
3	0.00000E+00	-3.21562E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
4	0.00000E+00	-2.89406E-02	0.00000E+00	-1.33984E-04	0.00000E+00	-2.50551E-02
5	0.00000E+00	-2.33096E-02	0.00000E+00	0.00000E+00	0.00000E+00	5.35938E-04
6	0.00000E+00	-1.44703E-02	0.00000E+00	4.01953E-04	0.00000E+00	0.00000E+00
7	0.00000E+00	-1.44703E-02	0.00000E+00	4.01953E-04	0.00000E+00	0.00000E+00
8	0.00000E+00	-2.33096E-02	0.00000E+00	0.00000E+00	0.00000E+00	-5.35938E-04
9	0.00000E+00	-2.89406E-02	0.00000E+00	1.33984E-04	0.00000E+00	2.50551E-02
10	0.00000E+00	-3.21562E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
11	0.00000E+00	-2.89406E-02	0.00000E+00	1.33984E-04	0.00000E+00	-2.50551E-02
12	0.00000E+00	-2.33096E-02	0.00000E+00	0.00000E+00	0.00000E+00	5.35938E-04
13	0.00000E+00	-9.64687E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
14	0.00000E+00	-9.64687E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
15	0.00000E+00	-9.64687E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
16	0.00000E+00	-1.44703E-02	0.00000E+00	-4.01953E-04	0.00000E+00	0.00000E+00
17	0.00000E+00	-1.44703E-02	0.00000E+00	-4.01953E-04	0.00000E+00	0.00000E+00
18	0.00000E+00	-9.64687E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
19	0.00000E+00	-3.08190E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.57250E-02
20	0.00000E+00	-3.08190E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.57250E-02
21	0.00000E+00	-1.75252E-02	0.00000E+00	0.00000E+00	0.00000E+00	1.07188E-03
22	0.00000E+00	-1.75252E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03
23	0.00000E+00	-1.75252E-02	0.00000E+00	0.00000E+00	0.00000E+00	1.07188E-03
24	0.00000E+00	-1.75252E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03
25	0.00000E+00	-3.08190E-02	0.00000E+00	0.00000E+00	0.00000E+00	2.57250E-02
26	0.00000E+00	-3.08190E-02	0.00000E+00	0.00000E+00	0.00000E+00	2.57250E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
 LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.229106603E+00
 Z = -0.100000003E+01

STAAD SPACE

-- PAGE NO. 7

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = -0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.51 MY= 0.00 MZ= -5.05

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = -0.00
 SUMMATION FORCE-Y = 0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.51 MY= -0.00 MZ= 5.05

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)
 MAXIMUMS AT NODE
 X = 1.99407E-07 17
 Y = -3.28613E-01 1
 Z = 1.09662E-06 6
 RX= -2.24429E-04 21
 RY= -4.99911E-08 2
 RZ= 4.20218E-03 1

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/	
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ	
							SUPPORT=1
13	0.00	-0.01	0.00	0.00	0.00	0.00	
	0.00	-0.12	-0.01	0.01	0.00	0.00	111111
14	0.00	-0.01	0.00	0.00	0.00	0.00	
	-0.00	-0.12	-0.01	0.01	-0.00	-0.00	111111
15	0.00	-0.01	0.00	0.00	0.00	0.00	
	-0.00	-0.12	0.01	-0.01	0.00	-0.00	111111
18	0.00	-0.01	0.00	0.00	0.00	0.00	
	0.00	-0.12	0.01	-0.01	-0.00	0.00	111111

FOR LOADING - 2
 APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
5	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
8	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
12	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
 LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.613718474E+00
 Z = -0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.620689705E+00
 Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)
 SUMMATION FORCE-X = 0.11
 SUMMATION FORCE-Y = 0.00
 SUMMATION FORCE-Z = -0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.13 MY= 1.98 MZ= -0.07

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)
 SUMMATION FORCE-X = -0.11
 SUMMATION FORCE-Y = 0.00
 SUMMATION FORCE-Z = 0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.13 MY= -1.98 MZ= 0.07

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)
 MAXIMUMS AT NODE
 X = 6.66256E-03 8
 Y = -2.21503E-01 12
 Z = -4.94213E-02 5
 RX= -2.08291E-02 5
 RY= -1.18390E-04 9
 RZ= -2.96009E-03 1

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ

SUPPORT=1

FOR LOADING - 3

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
21	6.92500E-03	0.00000E+00	-7.32500E-03	-4.32500E-03	0.00000E+00	-3.97500E-03
22	6.92500E-03	0.00000E+00	-7.32500E-03	-4.32500E-03	0.00000E+00	-3.97500E-03
23	6.92500E-03	0.00000E+00	-7.32500E-03	-4.32500E-03	0.00000E+00	-3.97500E-03
24	6.92500E-03	0.00000E+00	-7.32500E-03	-4.32500E-03	0.00000E+00	-3.97500E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
LOADTYPE WIND TITLE W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.574007281E+00
Z = -0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.590443686E+00
Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)
SUMMATION FORCE-X = 2.7700000E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -2.9300001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -0.02 MY= 0.27 MZ= -0.02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)
SUMMATION FORCE-X = -2.7700000E-02
SUMMATION FORCE-Y = -1.0928758E-16
SUMMATION FORCE-Z = 2.9300001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 0.02 MY= -0.27 MZ= 0.02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)
MAXIMUMS AT NODE
X = 1.52301E-03 21
Y = -1.87683E-03 1
Z = -5.74874E-04 10
RX= -3.70313E-04 22
RY= 4.79082E-06 2
RZ= 6.31610E-05 6

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ

SUPPORT=1

FOR LOADING - 4

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
-------	---------	---------	---------	-------	-------	-------

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
5	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
8	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
12	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
21	5.19000E-03	0.00000E+00	-5.49000E-03	-3.24000E-03	0.00000E+00	2.98000E-03
22	5.19000E-03	0.00000E+00	-5.49000E-03	-3.24000E-03	0.00000E+00	2.98000E-03
23	5.19000E-03	0.00000E+00	-5.49000E-03	-3.24000E-03	0.00000E+00	2.98000E-03
24	5.19000E-03	0.00000E+00	-5.49000E-03	-3.24000E-03	0.00000E+00	2.98000E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 4
LOADTYPE WIND TITLE 0.75W3

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.382588800E+00
Z = -0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.612272402E+00
Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 4)

SUMMATION FORCE-X = 0.10
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = -0.18

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.11 MY= 1.67 MZ= -0.04

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 4)

SUMMATION FORCE-X = -0.10
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = 0.18

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.11 MY= -1.67 MZ= 0.04

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 4)

MAXIMUMS AT NODE
X = 6.18301E-03 5
Y = -1.63301E-01 12
Z = -3.71637E-02 8
RX= -1.53303E-02 5
RY= 8.70662E-05 4
RZ= -2.18833E-03 1

STAAD SPACE

-- PAGE NO. 11

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
----	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUPPORT=1

LOAD COMBINATION NO. 5
1.25DL

LOADING- 1.
FACTOR - 1.25

LOAD COMBINATION NO. 6
1.1DL+1.0W1

LOADING- 1. 2.
FACTOR - 1.10 1.00

LOAD COMBINATION NO. 7
1.1DL+1.0W2

LOADING- 1. 3.
FACTOR - 1.10 1.00

***** END OF DATA FROM INTERNAL STORAGE *****

86. PARAMETER 2
87. CODE LRFD
88. CHECK CODE ALL

STAAD.Pro CODE CHECKING - (LRFD 3RD EDITION) v1.0

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE Noted)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
1	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.028	2
		0.06 T	0.12	-0.03	1.00
2	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.095	5
		0.00 C	0.00	0.50	0.00
3	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.087	5
		0.00 T	-0.00	0.46	0.50
4	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.095	5
		0.00 C	0.00	0.50	0.00
5	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.030	2
		0.05 C	-0.16	0.00	0.00
6	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.028	6
		0.06 T	0.08	0.07	0.00
7	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.027	2
		0.06 C	0.14	0.00	0.00
8	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.030	2
		0.05 T	-0.16	0.00	0.50
9	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.027	6
		0.11 C	0.12	0.02	1.00
10	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.135	6
		0.38 C	-0.04	0.66	0.00
11	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.126	6
		0.25 C	-0.01	0.65	0.50
12	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.168	6
		0.21 C	-0.18	0.69	0.00
13	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.033	6
		0.05 T	-0.09	0.08	3.00
14	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.034	6
		0.07 T	-0.09	0.09	3.00
15	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.032	2
		0.07 T	-0.08	-0.09	0.00

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
16	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.031	2
		0.09 T	-0.08	-0.08	0.00
17	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.033	6
		0.02 C	0.08	0.09	0.00
18	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.029	6
		0.01 C	-0.07	0.09	0.00
19	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.095	5
		0.00 C	0.00	0.50	7.00
20	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.161	6
		0.26 C	-0.18	0.66	7.00
21	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.087	5
		0.00 T	-0.00	0.46	0.00
22	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.095	5
		0.00 C	0.00	0.50	1.50
23	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.125	6
		0.25 C	-0.01	0.64	0.50
24	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.139	6
		0.38 C	-0.03	0.69	1.50
25	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.029	6
		0.11 T	0.12	0.03	0.00
26	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.033	6
		0.06 C	0.12	0.05	0.00

***** END OF TABULATED RESULT OF DESIGN *****

89. PERFORM ANALYSIS PRINT STATICS CHECK

*WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 3 EQN.NO. 64
 LOADS APPLIED OR DISTRIBUTED HERE FROM ELEMENTS WILL BE IGNORED.
 THIS MAY BE DUE TO ALL MEMBERS AT THIS JOINT BEING RELEASED OR
 EFFECTIVELY RELEASED IN THIS DIRECTION.
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 10 EQN.NO. 82

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
 LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.229106603E+00
 Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = -0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.51 MY= 0.00 MZ= -5.05

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = -0.00
 SUMMATION FORCE-Y = 0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.51 MY= -0.00 MZ= 5.05

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)

MAXIMUMS AT NODE
 X = 1.99407E-07 17
 Y = -3.28613E-01 1
 Z = 1.09662E-06 6
 RX= -2.24429E-04 21
 RY= -4.99911E-08 2
 RZ= 4.20218E-03 1

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
 LOADTYPE WIND TITLE W1

STAAD SPACE

-- PAGE NO. 15

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.613718474E+00
Z = -0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.620689705E+00
Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = 0.11
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = -0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.13 MY= 1.98 MZ= -0.07

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = -0.11
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = 0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.13 MY= -1.98 MZ= 0.07

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)

MAXIMUMS	AT NODE
X = 6.66256E-03	8
Y = -2.21503E-01	12
Z = -4.94213E-02	5
RX= -2.08291E-02	5
RY= -1.18390E-04	9
RZ= -2.96009E-03	1

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
LOADTYPE WIND TITLE W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.574007281E+00
Z = -0.100000003E+01

STAAD SPACE

-- PAGE NO. 16

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.590443686E+00
 Z = -0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 2.7700000E-02
 SUMMATION FORCE-Y = 0.0000000E+00
 SUMMATION FORCE-Z = -2.9300001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.02 MY= 0.27 MZ= -0.02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -2.7700000E-02
 SUMMATION FORCE-Y = -1.0928758E-16
 SUMMATION FORCE-Z = 2.9300001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.02 MY= -0.27 MZ= 0.02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)

	MAXIMUMS	AT NODE
X =	1.52301E-03	21
Y =	-1.87683E-03	1
Z =	-5.74874E-04	10
RX=	-3.70313E-04	22
RY=	4.79082E-06	2
RZ=	6.31610E-05	6

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 4
 LOADTYPE WIND TITLE 0.75W3

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.382588800E+00
 Z = -0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.612272402E+00
 Z = -0.100000003E+01

STAAD SPACE

-- PAGE NO. 17

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 4)

SUMMATION FORCE-X = 0.10
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = -0.18

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.11 MY= 1.67 MZ= -0.04

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 4)

SUMMATION FORCE-X = -0.10
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = 0.18

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.11 MY= -1.67 MZ= 0.04

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 4)

MAXIMUMS AT NODE

X = 6.18301E-03 5
Y = -1.63301E-01 12
Z = -3.71637E-02 8
RX= -1.53303E-02 5
RY= 8.70662E-05 4
RZ= -2.18833E-03 1

***** END OF DATA FROM INTERNAL STORAGE *****

90. FINISH

***** END OF THE STAAD.Pro RUN *****

**** DATE= JUL 19,2018 TIME= 12:29:10 ****

* For technical assistance on STAAD.Pro, please visit *
* <http://selectservices.bentley.com/en-US/> *
* * * * *
* Details about additional assistance from *
* Bentley and Partners can be found at program menu *
* Help->Technical Support *
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Job No
148872000

Sheet No
1

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	19-Jun-18		

Project ID	
Project Name	

Structure Type	SPACE FRAME
-----------------------	-------------

Number of Nodes	26	Highest Node	26
Number of Elements	26	Highest Beam	26
Number of Plates	3	Highest Plate	29

Number of Basic Load Cases	4
Number of Combination Load Cases	3

Included in this printout are data for:

All	The Whole Structure
------------	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	W1
Primary	3	W2
Primary	4	0.75W3
Combination	5	1.25DL
Combination	6	1.1DL+1.0W1
Combination	7	1.1DL+1.0W2

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	19	1.000	2	0
2	2	21	1.500	2	0
3	3	22	0.500	2	0
4	4	25	7.000	2	0
5	2	17	0.500	2	0
6	6	9	0.500	2	0
7	4	16	0.500	2	0
8	7	11	0.500	2	0
9	8	20	1.000	2	0
10	9	23	1.500	2	0
11	10	24	0.500	2	0
12	11	26	7.000	2	0



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Job No
148872000

Sheet No
2

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
16	15	16	3.000	2	0
17	16	7	1.000	2	0
18	17	6	1.000	2	0
19	19	2	7.000	2	0
20	20	9	7.000	2	0
21	21	3	0.500	2	0
22	22	4	1.500	2	0
23	23	10	0.500	2	0
24	24	11	1.500	2	0
25	25	5	1.000	2	0
26	26	12	1.000	2	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
27	1	8	20	19	1
28	21	23	24	22	1
29	25	26	12	5	1

Materials

Mat	Name	E (kip/in ²)	ν	Density (kip/in ³)	α (1/°F)
1	STEEL	29E+3	0.300	0.000	6E-6
2	STAINLESSSTEEL	28E+3	0.300	0.000	10E-6
3	ALUMINUM	10E+3	0.330	0.000	13E-6
4	A500-GR.	29E+3	0.300	0.000	6E-6
5	CONCRETE	3.15E+3	0.170	0.000	5E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
13	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
14	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
15	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
18	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed



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Job No
148872000

Sheet No
3

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	W1	Wind
3	W2	Wind
4	0.75W3	Wind

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
5	1.25DL	1	DL	1.25
6	1.1DL+1.0W1	1	DL	1.10
		2	W1	1.00
7	1.1DL+1.0W2	1	DL	1.10
		3	W2	1.00

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	5	6:1.1DL+1.0W'	0.007	-0.171	-0.049	0.178	-0.021	0.000	-0.002
Min X	7	5:1.25DL	-0.000	-0.000	0.000	0.000	-0.000	-0.000	-0.000
Max Y	1	2:W1	0.006	0.222	-0.049	0.227	-0.021	-0.000	-0.003
Min Y	12	6:1.1DL+1.0W'	0.006	-0.583	-0.049	0.585	-0.021	0.000	-0.008
Max Z	6	5:1.25DL	0.000	-0.000	0.000	0.000	-0.000	0.000	0.000
Min Z	8	6:1.1DL+1.0W'	0.007	-0.552	-0.049	0.554	-0.021	-0.000	0.007
Max rX	24	6:1.1DL+1.0W'	0.006	0.029	-0.002	0.030	0.001	0.000	-0.001
Min rX	5	6:1.1DL+1.0W'	0.007	-0.171	-0.049	0.178	-0.021	0.000	-0.002
Max rY	4	6:1.1DL+1.0W'	0.006	-0.001	-0.003	0.007	0.000	0.000	-0.001
Min rY	9	2:W1	0.006	0.000	-0.003	0.007	0.000	-0.000	0.001
Max rZ	20	6:1.1DL+1.0W'	0.007	-0.468	-0.049	0.471	-0.013	-0.000	0.007
Min rZ	12	6:1.1DL+1.0W'	0.006	-0.583	-0.049	0.585	-0.021	0.000	-0.008
Max Rst	12	6:1.1DL+1.0W'	0.006	-0.583	-0.049	0.585	-0.021	0.000	-0.008



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Beam Displacement Detail Summary

Displacements shown in italic indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	25	2:W1	1.000	0.007	0.190	-0.049	0.197
Min X	4	1:DL	6.300	-0.000	-0.243	0.000	0.243
Max Y	1	2:W1	0.000	0.006	0.222	-0.049	0.227
Min Y	26	6:1.1DL+1.0W1	1.000	0.006	-0.583	-0.049	0.585
Max Z	15	5:1.25DL	2.100	0.000	-0.000	0.000	0.000
Min Z	25	2:W1	1.000	0.007	0.190	-0.049	0.197
Max Rst	26	6:1.1DL+1.0W1	1.000	0.006	-0.583	-0.049	0.585

Beam End Displacement Summary

Displacements shown in italic indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	25	5	2:W1	0.007	0.190	-0.049	0.197
Min X	1	1	1:DL	0.000	-0.329	0.000	0.329
Max Y	1	1	2:W1	0.006	0.222	-0.049	0.227
Min Y	26	12	6:1.1DL+1.0W1	0.006	-0.583	-0.049	0.585
Max Z	6	6	1:DL	0.000	-0.000	0.000	0.000
Min Z	25	5	2:W1	0.007	0.190	-0.049	0.197
Max Rst	26	12	6:1.1DL+1.0W1	0.006	-0.583	-0.049	0.585

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	10	9	2:W1	0.384	-0.009	0.005	-0.000	-0.479	2.615
Min Fx	2	2	6:1.1DL+1.0W1	-0.384	0.018	-0.005	-0.000	-0.334	2.286
Max Fy	8	7	6:1.1DL+1.0W1	-0.048	0.155	-0.177	-0.000	-0.813	0.920
Min Fy	5	17	5:1.25DL	-0.000	-0.130	0.000	-0.000	-0.000	0.767
Max Fz	1	1	2:W1	-0.059	0.025	0.183	-0.000	-0.761	-0.034
Min Fz	26	26	6:1.1DL+1.0W1	0.059	0.054	-0.183	0.000	1.437	0.641
Max Mx	26	26	6:1.1DL+1.0W1	0.059	0.054	-0.183	0.000	1.437	0.641
Min Mx	9	8	6:1.1DL+1.0W1	0.112	-0.047	0.183	-0.000	-0.776	-0.373
Max My	12	26	6:1.1DL+1.0W1	0.207	0.067	0.053	0.000	2.202	0.609
Min My	12	11	6:1.1DL+1.0W1	0.207	0.117	0.053	0.000	-2.208	8.332
Max Mz	12	11	6:1.1DL+1.0W1	0.207	0.117	0.053	0.000	-2.208	8.332
Min Mz	2	2	2:W1	-0.384	-0.009	-0.005	-0.000	-0.335	-3.023



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Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip-in)	My (kip-in)	Mz (kip-in)
Max Fx	10	2:W1	0.000	0.384	-0.009	0.005	-0.000	-0.479	2.615
Min Fx	2	6:1.1DL+1.0W'	0.000	-0.384	0.018	-0.005	-0.000	-0.334	2.286
Max Fy	8	6:1.1DL+1.0W'	0.000	-0.048	0.155	-0.177	-0.000	-0.813	0.920
Min Fy	5	5:1.25DL	0.500	-0.000	-0.130	0.000	-0.000	-0.000	0.767
Max Fz	1	2:W1	0.000	-0.059	0.025	0.183	-0.000	-0.761	-0.034
Min Fz	26	6:1.1DL+1.0W'	0.000	0.059	0.054	-0.183	0.000	1.437	0.641
Max Mx	26	6:1.1DL+1.0W'	0.000	0.059	0.054	-0.183	0.000	1.437	0.641
Min Mx	9	6:1.1DL+1.0W'	0.000	0.112	-0.047	0.183	-0.000	-0.776	-0.373
Max My	12	6:1.1DL+1.0W'	7.000	0.207	0.067	0.053	0.000	2.202	0.609
Min My	12	6:1.1DL+1.0W'	0.000	0.207	0.117	0.053	0.000	-2.208	8.332
Max Mz	12	6:1.1DL+1.0W'	0.000	0.207	0.117	0.053	0.000	-2.208	8.332
Min Mz	2	2:W1	0.000	-0.384	-0.009	-0.005	-0.000	-0.335	-3.023

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	1:DL	1.000	170.003	1.000	3	-170.020	1.000	1
	2:W1	1.000	1.05E+3	1.000	2	-1.11E+3	1.000	4
	3:W2	1.000	1.188	1.000	1	-0.818	1.000	3
	4:0.75W3	1.000	785.253	1.000	2	-831.093	1.000	4
	5:1.25DL	1.000	212.504	1.000	3	-212.525	1.000	1
	6:1.1DL+1.0W'	1.000	861.783	1.000	2	-923.942	1.000	1
	7:1.1DL+1.0W'	1.000	187.659	1.000	3	-187.308	1.000	1
2	1:DL	1.500	2.94E+3	0.000	3	-2.94E+3	0.000	1
	2:W1	1.500	1.84E+3	0.000	1	-2.25E+3	0.000	3
	3:W2	1.500	109.371	1.500	3	-111.413	1.500	1
	4:0.75W3	1.500	1.39E+3	0.000	1	-1.69E+3	0.000	3
	5:1.25DL	1.500	3.68E+3	0.000	3	-3.68E+3	0.000	1
	6:1.1DL+1.0W'	1.500	1.39E+3	0.000	3	-1.8E+3	0.000	1
	7:1.1DL+1.0W'	1.500	3.26E+3	0.000	3	-3.26E+3	0.000	1
3	1:DL	0.500	2.72E+3	0.500	3	-2.72E+3	0.500	1
	2:W1	0.500	1.66E+3	0.000	1	-1.92E+3	0.000	3
	3:W2	0.500	80.577	0.500	3	-77.704	0.500	1
	4:0.75W3	0.500	1.17E+3	0.000	1	-1.37E+3	0.000	3
	5:1.25DL	0.500	3.39E+3	0.500	3	-3.39E+3	0.500	1
	6:1.1DL+1.0W'	0.500	1.24E+3	0.500	4	-1.5E+3	0.500	2
	7:1.1DL+1.0W'	0.500	3.07E+3	0.500	3	-3.07E+3	0.500	1
4	1:DL	7.000	2.94E+3	0.000	3	-2.94E+3	0.000	1
	2:W1	7.000	2.78E+3	0.000	1	-3.06E+3	0.000	3
	3:W2	7.000	3.347	7.000	1	-3.116	7.000	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	4:0.75W3	7.000	2.06E+3	0.000	1	-2.27E+3	0.000	3
	5:1.25DL	7.000	3.68E+3	0.000	3	-3.68E+3	0.000	1
	6:1.1DL+1.0W ¹	7.000	2.83E+3	0.000	3	-3.11E+3	0.000	1
	7:1.1DL+1.0W ²	7.000	3.24E+3	0.000	3	-3.24E+3	0.000	1
5	1:DL	0.500	374.048	0.500	3	-374.134	0.500	1
	2:W1	0.500	1.17E+3	0.000	1	-1.12E+3	0.000	2
	3:W2	0.500	55.247	0.500	2	-48.709	0.500	4
	4:0.75W3	0.500	859.205	0.000	1	-816.780	0.000	2
	5:1.25DL	0.500	467.560	0.500	3	-467.668	0.500	1
	6:1.1DL+1.0W ¹	0.500	1.17E+3	0.000	1	-1.12E+3	0.000	2
	7:1.1DL+1.0W ²	0.500	420.114	0.500	3	-413.670	0.500	1
6	1:DL	0.500	374.048	0.000	3	-374.134	0.000	1
	2:W1	0.500	1E+3	0.500	2	-1.06E+3	0.500	1
	3:W2	0.500	44.181	0.500	1	-53.146	0.500	2
	4:0.75W3	0.500	707.863	0.500	2	-759.597	0.500	1
	5:1.25DL	0.500	467.560	0.000	3	-467.668	0.000	1
	6:1.1DL+1.0W ¹	0.500	1.06E+3	0.000	2	-1.12E+3	0.000	1
	7:1.1DL+1.0W ²	0.500	421.377	0.000	3	-430.436	0.000	1
7	1:DL	0.500	374.048	0.500	3	-374.134	0.500	1
	2:W1	0.500	1.06E+3	0.000	2	-1E+3	0.000	1
	3:W2	0.500	53.146	0.000	1	-44.181	0.000	2
	4:0.75W3	0.500	759.597	0.000	2	-707.863	0.000	1
	5:1.25DL	0.500	467.560	0.500	3	-467.668	0.500	1
	6:1.1DL+1.0W ¹	0.500	1.06E+3	0.000	2	-1E+3	0.000	1
	7:1.1DL+1.0W ²	0.500	412.841	0.500	3	-403.971	0.500	1
8	1:DL	0.500	374.048	0.000	3	-374.134	0.000	1
	2:W1	0.500	1.12E+3	0.500	1	-1.17E+3	0.500	2
	3:W2	0.500	48.709	0.000	2	-55.247	0.000	1
	4:0.75W3	0.500	816.780	0.500	1	-859.205	0.500	2
	5:1.25DL	0.500	467.560	0.000	3	-467.668	0.000	1
	6:1.1DL+1.0W ¹	0.500	1.12E+3	0.500	1	-1.17E+3	0.500	2
	7:1.1DL+1.0W ²	0.500	460.162	0.000	3	-466.794	0.000	1
9	1:DL	1.000	170.003	1.000	3	-170.020	1.000	1
	2:W1	1.000	966.904	1.000	2	-848.588	1.000	1
	3:W2	1.000	1.711	1.000	4	-1.513	1.000	2
	4:0.75W3	1.000	724.042	1.000	2	-635.189	1.000	1
	5:1.25DL	1.000	212.504	1.000	3	-212.525	1.000	1
	6:1.1DL+1.0W ¹	1.000	1.07E+3	1.000	3	-948.958	1.000	1
	7:1.1DL+1.0W ²	1.000	188.673	1.000	3	-188.494	1.000	1
10	1:DL	1.500	2.94E+3	0.000	3	-2.94E+3	0.000	1
	2:W1	1.500	2.13E+3	1.500	4	-1.72E+3	1.500	2
	3:W2	1.500	65.634	1.500	2	-78.248	1.500	4
	4:0.75W3	1.500	1.58E+3	0.000	3	-1.29E+3	0.000	1
	5:1.25DL	1.500	3.68E+3	0.000	3	-3.68E+3	0.000	1



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	6:1.1DL+1.0W ¹	1.500	5.33E+3	0.000	3	-4.92E+3	0.000	1
	7:1.1DL+1.0W ²	1.500	3.28E+3	0.000	3	-3.29E+3	0.000	1
11	1:DL	0.500	2.72E+3	0.500	3	-2.72E+3	0.500	1
	2:W1	0.500	1.95E+3	0.500	4	-1.69E+3	0.500	2
	3:W2	0.500	69.757	0.000	1	-72.631	0.000	3
	4:0.75W3	0.500	1.39E+3	0.500	4	-1.19E+3	0.500	2
	5:1.25DL	0.500	3.39E+3	0.500	3	-3.39E+3	0.500	1
	6:1.1DL+1.0W ¹	0.500	4.94E+3	0.500	4	-4.68E+3	0.500	2
	7:1.1DL+1.0W ²	0.500	2.95E+3	0.500	3	-2.95E+3	0.500	1
12	1:DL	7.000	2.94E+3	0.000	3	-2.94E+3	0.000	1
	2:W1	7.000	3.3E+3	0.000	3	-3.08E+3	0.000	1
	3:W2	7.000	4.650	0.000	1	-4.881	0.000	2
	4:0.75W3	7.000	2.46E+3	0.000	3	-2.3E+3	0.000	1
	5:1.25DL	7.000	3.68E+3	0.000	3	-3.68E+3	0.000	1
	6:1.1DL+1.0W ¹	7.000	6.54E+3	0.000	3	-6.32E+3	0.000	1
	7:1.1DL+1.0W ²	7.000	3.24E+3	0.000	3	-3.24E+3	0.000	1
13	1:DL	3.000	91.236	0.000	2	-204.491	0.000	1
	2:W1	3.000	1.24E+3	3.000	4	-1.15E+3	3.000	2
	3:W2	3.000	243.898	3.000	4	-229.112	3.000	2
	4:0.75W3	3.000	1.12E+3	3.000	4	-1.04E+3	3.000	2
	5:1.25DL	3.000	114.045	0.000	2	-255.613	0.000	1
	6:1.1DL+1.0W ¹	3.000	1.25E+3	3.000	4	-1.3E+3	3.000	2
	7:1.1DL+1.0W ²	3.000	251.605	3.000	4	-383.857	3.000	2
14	1:DL	3.000	91.236	0.000	2	-204.491	0.000	1
	2:W1	3.000	1.28E+3	3.000	4	-1.2E+3	3.000	2
	3:W2	3.000	243.403	3.000	4	-232.823	3.000	2
	4:0.75W3	3.000	1.14E+3	3.000	4	-1.07E+3	3.000	2
	5:1.25DL	3.000	114.045	0.000	2	-255.613	0.000	1
	6:1.1DL+1.0W ¹	3.000	1.28E+3	3.000	4	-1.35E+3	3.000	2
	7:1.1DL+1.0W ²	3.000	251.065	3.000	4	-387.523	3.000	2
15	1:DL	3.000	91.236	3.000	1	-204.491	3.000	2
	2:W1	3.000	1.2E+3	0.000	1	-1.28E+3	0.000	2
	3:W2	3.000	232.823	0.000	1	-243.403	0.000	3
	4:0.75W3	3.000	1.07E+3	0.000	1	-1.14E+3	0.000	3
	5:1.25DL	3.000	114.045	3.000	1	-255.613	3.000	2
	6:1.1DL+1.0W ¹	3.000	1.04E+3	0.000	1	-1.27E+3	0.000	2
	7:1.1DL+1.0W ²	3.000	78.122	0.000	1	-235.741	0.000	3
16	1:DL	3.000	91.236	3.000	1	-204.491	3.000	2
	2:W1	3.000	1.15E+3	0.000	1	-1.24E+3	0.000	2
	3:W2	3.000	229.112	0.000	1	-243.898	0.000	3
	4:0.75W3	3.000	1.04E+3	0.000	1	-1.12E+3	0.000	3
	5:1.25DL	3.000	114.045	3.000	1	-255.613	3.000	2
	6:1.1DL+1.0W ¹	3.000	991.348	0.000	1	-1.23E+3	0.000	2
	7:1.1DL+1.0W ²	3.000	74.368	0.000	1	-236.192	0.000	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
17	1:DL	1.000	231.528	0.000	3	-220.928	0.000	1
	2:W1	1.000	1.03E+3	0.000	2	-1.02E+3	0.000	1
	3:W2	1.000	84.886	1.000	2	-83.464	1.000	4
	4:0.75W3	1.000	808.677	0.000	2	-803.500	0.000	1
	5:1.25DL	1.000	289.410	0.000	3	-276.160	0.000	1
	6:1.1DL+1.0W1	1.000	1.28E+3	0.000	3	-1.27E+3	0.000	1
	7:1.1DL+1.0W2	1.000	324.903	0.000	3	-311.821	0.000	1
18	1:DL	1.000	231.528	0.000	3	-220.928	0.000	1
	2:W1	1.000	1.02E+3	1.000	2	-1.03E+3	1.000	4
	3:W2	1.000	83.464	0.000	3	-84.886	0.000	1
	4:0.75W3	1.000	803.500	1.000	2	-808.677	1.000	4
	5:1.25DL	1.000	289.410	0.000	3	-276.160	0.000	1
	6:1.1DL+1.0W1	1.000	1.15E+3	0.000	3	-1.14E+3	0.000	1
	7:1.1DL+1.0W2	1.000	337.749	0.000	3	-327.509	0.000	1
19	1:DL	7.000	2.94E+3	7.000	3	-2.94E+3	7.000	1
	2:W1	7.000	3.08E+3	7.000	1	-3.3E+3	7.000	3
	3:W2	7.000	4.881	7.000	1	-4.650	7.000	3
	4:0.75W3	7.000	2.3E+3	7.000	1	-2.46E+3	7.000	3
	5:1.25DL	7.000	3.68E+3	7.000	3	-3.68E+3	7.000	1
	6:1.1DL+1.0W1	7.000	2.63E+3	7.000	4	-2.85E+3	7.000	2
	7:1.1DL+1.0W2	7.000	3.24E+3	7.000	3	-3.24E+3	7.000	1
20	1:DL	7.000	2.94E+3	7.000	3	-2.94E+3	7.000	1
	2:W1	7.000	3.06E+3	7.000	4	-2.78E+3	7.000	2
	3:W2	7.000	3.116	0.000	1	-3.347	0.000	2
	4:0.75W3	7.000	2.27E+3	7.000	4	-2.06E+3	7.000	2
	5:1.25DL	7.000	3.68E+3	7.000	3	-3.68E+3	7.000	1
	6:1.1DL+1.0W1	7.000	6.29E+3	7.000	4	-6.02E+3	7.000	2
	7:1.1DL+1.0W2	7.000	3.24E+3	7.000	3	-3.24E+3	7.000	1
21	1:DL	0.500	2.72E+3	0.000	3	-2.72E+3	0.000	1
	2:W1	0.500	1.69E+3	0.000	1	-1.95E+3	0.000	3
	3:W2	0.500	72.631	0.500	3	-69.757	0.500	1
	4:0.75W3	0.500	1.19E+3	0.000	1	-1.39E+3	0.000	3
	5:1.25DL	0.500	3.39E+3	0.000	3	-3.39E+3	0.000	1
	6:1.1DL+1.0W1	0.500	1.21E+3	0.500	4	-1.47E+3	0.500	2
	7:1.1DL+1.0W2	0.500	3.05E+3	0.500	3	-3.05E+3	0.500	1
22	1:DL	1.500	2.94E+3	1.500	3	-2.94E+3	1.500	1
	2:W1	1.500	1.72E+3	0.000	1	-2.13E+3	0.000	3
	3:W2	1.500	78.248	0.000	2	-65.634	0.000	1
	4:0.75W3	1.500	1.29E+3	1.500	1	-1.58E+3	1.500	3
	5:1.25DL	1.500	3.68E+3	1.500	3	-3.68E+3	1.500	1
	6:1.1DL+1.0W1	1.500	1.73E+3	1.500	4	-2.14E+3	1.500	2
	7:1.1DL+1.0W2	1.500	3.29E+3	1.500	4	-3.28E+3	1.500	2
23	1:DL	0.500	2.72E+3	0.000	3	-2.72E+3	0.000	1
	2:W1	0.500	1.92E+3	0.500	4	-1.66E+3	0.500	2



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Rev
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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	3:W2	0.500	77.704	0.000	1	-80.577	0.000	3
	4:0.75W3	0.500	1.37E+3	0.500	4	-1.17E+3	0.500	2
	5:1.25DL	0.500	3.39E+3	0.000	3	-3.39E+3	0.000	1
	6:1.1DL+1.0W ₁	0.500	4.9E+3	0.500	4	-4.64E+3	0.500	2
	7:1.1DL+1.0W ₂	0.500	2.93E+3	0.500	3	-2.94E+3	0.500	1
24	1:DL	1.500	2.94E+3	1.500	3	-2.94E+3	1.500	1
	2:W1	1.500	2.25E+3	1.500	4	-1.84E+3	1.500	2
	3:W2	1.500	111.413	0.000	1	-109.371	0.000	3
	4:0.75W3	1.500	1.69E+3	1.500	4	-1.39E+3	1.500	2
	5:1.25DL	1.500	3.68E+3	1.500	3	-3.68E+3	1.500	1
	6:1.1DL+1.0W ₁	1.500	5.49E+3	1.500	4	-5.08E+3	1.500	2
	7:1.1DL+1.0W ₂	1.500	3.26E+3	1.500	4	-3.26E+3	1.500	2
25	1:DL	1.000	170.003	0.000	3	-170.020	0.000	1
	2:W1	1.000	848.588	0.000	2	-966.904	0.000	1
	3:W2	1.000	1.513	0.000	1	-1.711	0.000	2
	4:0.75W3	1.000	635.189	0.000	2	-724.042	0.000	1
	5:1.25DL	1.000	212.504	0.000	3	-212.525	0.000	1
	6:1.1DL+1.0W ₁	1.000	1.04E+3	0.000	2	-1.15E+3	0.000	1
	7:1.1DL+1.0W ₂	1.000	187.985	0.000	3	-188.201	0.000	1
26	1:DL	1.000	170.003	0.000	3	-170.020	0.000	1
	2:W1	1.000	1.11E+3	0.000	2	-1.05E+3	0.000	1
	3:W2	1.000	0.818	0.000	1	-1.188	0.000	2
	4:0.75W3	1.000	831.093	0.000	2	-785.253	0.000	1
	5:1.25DL	1.000	212.504	0.000	3	-212.525	0.000	1
	6:1.1DL+1.0W ₁	1.000	1.3E+3	0.000	2	-1.24E+3	0.000	1
	7:1.1DL+1.0W ₂	1.000	187.780	0.000	3	-188.169	0.000	1

Plate Center Principal Stress Summary

	Plate	L/C	Principal		Von Mis		Tresca	
			Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)
Max (t)	27	2:W1	1.09E+3	1.24E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3
Max (b)	29	6:1.1DL+1.0W ₁	1.08E+3	1.25E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3
Max VM (t)	29	6:1.1DL+1.0W ₁	1.08E+3	1.25E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3
Max VM (b)	29	6:1.1DL+1.0W ₁	1.08E+3	1.25E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3
Tresca (t)	29	6:1.1DL+1.0W ₁	1.08E+3	1.25E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3
Tresca (b)	29	6:1.1DL+1.0W ₁	1.08E+3	1.25E+3	1.88E+3	2.15E+3	2.17E+3	2.49E+3



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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	14	5:1.25DL	0.000	0.158	0.013	-0.151	0.000	0.000
Min FX	18	6:1.1DL+1.0W'	-0.028	0.213	0.042	-0.873	-0.000	-1.022
Max FY	15	6:1.1DL+1.0W'	-0.027	0.230	0.040	-0.853	-0.000	-0.973
Min FY	13	2:W1	-0.027	-0.091	0.051	-0.986	0.000	-0.973
Max FZ	14	6:1.1DL+1.0W'	-0.028	0.065	0.064	-1.139	0.000	-1.022
Min FZ	15	5:1.25DL	0.000	0.158	-0.013	0.151	-0.000	0.000
Max MX	15	5:1.25DL	0.000	0.158	-0.013	0.151	-0.000	0.000
Min MX	14	6:1.1DL+1.0W'	-0.028	0.065	0.064	-1.139	0.000	-1.022
Max MY	13	2:W1	-0.027	-0.091	0.051	-0.986	0.000	-0.973
Min MY	15	6:1.1DL+1.0W'	-0.027	0.230	0.040	-0.853	-0.000	-0.973
Max MZ	14	5:1.25DL	0.000	0.158	0.013	-0.151	0.000	0.000
Min MZ	18	6:1.1DL+1.0W'	-0.028	0.213	0.042	-0.873	-0.000	-1.022



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Rev
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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 1 Check 1

```

*****
MEMBER 1 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 10.52
KL/R-Z= 10.52
UNL = 12.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.1 0.0 0.2 0.1 0.0
LOCATION 0.0 1.0 0.0 1.0 1.0
LOADING 6 5 2 2 5
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.028 2
0.06 T 0.12 -0.03 1.00
*****
1 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 2 Check 1

```

*****
MEMBER 2 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

PARAMETER	0.5 (KIP-FEET)						
IN KIP	INCH	L5	L5	L5	L5	L5	L5
KL/R-Y=	15.78						
KL/R-Z=	15.78						
UNL =	18.00						
CB =	1.00						
PHIC =	0.00						
PHIB =	0.90						
FYLD =	36.00						
NSF =	1.00						
DFE =	0.00	0.5					
dff =	0.00						

```

*****
CAPACITIES
IN KIP INCH
-----
PNC=0.5708E+2
pnc=0.0000E+0
PNT=0.6124E+2
pnt=0.0000E+0
MNZ=0.6383E+2
mnz=0.6033E+1
MNY=0.6383E+2
mny=0.6638E-3
VN =0.2030E+2
vn =0.2995E-1

```

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)

	AXIAL	SHEAR-Y	SHEAR-Z	MOMENT-Y	MOMENT-Z
VALUE	-0.4	0.0	0.0	0.0	0.5
LOCATION	0.0	0.0	0.0	1.5	0.0
LOADING	6	5	3	6	5

```

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.095 5
0.00 C 0.00 0.50 0.00
*****

```

2 ST HSST3X3X0.188 (AISC SECTIONS)



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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 3 Check 1

```

*****
MEMBER 3 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.0 0.0 0.0 0.5
LOCATION 0.0 0.5 0.0 0.0 0.5
LOADING 6 6 2 6 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS BEND Z 0.087 5
0.00 T -0.00 0.46 0.50
*****
3 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 4 Check 1

```

*****
MEMBER 4 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****

```

PARAMETER	0.5 (KIP-FEET)				
IN KIP INCH	L5	L5	L5	L5	L5
KL/R-Y=	73.63				
KL/R-Z=	73.63				
UNL =	84.00				
CB =	1.00				
PHIC =	0.00				
PHIB =	0.90				
FYLD =	36.00				
NSF =	1.00				
DFE =	0.00				
dfe =	0.00				

```

*****
CAPACITIES
IN KIP INCH
-----
PNC=0.4348E+2
pnc=0.0000E+0
PNT=0.6124E+2
pnt=0.0000E+0
MNZ=0.6383E+2
mnz=0.6033E+1
MNY=0.6383E+2
mny=0.2871E-3
VN =0.2030E+2
vn =0.9580E-1

```

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)

	AXIAL	SHEAR-Y	SHEAR-Z	MOMENT-Y	MOMENT-Z
VALUE	-0.3	0.1	0.1	0.2	0.5
LOCATION	0.0	0.0	0.0	7.0	0.0
LOADING	2	5	2	2	5

```

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS BEND Z 0.095 5
0.00 C 0.00 0.50 0.00
*****

```

4 ST HSST3X3X0.188 (AISC SECTIONS)



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148872000

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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 5 Check 1

```

*****
MEMBER 5 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.1 0.2 0.2 0.1
LOCATION 0.0 0.5 0.0 0.0 0.5
LOADING 2 5 6 6 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.030 2
0.05 C -0.16 0.00 0.00
*****
5 ST HSST3X3X0.188 (AISC SECTIONS)

```



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148872000

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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 6 Check 1

```

*****
MEMBER 6 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH | L6
*****
KL/R-Y= 5.26 |
KL/R-Z= 5.26 +
UNL = 6.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.1 0.1 0.1 0.1 0.1
LOCATION 0.0 0.0 0.0 0.5 0.0
LOADING 6 6 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.028 6
0.06 T 0.08 0.07 0.00
*****
6 ST HSST3X3X0.188 (AISC SECTIONS)

```



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148872000

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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 7 Check 1

```

*****
MEMBER 7 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.1 0.1 0.1
LOCATION 0.0 0.5 0.0 0.0 0.5
LOADING 2 5 6 6 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.027 2
0.06 C 0.14 0.00 0.00
*****
7 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
18

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 8 Check 1

```

*****
MEMBER 8 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER 0.1 (KIP-FEET)
IN KIP INCH L6
CAPACITIES
IN KIP INCH
L6 L6
KL/R-Y= 5.26 +
KL/R-Z= 5.26 +
UNL = 6.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.0 0.2 0.2 0.2 0.1
LOCATION 0.0 0.0 0.0 0.5 0.0
LOADING 6 6 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.030 2
0.05 T -0.16 0.00 0.50
*****
8 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

Sheet No
19

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 9 Check 1

```

*****
MEMBER 9 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH |L6
*****
+ L2 L5
KL/R-Y= 10.52 |
KL/R-Z= 10.52 +
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.2 0.1 0.0
LOCATION 0.0 1.0 0.0 1.0 0.0
LOADING 2 6 6 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.027 6
0.11 C 0.12 0.02 1.00
*****
9 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
20

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 10 Check 1

```

*****
MEMBER 10 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FEET)
IN KIP INCH L6
*****
KL/R-Y= 15.78
KL/R-Z= 15.78
UNL = 18.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.4 0.0 0.0 0.0 0.7
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 5 4 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.135 6
0.38 C -0.04 0.66 0.00
*****
10 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
21

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 11 Check 1

```

*****
MEMBER 11 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.6 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.2 0.0 0.0 0.0 0.6
LOCATION 0.0 0.5 0.0 0.5 0.5
LOADING 2 6 2 2 6
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.126 6
0.25 C -0.01 0.65 0.50
*****
11 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
22

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 12 Check 1

```

*****
MEMBER 12 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FEET)
IN KIP INCH L6
*****
KL/R-Y= 73.63
KL/R-Z= 73.63
UNL = 84.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.2 0.1 0.1 0.2 0.7
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 6 6 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.168 6
0.21 C -0.18 0.69 0.00
*****
12 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

Sheet No
24

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 14 Check 1

```

*****
MEMBER 14 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 3.00 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER          0.1 (KIP-FEET)
IN KIP INCH        |
+-----+-----+-----+-----+-----+-----+
KL/R-Y= 31.55      |
KL/R-Z= 31.55      |
UNL = 36.00        |
CB = 1.00          |
PHIC = 0.00        |
PHIB = 0.90        |
FYLD = 36.00       |
NSF = 1.00         |
DFE = 0.00         |
dff = 0.00         |
+-----+-----+-----+-----+-----+
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
          AXIAL      SHEAR-Y      SHEAR-Z      MOMENT-Y      MOMENT-Z
VALUE      -0.2        0.0          0.1          0.1          0.1
LOCATION     3.0        0.0          0.0          0.0          3.0
LOADING     5         2           6           6           2

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/    CRITICAL COND/    RATIO/    LOADING/
FX          MY              MZ        LOCATION
=====
PASS      HSS FLEX+AXL    0.034     6
0.07 T    -0.09          0.09     3.00
*****
14 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 15 Check 1

```

*****
MEMBER 15 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 3.00 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER 0.1 (KIP-FEET)
IN KIP INCH L6
CAPACITIES
IN KIP INCH
KL/R-Y= 31.55 +
KL/R-Z= 31.55 +
UNL = 36.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.0 0.1 0.1 0.1
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 6 6 2 2 6

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.032 2
0.07 T -0.08 -0.09 0.00
*****
15 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

Sheet No
27

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 17 Check 1

```

*****
MEMBER 17 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH L6
*****
KL/R-Y= 10.52
KL/R-Z= 10.52
UNL = 12.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.1 0.1 0.1 0.1
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 6 6 2 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.033 6
0.02 C 0.08 0.09 0.00
*****
17 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 18 Check 1

```

*****
MEMBER 18 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
0.1 (KIP-FEET)
PARAMETER | L6
IN KIP INCH |
-----+-----
KL/R-Y= 10.52 | L6
KL/R-Z= 10.52 | L6
UNL = 12.00 | L6
CB = 1.00 + L2
PHIC = 0.00 | L6 L2
PHIB = 0.90 + L2
FYLD = 36.00 | L5 L5 L5
NSF = 1.00 +-----+-----+-----+-----+-----+-----+
DFE = 0.00 0.0
dff = 0.00
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.1 0.1 0.1 0.1
LOCATION 0.0 0.0 0.0 1.0 0.0
LOADING 5 6 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.029 6
0.01 C -0.07 0.09 0.00
*****
18 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
29

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 19 Check 1

```

*****
MEMBER 19 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 73.63
KL/R-Z= 73.63
UNL = 84.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.1 0.1 0.2 0.5
LOCATION 0.0 7.0 0.0 7.0 7.0
LOADING 2 5 2 2 5
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS BEND Z 0.095 5
0.00 C 0.00 0.50 7.00
*****
19 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
30

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 20 Check 1

```

*****
MEMBER 20 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FEET)
IN KIP INCH
KL/R-Y= 73.63
KL/R-Z= 73.63
UNL = 84.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.3 0.1 0.1 0.2 0.7
LOCATION 0.0 7.0 0.0 0.0 7.0
LOADING 2 6 6 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.161 6
0.26 C -0.18 0.66 7.00
*****
20 ST HSST3X3X0.188 (AISC SECTIONS)

```



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
31

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 21 Check 1

```

*****
MEMBER 21 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FEET)
IN KIP INCH L5
*****
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.0 0.0 0.0 0.5
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 6 2 2 6 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS BEND Z 0.087 5
0.00 T -0.00 0.46 0.00
*****
21 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
32

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 22 Check 1

```

*****
MEMBER 22 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 15.78
KL/R-Z= 15.78
UNL = 18.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.4 0.0 0.0 0.0 0.5
LOCATION 0.0 1.5 0.0 1.5 1.5
LOADING 6 6 4 2 5
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.095 5
0.00 C 0.00 0.50 1.50
*****
22 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
33

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 23 Check 1

```

*****
MEMBER 23 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.6 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.2 0.0 0.0 0.0 0.6
LOCATION 0.0 0.0 0.0 0.5 0.5
LOADING 2 2 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.125 6
0.25 C -0.01 0.64 0.50
*****
23 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 24 Check 1

```

*****
MEMBER 24 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FEET)
IN KIP INCH
KL/R-Y= 15.78
KL/R-Z= 15.78
UNL = 18.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.4 0.0 0.0 0.0 0.7
LOCATION 0.0 1.5 0.0 0.0 1.5
LOADING 2 6 7 2 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.139 6
0.38 C -0.03 0.69 1.50
*****
24 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

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Rev
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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 25 Check 1

```

*****
MEMBER 25 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH |L6
*****
KL/R-Y= 10.52 |
KL/R-Z= 10.52 +
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.1 0.0 0.2 0.1 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 6 5 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.029 6
0.11 T 0.12 0.03 0.00
*****
25 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Steel Design (Track 2) Beam 26 Check 1

```

*****
MEMBER 26 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH | L6
*****
KL/R-Y= 10.52 |
KL/R-Z= 10.52 |
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.2 0.1 0.1
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 6 6 6 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.033 6
0.06 C 0.12 0.05 0.00
*****
26 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.028	1.000	0.028	HSS FLEX+A	2	1.890	2.460	2.460	4.030
2	HSST3X3X0	HSST3X3X0	0.095	1.000	0.095	HSS FLEX+A	5	1.890	2.460	2.460	4.030
3	HSST3X3X0	HSST3X3X0	0.087	1.000	0.087	HSS BEND Z	5	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.095	1.000	0.095	HSS BEND Z	5	1.890	2.460	2.460	4.030
5	HSST3X3X0	HSST3X3X0	0.030	1.000	0.030	HSS FLEX+A	2	1.890	2.460	2.460	4.030
6	HSST3X3X0	HSST3X3X0	0.028	1.000	0.028	HSS FLEX+A	6	1.890	2.460	2.460	4.030
7	HSST3X3X0	HSST3X3X0	0.027	1.000	0.027	HSS FLEX+A	2	1.890	2.460	2.460	4.030
8	HSST3X3X0	HSST3X3X0	0.030	1.000	0.030	HSS FLEX+A	2	1.890	2.460	2.460	4.030
9	HSST3X3X0	HSST3X3X0	0.027	1.000	0.027	HSS FLEX+A	6	1.890	2.460	2.460	4.030
10	HSST3X3X0	HSST3X3X0	0.135	1.000	0.135	HSS FLEX+A	6	1.890	2.460	2.460	4.030
11	HSST3X3X0	HSST3X3X0	0.126	1.000	0.126	HSS FLEX+A	6	1.890	2.460	2.460	4.030
12	HSST3X3X0	HSST3X3X0	0.168	1.000	0.168	HSS FLEX+A	6	1.890	2.460	2.460	4.030
13	HSST3X3X0	HSST3X3X0	0.033	1.000	0.033	HSS FLEX+A	6	1.890	2.460	2.460	4.030
14	HSST3X3X0	HSST3X3X0	0.034	1.000	0.034	HSS FLEX+A	6	1.890	2.460	2.460	4.030
15	HSST3X3X0	HSST3X3X0	0.032	1.000	0.032	HSS FLEX+A	2	1.890	2.460	2.460	4.030
16	HSST3X3X0	HSST3X3X0	0.031	1.000	0.031	HSS FLEX+A	2	1.890	2.460	2.460	4.030
17	HSST3X3X0	HSST3X3X0	0.033	1.000	0.033	HSS FLEX+A	6	1.890	2.460	2.460	4.030
18	HSST3X3X0	HSST3X3X0	0.029	1.000	0.029	HSS FLEX+A	6	1.890	2.460	2.460	4.030
19	HSST3X3X0	HSST3X3X0	0.095	1.000	0.095	HSS BEND Z	5	1.890	2.460	2.460	4.030
20	HSST3X3X0	HSST3X3X0	0.161	1.000	0.161	HSS FLEX+A	6	1.890	2.460	2.460	4.030
21	HSST3X3X0	HSST3X3X0	0.087	1.000	0.087	HSS BEND Z	5	1.890	2.460	2.460	4.030
22	HSST3X3X0	HSST3X3X0	0.095	1.000	0.095	HSS FLEX+A	5	1.890	2.460	2.460	4.030
23	HSST3X3X0	HSST3X3X0	0.125	1.000	0.125	HSS FLEX+A	6	1.890	2.460	2.460	4.030
24	HSST3X3X0	HSST3X3X0	0.139	1.000	0.139	HSS FLEX+A	6	1.890	2.460	2.460	4.030
25	HSST3X3X0	HSST3X3X0	0.029	1.000	0.029	HSS FLEX+A	6	1.890	2.460	2.460	4.030
26	HSST3X3X0	HSST3X3X0	0.033	1.000	0.033	HSS FLEX+A	6	1.890	2.460	2.460	4.030

Failed Members

There is no data of this type.



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Sheet No
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Rev
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Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Statics Check Results

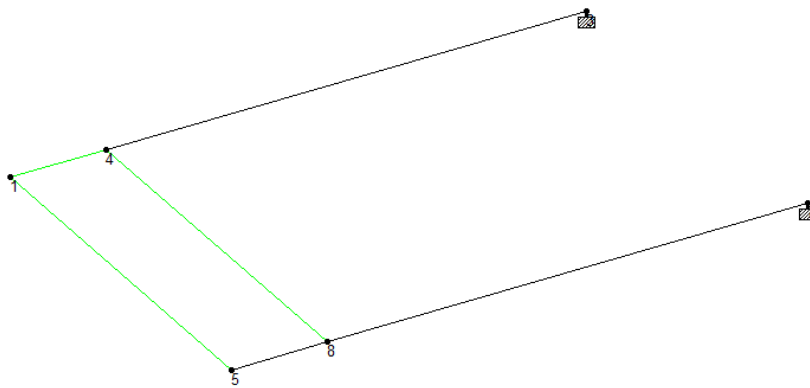
L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
1:DL	Loads	0.000	-0.505	0.000	-6.063	0.000	-60.633
1:DL	Reactions	-0.000	0.505	0.000	6.063	-0.000	60.633
	Difference	-0.000	0.000	0.000	0.000	-0.000	0.000
2:W1	Loads	0.111	0.000	-0.209	-1.555	23.726	-0.816
2:W1	Reactions	-0.111	0.000	0.209	1.555	-23.726	0.816
	Difference	-0.000	0.000	0.000	0.000	-0.000	-0.000
3:W2	Loads	0.028	0.000	-0.029	-0.208	3.184	-0.191
3:W2	Reactions	-0.028	-0.000	0.029	0.208	-3.184	0.191
	Difference	-0.000	-0.000	0.000	-0.000	-0.000	0.000
4:0.75W3	Loads	0.105	0.000	-0.178	-1.308	20.098	-0.481
4:0.75W3	Reactions	-0.105	0.000	0.178	1.308	-20.098	0.481
	Difference	-0.000	0.000	0.000	0.000	-0.000	-0.000



Abutment-Sides

The following structure spacing was accommodated from analyzing the THEA contract plans reinforcement for the abutment. The spacing is dependent on the abutment, refer to Table 1 for recommended distances.

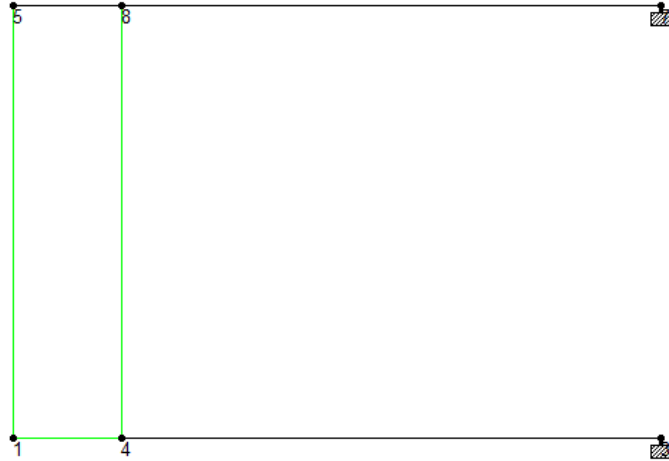
3D View-Length:



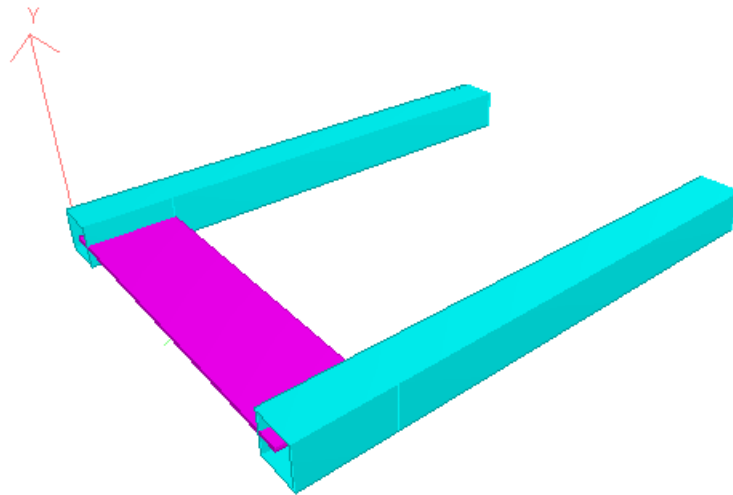
Side View:



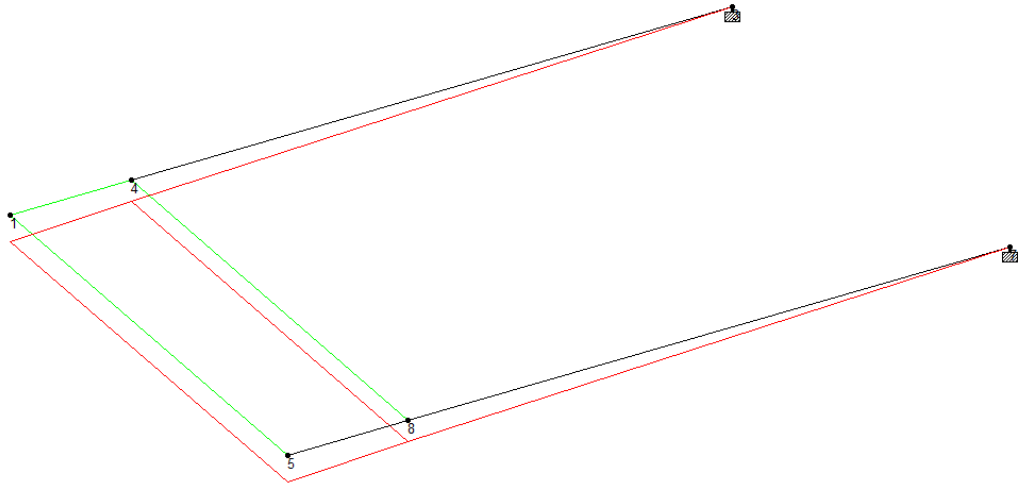
Plan View:



3D View:



Deflection View:





STAAD Analysis



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Job No 148872000	Sheet No 1	Rev 3
Part		
Ref		
By IERM	Date 19-Jun-18	Chd
Client THEA	File THEA3 Redesign- Abutm	Date/Time 06-Feb-2020 10:42

Job Title Abutment-Sides

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	19-Jun-18		

Project ID	
Project Name	

Structure Type	SPACE FRAME
----------------	-------------

Number of Nodes	6	Highest Node	8
Number of Elements	4	Highest Beam	9
Number of Plates	1	Highest Plate	7

Number of Basic Load Cases	5
Number of Combination Load Cases	8

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	DYNO DRUM HO: LIGHT WIND LOAD (X)
Primary	3	DYNO DRUM HO: LIGHT WIND LOAD (Z)
Primary	7	WIND LOAD ON STRUCTURE (Z) DIREC
Primary	8	WIND RESULTANT
Combination	4	1.25DL
Combination	5	1.1DL+1.0WX
Combination	6	CASE I: VX
Combination	9	1.1DL+WZ
Combination	10	CASE I: VY
Combination	11	CASE III: VY
Combination	12	CASE III: VZ
Combination	13	CASE III: VX

Nodes

Node	X (ft)	Y (ft)	Z (ft)
1	0	0	0
3	3.000	0	0
4	0.500	0	0
5	0	0	2.000
7	3.000	0	2.000
8	0.500	0	2.000



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
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Rev
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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	4	0.500	2	0
4	5	8	0.500	2	0
8	4	3	2.500	2	0
9	8	7	2.500	2	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
7	5	1	4	8	1

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
2	HSST3X3X0.188	1.890	2.460	2.460	3.927	STEEL_36_KS

Plate Thickness

Prop	Node A (in)	Node B (in)	Node C (in)	Node D (in)	Material
1	0.250	0.250	0.250	0.250	-

Materials

Mat	Name	E (kip/in ²)	ν	Density (kip/in ³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E -6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E -6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E -6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E -6
5	A500-GR.B	29E+3	0.300	0.000	6E -6
6	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E -6
7	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E -6
8	STEEL	29E+3	0.300	0.000283	6E -6
9	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E -6



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CONNECTED User: Ivonne Rios

Job No 148872000	Sheet No 3	Rev 3
Part		
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By IERM	Date 19-Jun-18	Chd
Client THEA	File THEA3 Redesign- Abutm	Date/Time 06-Feb-2020 10:42

Job Title	Abutment-Sides
-----------	----------------

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
3	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
7	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed

Releases

There is no data of this type.

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	DYNO DRUM HO: LIGHT WIND LOAD (X)	Wind
3	DYNO DRUM HO: LIGHT WIND LOAD (Z)	Wind
7	WIND LOAD ON STRUCTURE (Z) DIREC	Wind
8	WIND RESULTANT	Wind

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	1.25DL	1	DL	1.25
5	1.1DL+1.0WX	1	DL	1.10
		2	DYNO DRUM HO: LIGHT WIND LOAD (X)	1.00
6	CASE I: VX	2	DYNO DRUM HO: LIGHT WIND LOAD (X)	1.00
9	1.1DL+WZ	1	DL	1.10
		3	DYNO DRUM HO: LIGHT WIND LOAD (Z)	1.00
		7	WIND LOAD ON STRUCTURE (Z) DIREC	1.00
10	CASE I: VY	1	DL	1.00
11	CASE III: VY	1	DL	0.75
12	CASE III: VZ	3	DYNO DRUM HO: LIGHT WIND LOAD (Z)	0.75
13	CASE III: VX	2	DYNO DRUM HO: LIGHT WIND LOAD (X)	0.75

Load Generators

There is no data of this type.

1 DL : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	-	-0.0261	-	-	-	-
5	-	-0.0261	-	-	-	-



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
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Rev
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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

1 DL : Selfweight

Direction	Factor	Assigned Geometry
Y	-1.000	ALL

2 DYNO DRUM HO: LIGHT WIND LOAD (X) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	0.0522	-	-	-	-	-
5	0.0522	-	-	-	-	-

3 DYNO DRUM HO: LIGHT WIND LOAD (Z) DIRECTION : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	-	-	0.02777	-	-	-
5	-	-	0.02777	-	-	-

7 WIND LOAD ON STRUCTURE (Z) DIRECTION : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI lbf/ft	GZ	20.000	0	-	0.500	-
4	UNI lbf/ft	GZ	20.000	0	-	0.500	-
8	UNI lbf/ft	GZ	20.000	0	-	2.500	-
9	UNI lbf/ft	GZ	20.000	0	-	2.500	-

8 WIND RESULTANT : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	0.022	-	-	-	-	-
3	-	0.053	-	-	-	-
4	0.022	-	-	-	-	-



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
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Rev
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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	5	9:1.1DL+WZ	0.000	-0.009	0.003	0.010	0.000	0.000	0.000
Min X	1	9:1.1DL+WZ	-0.000	-0.009	0.003	0.010	-0.000	0.000	0.000
Max Y	3	1:DL	0	0	0	0	0	0	0
Min Y	1	4:1.25DL	0	-0.010	0	0.010	-0.000	0	0.000
Max Z	1	9:1.1DL+WZ	-0.000	-0.009	0.003	0.010	-0.000	0.000	0.000
Min Z	1	2:DYNO DRUM	0.000	0	-0.000	0.000	0	-0.000	0
Max rX	5	4:1.25DL	0	-0.010	0	0.010	0.000	0	0.000
Min rX	1	4:1.25DL	0	-0.010	0	0.010	-0.000	0	0.000
Max rY	4	9:1.1DL+WZ	-0.000	-0.007	0.003	0.007	0.000	0.000	0.000
Min rY	1	2:DYNO DRUM	0.000	0	-0.000	0.000	0	-0.000	0
Max rZ	1	4:1.25DL	0	-0.010	0	0.010	-0.000	0	0.000
Min rZ	3	1:DL	0	0	0	0	0	0	0
Max Rst	1	4:1.25DL	0	-0.010	0	0.010	-0.000	0	0.000

Beam Displacement Detail Summary

Displacements shown in italic indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	4	9:1.1DL+WZ	0	0.000	-0.009	0.003	0.010
Min X	1	9:1.1DL+WZ	0	-0.000	-0.009	0.003	0.010
Max Y	8	1:DL	2.500	0	0	0	0
Min Y	1	4:1.25DL	0	0	-0.010	0	0.010
Max Z	1	9:1.1DL+WZ	0	-0.000	-0.009	0.003	0.010
Min Z	1	1:DL	0	0	-0.008	0	0.008
Max Rst	1	4:1.25DL	0	0	-0.010	0	0.010

Beam End Displacement Summary

Displacements shown in italic indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	4	5	9:1.1DL+WZ	0.000	-0.009	0.003	0.010
Min X	1	1	9:1.1DL+WZ	-0.000	-0.009	0.003	0.010
Max Y	8	3	1:DL	0	0	0	0
Min Y	1	1	4:1.25DL	0	-0.010	0	0.010
Max Z	1	1	9:1.1DL+WZ	-0.000	-0.009	0.003	0.010
Min Z	1	1	1:DL	0	-0.008	0	0.008
Max Rst	1	1	4:1.25DL	0	-0.010	0	0.010



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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	9	8	9:1.1DL+WZ	0.077	-0.038	0.03777	-0.000	-0.729	0.200
Min Fx	8	4	9:1.1DL+WZ	-0.077	-0.038	0.03777	0.000	-0.729	0.200
Max Fy	1	1	2:DYNO DRUM	0.048	0	0.000	0	-0.015	0
Min Fy	8	3	4:1.25DL	-0	-0.063	-0	0.000	-0	1.818
Max Fz	8	3	9:1.1DL+WZ	-0.077	-0.055	0.08777	0.000	1.154	1.600
Min Fz	1	1	9:1.1DL+WZ	-0.038	-0.031	-0.127	-0.003	0.062	0.001
Max Mx	4	5	4:1.25DL	0	-0.035	0	0.003	0	0.001
Min Mx	1	1	4:1.25DL	0	-0.035	0	-0.003	0	0.001
Max My	8	3	9:1.1DL+WZ	-0.077	-0.055	0.08777	0.000	1.154	1.600
Min My	8	4	9:1.1DL+WZ	-0.077	-0.038	0.03777	0.000	-0.729	0.200
Max Mz	8	3	4:1.25DL	-0	-0.063	-0	0.000	-0	1.818
Min Mz	1	1	2:DYNO DRUM	0.048	0	0.000	0	-0.015	0

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	9	9:1.1DL+WZ	0	0.077	-0.038	0.03777	-0.000	-0.729	0.200
Min Fx	8	9:1.1DL+WZ	0	-0.077	-0.038	0.03777	0.000	-0.729	0.200
Max Fy	1	2:DYNO DRUM	0	0.048	0	0.000	0	-0.015	0
Min Fy	8	4:1.25DL	2.500	-0	-0.063	-0	0.000	-0	1.818
Max Fz	8	9:1.1DL+WZ	2.500	-0.077	-0.055	0.08777	0.000	1.154	1.600
Min Fz	1	9:1.1DL+WZ	0	-0.038	-0.031	-0.127	-0.003	0.062	0.001
Max Mx	4	4:1.25DL	0	0	-0.035	0	0.003	0	0.001
Min Mx	1	4:1.25DL	0	0	-0.035	0	-0.003	0	0.001
Max My	8	9:1.1DL+WZ	2.500	-0.077	-0.055	0.08777	0.000	1.154	1.600
Min My	8	9:1.1DL+WZ	0	-0.077	-0.038	0.03777	0.000	-0.729	0.200
Max Mz	8	4:1.25DL	2.500	-0	-0.063	-0	0.000	-0	1.818
Min Mz	1	2:DYNO DRUM	0	0.048	0	0.000	0	-0.015	0



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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	1:DL	0.500	109.198	0.500	3	-109.198	0.500	1
	2:DYNO DRUM	0.500	34.821	0	1			
	3:DYNO DRUM	0.500	196.041	0.500	1	-218.346	0.500	2
	7:WIND LOAD	0.500	190.456	0.500	1	-208.472	0.500	2
	8:WIND RESU	0.500	118.768	0.500	1	-119.339	0.500	2
	4:1.25DL	0.500	136.498	0.500	3	-136.498	0.500	1
	5:1.1DL+1.0W)	0.500	154.325	0.500	4	-103.397	0.500	2
	6:CASE I:VX	0.500	34.821	0	1			
	9:1.1DL+WZ	0.500	506.615	0.500	4	-546.936	0.500	2
	10:CASE I: VY	0.500	109.198	0.500	3	-109.198	0.500	1
	11:CASE III: V)	0.500	81.899	0.500	3	-81.899	0.500	1
	12:CASE III: V)	0.500	147.031	0.500	1	-163.760	0.500	2
	13:CASE III: V)	0.500	26.116	0	1			
4	1:DL	0.500	109.198	0.500	3	-109.198	0.500	1
	2:DYNO DRUM	0.500	34.821	0	1			
	3:DYNO DRUM	0.500	218.346	0.500	1	-196.041	0.500	2
	7:WIND LOAD	0.500	208.472	0.500	1	-190.456	0.500	2
	8:WIND RESU	0.500	121.007	0.500	1	-109.611	0.500	2
	4:1.25DL	0.500	136.498	0.500	3	-136.498	0.500	1
	5:1.1DL+1.0W)	0.500	154.325	0.500	3	-103.397	0.500	1
	6:CASE I:VX	0.500	34.821	0	1			
	9:1.1DL+WZ	0.500	546.936	0.500	4	-506.615	0.500	2
	10:CASE I: VY	0.500	109.198	0.500	3	-109.198	0.500	1
	11:CASE III: V)	0.500	81.899	0.500	3	-81.899	0.500	1
	12:CASE III: V)	0.500	163.760	0.500	1	-147.031	0.500	2
	13:CASE III: V)	0.500	26.116	0	1			
8	1:DL	2.500	886.765	2.500	3	-886.765	2.500	1
	2:DYNO DRUM	2.500	29.307	0	1			
	3:DYNO DRUM	2.500	258.157	2.500	2	-305.554	2.500	1
	7:WIND LOAD	2.500	404.684	2.500	2	-438.921	2.500	1
	8:WIND RESU	2.500	162.139	2.500	2	-151.870	2.500	1
	4:1.25DL	2.500	1.11E+3	2.500	3	-1.11E+3	2.500	1
	5:1.1DL+1.0W)	2.500	1E+3	2.500	3	-948.600	2.500	1
	6:CASE I:VX	2.500	29.307	0	1			
	9:1.1DL+WZ	2.500	1.64E+3	2.500	3	-1.72E+3	2.500	1
	10:CASE I: VY	2.500	886.765	2.500	3	-886.765	2.500	1
	11:CASE III: V)	2.500	665.074	2.500	3	-665.074	2.500	1
	12:CASE III: V)	2.500	193.618	2.500	2	-229.165	2.500	1
	13:CASE III: V)	2.500	21.980	0	1			
9	1:DL	2.500	886.765	2.500	3	-886.765	2.500	1
	2:DYNO DRUM	2.500	29.307	0	1			
	3:DYNO DRUM	2.500	305.554	2.500	2	-258.157	2.500	1
	7:WIND LOAD	2.500	438.921	2.500	2	-404.684	2.500	1
	8:WIND RESU	2.500	167.067	2.500	2	-144.411	2.500	1



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Job Title **Abutment-Sides**

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By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	4:1.25DL	2.500	1.11E+3	2.500	3	-1.11E+3	2.500	1
	5:1.1DL+1.0WZ	2.500	1E+3	2.500	3	-948.600	2.500	1
	6:CASE I:VX	2.500	29.307	0	1			
	9:1.1DL+WZ	2.500	1.72E+3	2.500	3	-1.64E+3	2.500	1
	10:CASE I: VY	2.500	886.765	2.500	3	-886.765	2.500	1
	11:CASE III: V	2.500	665.074	2.500	3	-665.074	2.500	1
	12:CASE III: V _z	2.500	229.165	2.500	2	-193.618	2.500	1
	13:CASE III: V _z	2.500	21.980	0	1			

Plate Center Stress Summary

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Max Qx	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Min Qx	7	4:1.25DL	-0.000	-0.251	0	0	0	-0.020	-0.064	-0.000
Max Qy	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Min Qy	7	4:1.25DL	-0.000	-0.251	0	0	0	-0.020	-0.064	-0.000
Max Sx	7	3:DYNO DRUM	0	0	0.000	0.000	29.860	0	0	0
Min Sx	7	8:WIND RESU	0	0	-10.342	-0.888	14.273	0	0	0
Max Sy	7	9:1.1DL+WZ	-0.000	-0.221	-0.000	0.000	51.430	-0.017	-0.057	-0.000
Min Sy	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Max Sxy	7	9:1.1DL+WZ	-0.000	-0.221	-0.000	0.000	51.430	-0.017	-0.057	-0.000
Min Sxy	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Max Mx	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Min Mx	7	4:1.25DL	-0.000	-0.251	0	0	0	-0.020	-0.064	-0.000
Max My	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Min My	7	4:1.25DL	-0.000	-0.251	0	0	0	-0.020	-0.064	-0.000
Max Mxy	7	2:DYNO DRUM	0	0	-0.090	-1.358	-0.000	0	0	0
Min Mxy	7	4:1.25DL	-0.000	-0.251	0	0	0	-0.020	-0.064	-0.000

Plate Center Principal Stress Summary

	Plate	L/C	Principal		Von Mis		Tresca	
			Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)	Top (psi)	Bottom (psi)
Max (t)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929
Max (b)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929
Max VM (t)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929
Max VM (b)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929
Tresca (t)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929
Tresca (b)	7	9:1.1DL+WZ	47.906	55.023	89.210	89.210	102.929	102.929



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Job Title **Abutment-Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA3 Redesign- Abutm** Date/Time **06-Feb-2020 10:42**

Reactions

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
3	1:DL	0	0.050	0	-0.000	0	-1.454
	2:DYNO DRUM	-0.0522	0	0.000	0	0.001	0
	3:DYNO DRUM	0.045	0	-0.02777	0	-0.462	0
	7:WIND LOAD	0.032	0	-0.06	0	-0.692	0
	8:WIND RESU	-0.010	-0.053	-0.016	0	-0.257	0
	4:1.25DL	0	0.063	0	-0.000	0	-1.818
	5:1.1DL+1.0W)	-0.0522	0.055	0.000	-0.000	0.001	-1.600
	6:CASE I:VX	-0.0522	0	0.000	0	0.001	0
	9:1.1DL+WZ	0.077	0.055	-0.08777	-0.000	-1.154	-1.600
	10:CASE I: VY	0	0.050	0	-0.000	0	-1.454
	11:CASE III: V\	0	0.038	0	-0.000	0	-1.091
	12:CASE III: V;	0.034	0	-0.021	0	-0.347	0
	13:CASE III: V;	-0.03915	0	0.000	0	0.001	0
7	1:DL	0	0.050	0	0.000	0	-1.454
	2:DYNO DRUM	-0.0522	0	-0.000	0	-0.001	0
	3:DYNO DRUM	-0.045	0	-0.02777	0	-0.462	0
	7:WIND LOAD	-0.032	0	-0.06	0	-0.692	0
	8:WIND RESU	-0.021	0	-0.016	0	-0.255	0
	4:1.25DL	0	0.063	0	0.000	0	-1.818
	5:1.1DL+1.0W)	-0.0522	0.055	-0.000	0.000	-0.001	-1.600
	6:CASE I:VX	-0.0522	0	-0.000	0	-0.001	0
	9:1.1DL+WZ	-0.077	0.055	-0.08777	0.000	-1.154	-1.600
	10:CASE I: VY	0	0.050	0	0.000	0	-1.454
	11:CASE III: V\	0	0.038	0	0.000	0	-1.091
	12:CASE III: V;	-0.034	0	-0.021	0	-0.347	0
	13:CASE III: V;	-0.03915	0	-0.000	0	-0.001	0

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.014	1.000	0.014	HSS FLEX+A	9	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.014	1.000	0.014	HSS FLEX+A	9	1.890	2.460	2.460	4.030
8	HSST3X3X0	HSST3X3X0	0.044	1.000	0.044	HSS FLEX+A	9	1.890	2.460	2.460	4.030
9	HSST3X3X0	HSST3X3X0	0.044	1.000	0.044	HSS FLEX+A	9	1.890	2.460	2.460	4.030



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Job Title **Abutment-Sides**

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Ref

By **IERM** Date **19-Jun-18** Chd

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Statics Check Results

L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1:DL	Loads	0	-0.101	0	1.211	0	-0.724
1:DL	Reactions	0	0.101	0	-1.211	0	0.724
	Difference	0	-0.000	0	0.000	0	-0.000
2:DYNO DRUM F	Loads	0.104	0	0	0	1.253	0
2:DYNO DRUM F	Reactions	-0.104	0	0.000	0	-1.253	0
	Difference	0.000	0	0.000	0	0.000	0
3:DYNO DRUM F	Loads	0	0	0.05554	0	0	0
3:DYNO DRUM F	Reactions	0.000	0	-0.05554	0	-0.000	0
	Difference	0.000	0	-0.000	0	-0.000	0
7:WIND LOAD OI	Loads	0	0	0.120	0	-2.160	0
7:WIND LOAD OI	Reactions	0.000	0	-0.120	0	2.160	0
	Difference	0.000	0	-0.000	0	-0.000	0
8:WIND RESULT,	Loads	0.031	0.053	0.031	0	-0.093	1.908
8:WIND RESULT,	Reactions	-0.031	-0.053	-0.031	0	0.093	-1.908
	Difference	0.000	0	-0.000	0	-0.000	0

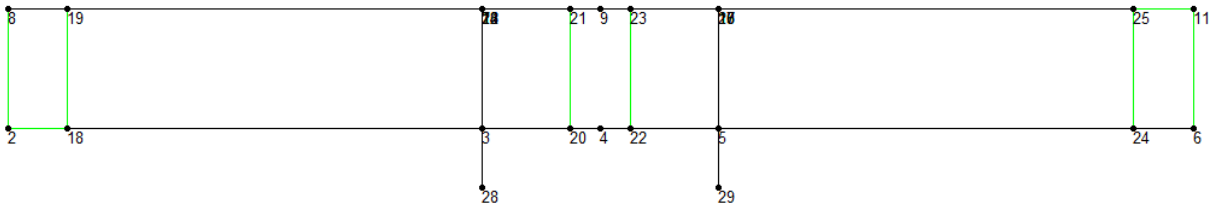
Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
Max FX	3	9:1.1DL+WZ	0.077	0.055	-0.08777	-0.000	-1.154	-1.600
Min FX	7	9:1.1DL+WZ	-0.077	0.055	-0.08777	0.000	-1.154	-1.600
Max FY	3	4:1.25DL	0	0.063	0	-0.000	0	-1.818
Min FY	3	8:WIND RESU	-0.010	-0.053	-0.016	0	-0.257	0
Max FZ	3	2:DYNO DRUM	-0.0522	0	0.000	0	0.001	0
Min FZ	3	9:1.1DL+WZ	0.077	0.055	-0.08777	-0.000	-1.154	-1.600
Max MX	7	4:1.25DL	0	0.063	0	0.000	0	-1.818
Min MX	3	4:1.25DL	0	0.063	0	-0.000	0	-1.818
Max MY	3	2:DYNO DRUM	-0.0522	0	0.000	0	0.001	0
Min MY	3	9:1.1DL+WZ	0.077	0.055	-0.08777	-0.000	-1.154	-1.600
Max MZ	3	2:DYNO DRUM	-0.0522	0	0.000	0	0.001	0
Min MZ	3	4:1.25DL	0	0.063	0	-0.000	0	-1.818

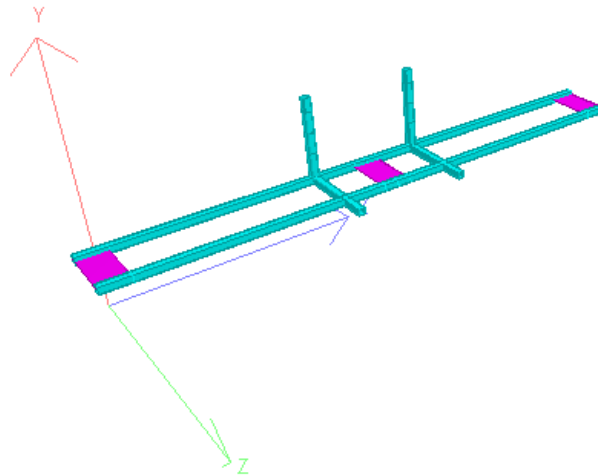


Abutment-Middle

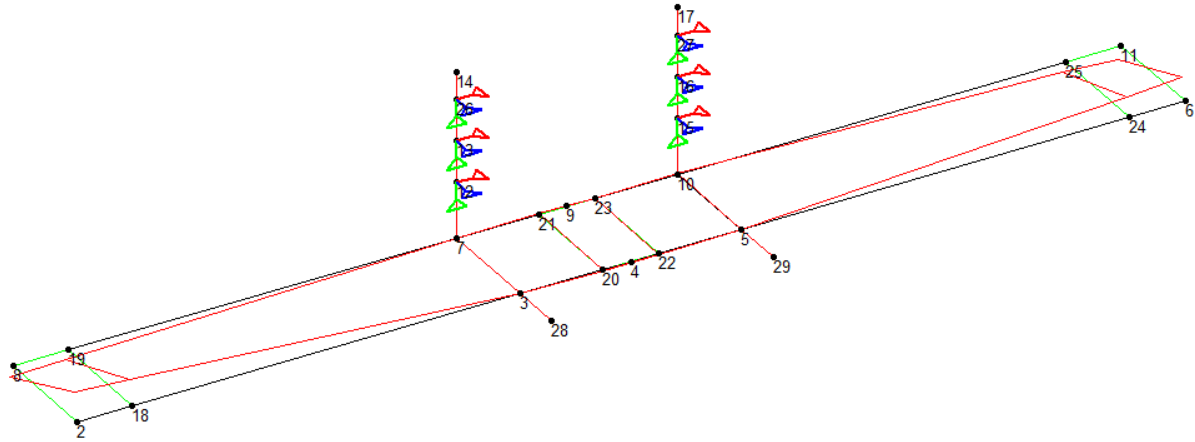
Plan View:



3D View:



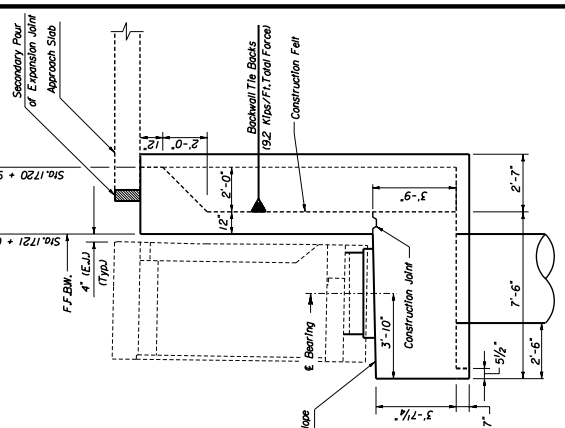
Deflection View:



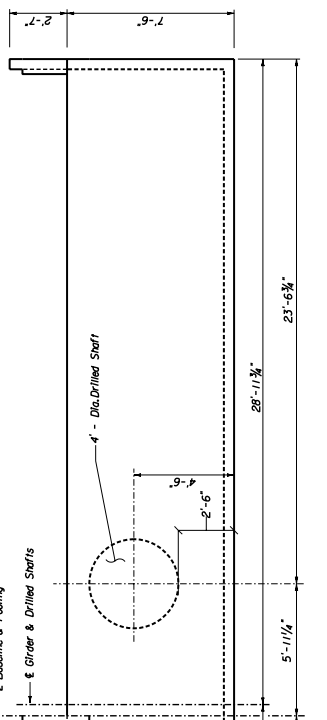


Existing Structural Plans

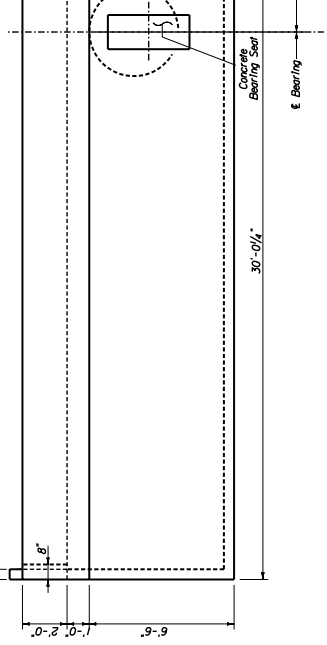
DATE	SCALE	REVISION
12/13/02	1/4" = 1'-0"	1
12/13/02	1/4" = 1'-0"	2
12/13/02	1/4" = 1'-0"	3
12/13/02	1/4" = 1'-0"	4
12/13/02	1/4" = 1'-0"	5
12/13/02	1/4" = 1'-0"	6
12/13/02	1/4" = 1'-0"	7
12/13/02	1/4" = 1'-0"	8
12/13/02	1/4" = 1'-0"	9
12/13/02	1/4" = 1'-0"	10



Section A-A



Section B-B

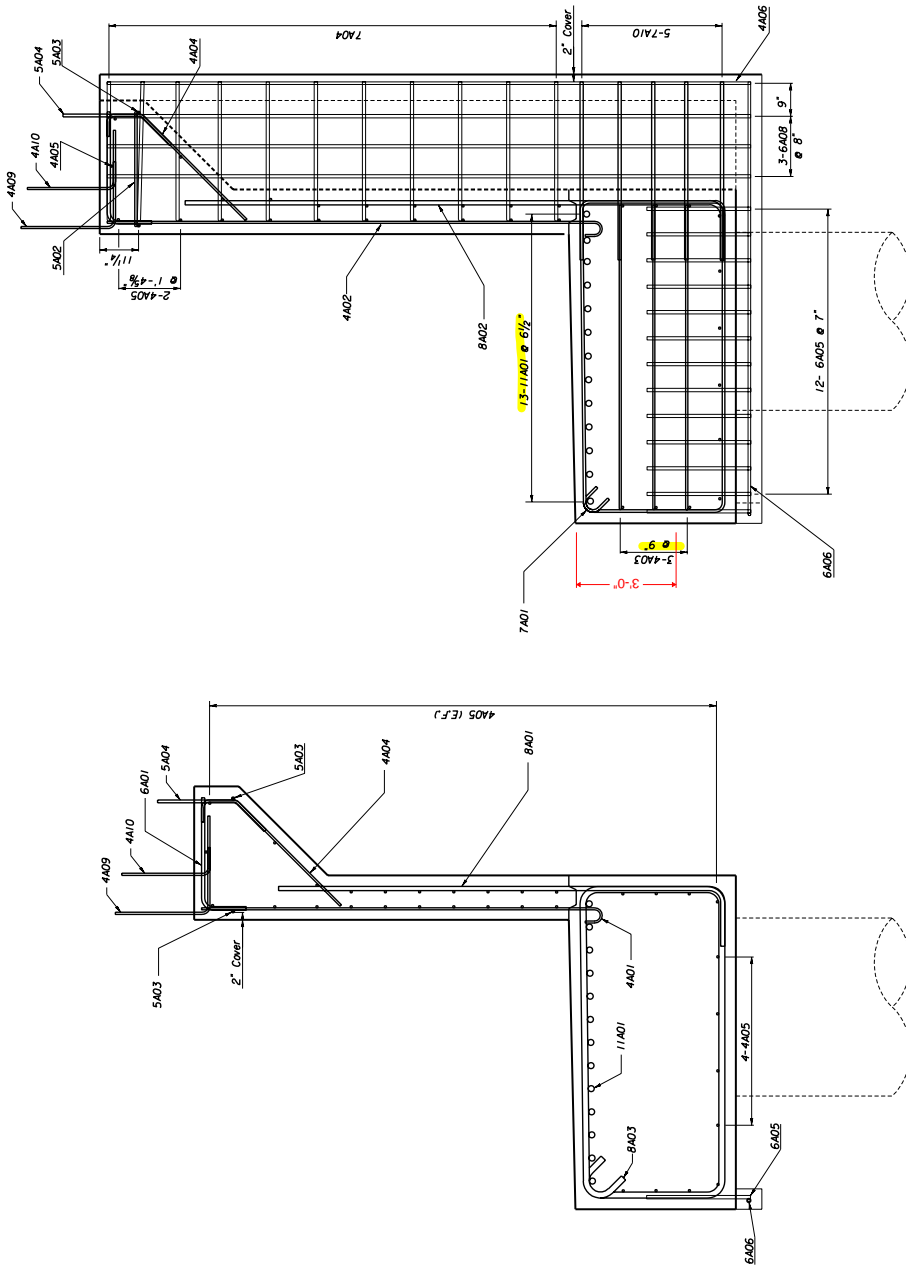


NOTES:

1. For Approach Slab Details See Sheet T-7.
2. For Wall Details See Corresponding Wall Plans.
3. For Bearing Details See Bearing Details Sheets.
4. For Expansion Joint Details See Expansion Joint Details Sheets.
5. For Drilled Shaft Details See Sheets T-156 through T-164.
6. Provide for 1/2" Polystyrene Joint Material between the Wall and Abutment.
7. Contractor must Coordinate Construction of Back Wall to Allow for Installation of Transition in the Superstructure. Contractor may require Blockout with Rebar Couplers based on Construction Schedule.
8. For Drainage Details, see Sheet T-102.
9. Traffic Rolling Barrier not shown. Barrier Transitions on Back Wall. See Sheet T-6 For Details.
10. Drainage Pipe to be Class 50 8" Ductile Iron Pipe w/ Push on Fittings. Cost of Bents to be included in the Cost of Pipe.

STRUCTURE NOS. 100800, 100806 & 100812		DRAWING NO. T-126	
PROJECT NAME: TAMPAN EXPRESSWAY AUTHORITY		PROJECT NO. 5140.01	
COUNTY: HILLSBOROUGH		CONSTRUCTION PROJECT NO. THCEA 5140.01	
S.R. 618		THCEA 5140.01	
ENGINEER OF RECORD: J. Rodriguez		DATE: 12-13-02	
CHECKED BY: DLS		DATE: 12-13-02	
DESIGNED BY: DLS		DATE: 12-13-02	
APPROVED BY: J. Rodriguez		DATE: 12-13-02	
REVISIONS		DESCRIPTION	
DATE	BY	DATE	DESCRIPTION

DATE	STATE	EXPIRES PROJECT NO.
12/13/02	FLA.	50-30-001 & 51-30-01

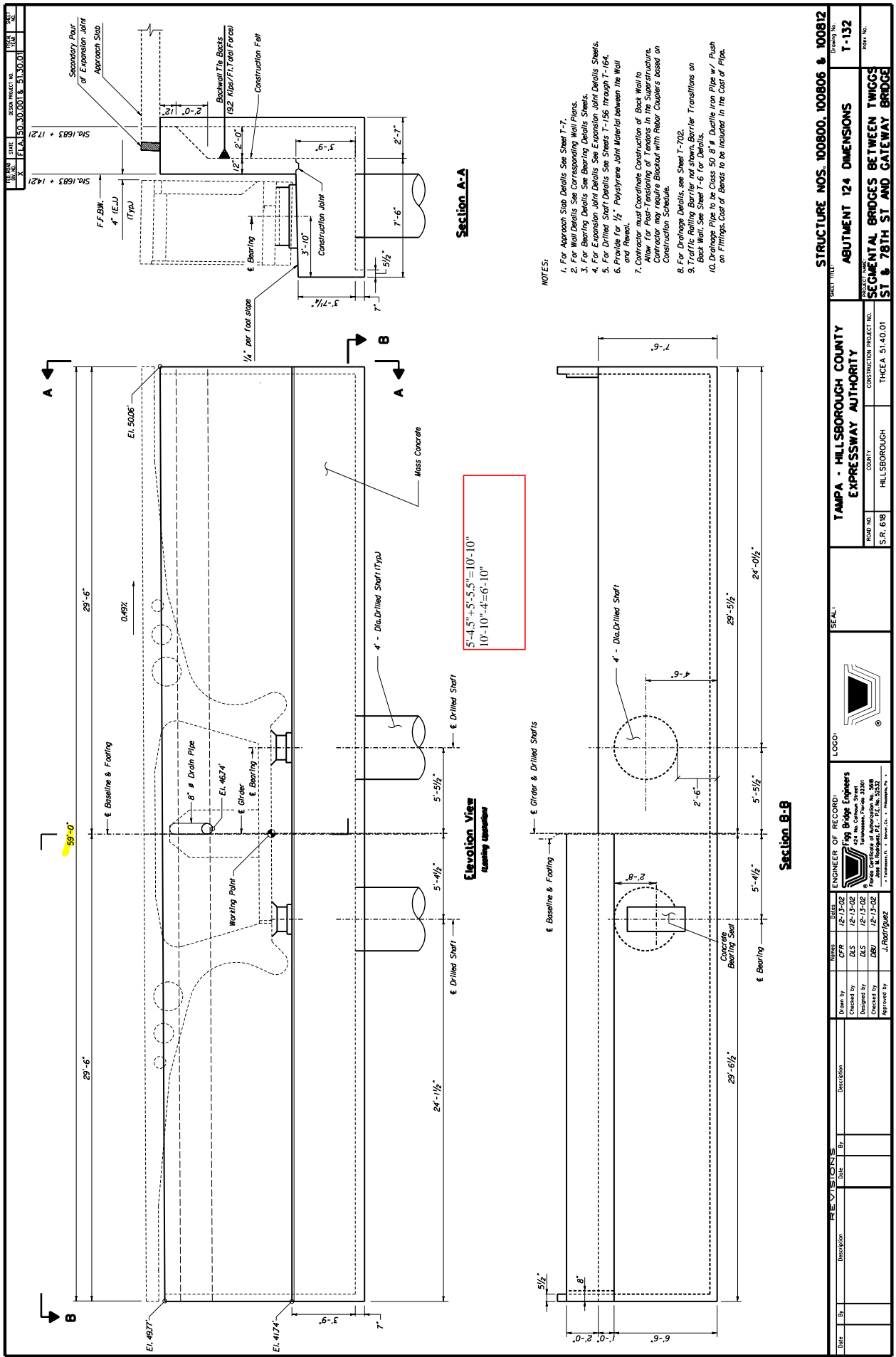


NOTE:
 1. Minimum Concrete Cover = 3" (Unless Otherwise Noted).
 2. (E.F.J) Denotes Each Face
 (O.F.) Denotes Outside Face
 (I.F.) Denotes Inside Face

Side View

Section E-E

DATE		BY		DESCRIPTION	
REVISIONS					
DRAWN BY		CHECKED BY		DESIGNED BY	
CFR		DLS		DLS	
DATE		DATE		DATE	
12-13-02		12-13-02		12-13-02	
APPROVED BY		APPROVED BY		APPROVED BY	
J. Rodriguez		J. Rodriguez		J. Rodriguez	
ENGINEER OF RECORD: Five Bridge Engineers 124 W. Carson Street Tallahassee, Florida 32301 P.E. No. 5332 P.E. No. 5332 Tallahassee, FL 32301					
LOGO		SEAL		PROJECT TITLE	
[Logo]		[Seal]		TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY	
FORM NO.		COUNTY		CONSTRUCTION PROJECT NO.	
S.R. 618		HILLSBOROUGH		THCEA 5140.01	
SHEET TITLE		DRAWING NO.		PROJECT NO.	
STRUCTURE NOS. 100800, 100806 & 100812		1-129		1-129	
SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE					



Section A-A

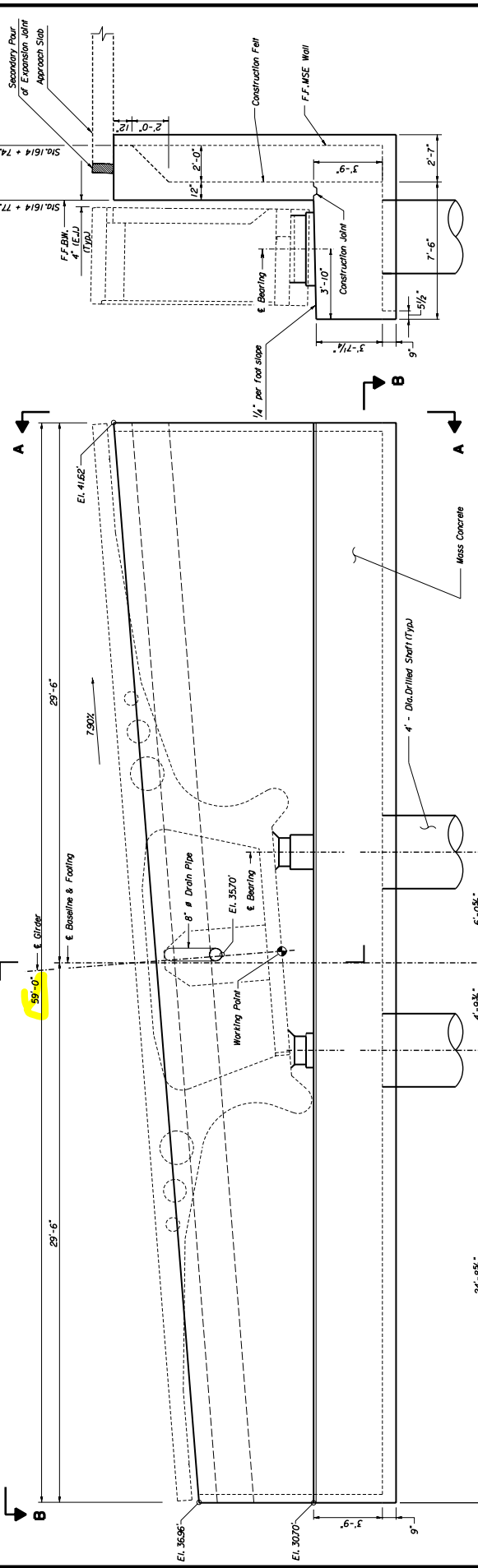
NOTES:

1. For Approach Sub Details See Sheet T-7.
2. For Back Wall See Connecting Wall Plans.
3. For Expansion Joints See Expansion Joint Details Sheets.
4. For Expansion Joint Details See Expansion Joint Details Sheets.
5. For Drilled Shaft Details See Sheets T-155 through T-164.
6. Provide for 1/2" Polystyrene Joint Material between the Wall and Retent.
7. Contractor must Coordinate Construction of Back Wall to Allow for Post-Tensioning of Tendons in the Superstructure. Contractor may require Backout with Fiber Couplers based on Construction Schedule.
8. For Drainage Details, see Sheet T-702.
9. Traffic Railing Barrier not shown. Barrier Transitions on Back Wall. See Sheet T-6 for Details.
10. Drainage Pipe to be Class 50 9" Diameter Iron Pipe w/ Push on Fittings. Cor of Bents to be Included in the Cor of Pipes.

Elevation View
Facing upstream

Section B-B

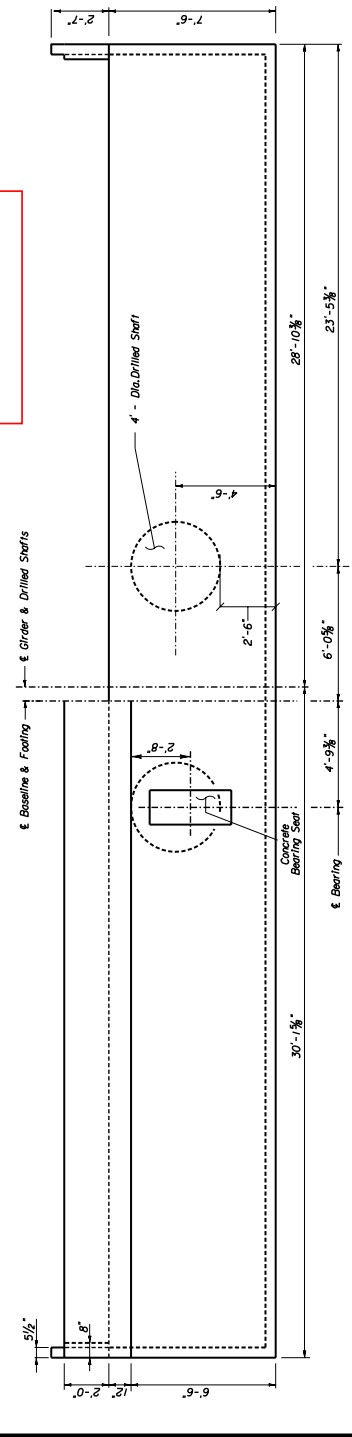
SHEET TITLE: STRUCTURE NOS. 100800, 100806 & 100812 DRAWING NO: T-132		PROJECT NAME: SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE PROJECT NO.: THCEA 5140.01	
COUNTY: HILLSBOROUGH S.R. NO.: 618		COUNTY: HILLSBOROUGH CONSTRUCTION PROJECT NO.: THCEA 5140.01	
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY			
ENGINEER OF RECORD: J. Rodriguez 124 N. Canyon Street Lakeland, Florida 33801 Phone: 813.948.2100 Fax: 813.948.2101 E-Mail: jrodriguez@jrodriguez.com		DATE: 12-13-02 DRAWN BY: CFR CHECKED BY: DLS DESIGNED BY: DLS APPROVED BY: J. Rodriguez	
DATE	DESCRIPTION	BY	REVISIONS



Section A-A

$4'-9.375'' + 6'-0.625'' = 10'-10''$
 $10'-10'' - 4'' = 6'-10''$

Elevation View
Cutaway Dimension



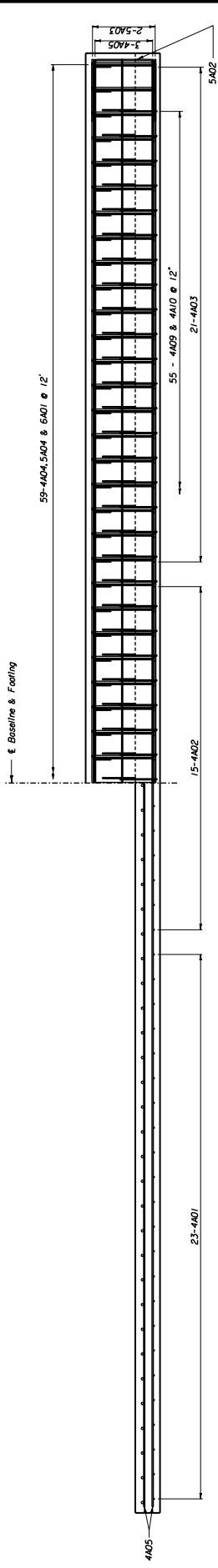
Section B-B

- NOTES:
1. For Approach Slab Details See Sheet T-7.
 2. For Wall Details See Corresponding Wall Plans.
 3. For Bearing Details See Bearing Details Sheets.
 4. For Expansion Joint Details See Expansion Joint Details Sheets.
 5. For Drilled Shaft Details See Sheets T-156 through T-164.
 6. Provide for 1/2" Polystyrene Joint Material between the Wall and Abutment.
 7. Contractor must Coordinate Construction of Back Wall to ensure proper fit with existing structures. Contractor may require Blockout with Rebar Couplers based on Construction Schedule.
 8. For Drainage Details, see Sheet T-702.
 9. Traffic Rolling Barrier not shown. Barrier Transitions on Back Wall. See Sheet T-6 for Details.
 10. Drainage Pipe to be Class 50 8" Ductile Iron Pipe w/ Push on Fittings. Cost of Bents to be included in the Cost of Pipe.

REVISIONS		DATE		DESCRIPTION	
NO.	BY	DATE	DESCRIPTION	NO.	BY

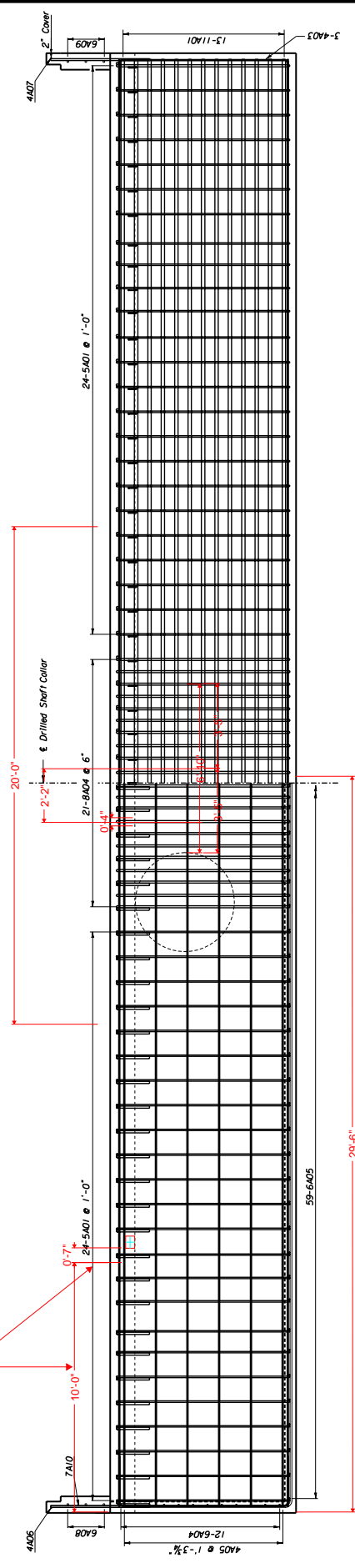
ENGINEER OF RECORD: FLORIAN BRIDGE EXPERTS 424 N. CAROL STREET TAMPA, FLORIDA 33601 PHONE: 813.281.1111 FAX: 813.281.1112 www.florianbridge.com	COUNTY: HILLSBOROUGH PROJECT NO.: THCEA 5140.01 DRAWING NO.: 1-138 SHEET NO.: 152	TAMP A - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY PROJECT NAME: SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE STRUCTURE NOS. 100800, 100806 & 100812
--	--	---

DATE	SCALE	REVISION
12/13/02	1/4" = 1'-0"	1. REVISED
12/13/02	1/4" = 1'-0"	2. REVISED
12/13/02	1/4" = 1'-0"	3. REVISED
12/13/02	1/4" = 1'-0"	4. REVISED
12/13/02	1/4" = 1'-0"	5. REVISED
12/13/02	1/4" = 1'-0"	6. REVISED
12/13/02	1/4" = 1'-0"	7. REVISED
12/13/02	1/4" = 1'-0"	8. REVISED
12/13/02	1/4" = 1'-0"	9. REVISED
12/13/02	1/4" = 1'-0"	10. REVISED
12/13/02	1/4" = 1'-0"	11. REVISED
12/13/02	1/4" = 1'-0"	12. REVISED
12/13/02	1/4" = 1'-0"	13. REVISED
12/13/02	1/4" = 1'-0"	14. REVISED
12/13/02	1/4" = 1'-0"	15. REVISED
12/13/02	1/4" = 1'-0"	16. REVISED
12/13/02	1/4" = 1'-0"	17. REVISED
12/13/02	1/4" = 1'-0"	18. REVISED
12/13/02	1/4" = 1'-0"	19. REVISED
12/13/02	1/4" = 1'-0"	20. REVISED
12/13/02	1/4" = 1'-0"	21. REVISED
12/13/02	1/4" = 1'-0"	22. REVISED
12/13/02	1/4" = 1'-0"	23. REVISED
12/13/02	1/4" = 1'-0"	24. REVISED
12/13/02	1/4" = 1'-0"	25. REVISED
12/13/02	1/4" = 1'-0"	26. REVISED
12/13/02	1/4" = 1'-0"	27. REVISED
12/13/02	1/4" = 1'-0"	28. REVISED
12/13/02	1/4" = 1'-0"	29. REVISED
12/13/02	1/4" = 1'-0"	30. REVISED
12/13/02	1/4" = 1'-0"	31. REVISED
12/13/02	1/4" = 1'-0"	32. REVISED
12/13/02	1/4" = 1'-0"	33. REVISED
12/13/02	1/4" = 1'-0"	34. REVISED
12/13/02	1/4" = 1'-0"	35. REVISED
12/13/02	1/4" = 1'-0"	36. REVISED
12/13/02	1/4" = 1'-0"	37. REVISED
12/13/02	1/4" = 1'-0"	38. REVISED
12/13/02	1/4" = 1'-0"	39. REVISED
12/13/02	1/4" = 1'-0"	40. REVISED
12/13/02	1/4" = 1'-0"	41. REVISED
12/13/02	1/4" = 1'-0"	42. REVISED
12/13/02	1/4" = 1'-0"	43. REVISED
12/13/02	1/4" = 1'-0"	44. REVISED
12/13/02	1/4" = 1'-0"	45. REVISED
12/13/02	1/4" = 1'-0"	46. REVISED
12/13/02	1/4" = 1'-0"	47. REVISED
12/13/02	1/4" = 1'-0"	48. REVISED
12/13/02	1/4" = 1'-0"	49. REVISED
12/13/02	1/4" = 1'-0"	50. REVISED
12/13/02	1/4" = 1'-0"	51. REVISED
12/13/02	1/4" = 1'-0"	52. REVISED
12/13/02	1/4" = 1'-0"	53. REVISED
12/13/02	1/4" = 1'-0"	54. REVISED
12/13/02	1/4" = 1'-0"	55. REVISED
12/13/02	1/4" = 1'-0"	56. REVISED
12/13/02	1/4" = 1'-0"	57. REVISED
12/13/02	1/4" = 1'-0"	58. REVISED
12/13/02	1/4" = 1'-0"	59. REVISED
12/13/02	1/4" = 1'-0"	60. REVISED
12/13/02	1/4" = 1'-0"	61. REVISED
12/13/02	1/4" = 1'-0"	62. REVISED
12/13/02	1/4" = 1'-0"	63. REVISED
12/13/02	1/4" = 1'-0"	64. REVISED
12/13/02	1/4" = 1'-0"	65. REVISED
12/13/02	1/4" = 1'-0"	66. REVISED
12/13/02	1/4" = 1'-0"	67. REVISED
12/13/02	1/4" = 1'-0"	68. REVISED
12/13/02	1/4" = 1'-0"	69. REVISED
12/13/02	1/4" = 1'-0"	70. REVISED
12/13/02	1/4" = 1'-0"	71. REVISED
12/13/02	1/4" = 1'-0"	72. REVISED
12/13/02	1/4" = 1'-0"	73. REVISED
12/13/02	1/4" = 1'-0"	74. REVISED
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12/13/02	1/4" = 1'-0"	78. REVISED
12/13/02	1/4" = 1'-0"	79. REVISED
12/13/02	1/4" = 1'-0"	80. REVISED
12/13/02	1/4" = 1'-0"	81. REVISED
12/13/02	1/4" = 1'-0"	82. REVISED
12/13/02	1/4" = 1'-0"	83. REVISED
12/13/02	1/4" = 1'-0"	84. REVISED
12/13/02	1/4" = 1'-0"	85. REVISED
12/13/02	1/4" = 1'-0"	86. REVISED
12/13/02	1/4" = 1'-0"	87. REVISED
12/13/02	1/4" = 1'-0"	88. REVISED
12/13/02	1/4" = 1'-0"	89. REVISED
12/13/02	1/4" = 1'-0"	90. REVISED
12/13/02	1/4" = 1'-0"	91. REVISED
12/13/02	1/4" = 1'-0"	92. REVISED
12/13/02	1/4" = 1'-0"	93. REVISED
12/13/02	1/4" = 1'-0"	94. REVISED
12/13/02	1/4" = 1'-0"	95. REVISED
12/13/02	1/4" = 1'-0"	96. REVISED
12/13/02	1/4" = 1'-0"	97. REVISED
12/13/02	1/4" = 1'-0"	98. REVISED
12/13/02	1/4" = 1'-0"	99. REVISED
12/13/02	1/4" = 1'-0"	100. REVISED



Section C-C

*Note: Abutment-Sides spacing.



Section A-A

Section B-B

- NOTE:
1. Minimum Concrete Cover - 3" (Unless Otherwise Noted).
 2. (E.F.) Denotes Each Face
 - (O.F.) Denotes Outside Face
 - (I.F.) Denotes Inside Face

DATE		DESCRIPTION		BY	DATE	DESCRIPTION
<p>ENGINEER OF RECORD: J. Rodriguez J. Rodriguez 123 N. Central Street Tallahassee, Florida 32301 P.E. No. 5332 F.L.A. No. 5332</p>						
TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		COUNTY: HILLSBOROUGH		CONSTRUCTION PROJECT NO.: THCA 5140.01		
FORM NO. S.R. 618		PROJECT NO. 100800, 100806 & 100812		DRAWING NO. T-140		
<p>SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE</p>						

13 DEC 2002 15:11:24



STAAD Analysis

```

*****
*
*          STAAD.Pro V8i SELECTseries6          *
*          Version  20.07.11.70                 *
*          Proprietary Program of               *
*          Bentley Systems, Inc.                *
*          Date=    JUL 19, 2018                *
*          Time=    13: 7:36                    *
*
*          USER ID: Kimley-Horn and Associates  *
*****

```

```

1. STAAD SPACE
INPUT FILE: \\kimley-horn.com\FL_ORL\ORL_Structures\_Projects-Structures\148872000 THEA Lighting Proje.. .STD
2. START JOB INFORMATION
3. ENGINEER DATE 05-JUN-18
4. JOB NAME ABUTMENT MIDDLE
5. JOB CLIENT THEA
6. JOB NO 148872000
7. JOB REV 3
8. ENGINEER NAME IERM
9. END JOB INFORMATION
10. INPUT WIDTH 79
11. UNIT FEET KIP
12. JOINT COORDINATES
13. 2 0 0 -1; 3 8 0 -1; 4 10 0 -1; 5 12 0 -1; 6 20 0 -1; 7 8 0 -3; 8 0 0 -3
14. 9 10 0 -3; 10 12 0 -3; 11 20 0 -3; 12 8 1 -3; 13 8 1.75 -3; 14 8 3 -3
15. 15 12 1 -3; 16 12 1.75 -3; 17 12 3 -3; 18 1 0 -1; 19 1 0 -3; 20 9.5 0 -1.
16. 21 9.5 0 -3; 22 10.5 0 -1; 23 10.5 0 -3; 24 19 0 -1; 25 19 0 -3; 26 8 2.5 -3
17. 27 12 2.5 -3; 28 8 0 0; 29 12 0 0
18. MEMBER INCIDENCES
19. 1 2 18; 2 3 20; 3 4 22; 4 5 24; 5 3 7; 6 5 10; 7 8 19; 8 7 21; 9 9 23
20. 10 10 25; 11 7 12; 12 12 13; 13 13 26; 14 10 15; 15 15 16; 16 16 27; 17 18 3
21. 18 19 7; 19 20 4; 20 21 9; 21 22 5; 22 23 10; 23 24 6; 24 25 11; 25 26 14
22. 26 27 17; 30 3 28; 31 5 29
23. ELEMENT INCIDENCES SHELL
24. 32 2 8 19 18; 33 20 21 23 22; 34 24 25 11 6
25. ELEMENT PROPERTY
26. 32 TO 34 THICKNESS 0.020833
27. DEFINE MATERIAL START
28. ISOTROPIC STEEL
29. E 4.176E+006
30. POISSON 0.3
31. DENSITY 0.489024
32. ALPHA 6E-006
33. DAMP 0.03
34. TYPE STEEL
35. STRENGTH FY 5184 FU 8352 RY 1.5 RT 1.2
36. G 1.60615E+006
37. ISOTROPIC ALUMINUM
38. E 1.44E+006

```

STAAD SPACE

-- PAGE NO. 2

39. POISSON 0.33
40. DENSITY 0.169344
41. ALPHA 1.3E-005
42. DAMP 0.03
43. ISOTROPIC A500-GR.B
44. E 4.176E+006
45. POISSON 0.3
46. DENSITY 0.49
47. ALPHA 6E-006
48. DAMP 0.03
49. G 1.6128E-006
50. TYPE STEEL
51. STRENGTH FY 6624 FU 8352 RY 1.1 RT 1.2
52. END DEFINE MATERIAL
53. MEMBER PROPERTY AMERICAN
54. 1 TO 26 30 31 TABLE ST HSST3X3X0.188
55. CONSTANTS
56. MATERIAL STEEL MEMB 32 TO 34
57. MATERIAL A500-GR.B MEMB 1 TO 26 30 31
58. SUPPORTS
59. 12 13 15 16 26 27 FIXED BUT MX MY MZ
60. LOAD 2 LOADTYPE WIND TITLE W1
61. JOINT LOAD
62. 2 6 8 11 FZ -0.0522
63. 2 6 8 11 MX -0.0324
64. 2 6 8 11 FX 0.0277
65. 2 6 8 11 MZ -0.017
66. LOAD 1 LOADTYPE DEAD TITLE DL
67. SELFWEIGHT Y -1
68. JOINT LOAD
69. 2 6 8 11 FY -0.015
70. 4 9 FY -0.0264
71. LOAD 3 LOADTYPE WIND TITLE W2
72. JOINT LOAD
73. 4 9 FZ -0.0293
74. 4 9 MX -0.0173
75. 4 9 FX 0.0277
76. 4 9 MZ -0.0159
77. LOAD 7 LOADTYPE WIND TITLE 0.75W3
78. JOINT LOAD
79. 2 6 8 11 FZ -0.039
80. 2 6 8 11 MX -0.024
81. 2 6 8 11 FX 0.021
82. 2 6 8 11 MZ -0.013
83. 4 9 FZ -0.022
84. 4 9 MX -0.013
85. 4 9 FX 0.021
86. 4 9 MZ -0.012
87. LOAD COMB 4 1.25DL
88. 1 1.25
89. LOAD COMB 5 1.1DL+1.0W1
90. 1 1.1 2 1.0
91. LOAD COMB 6 1.1DL+1.0W2
92. 1 1.1 3 1.0
93. LOAD COMB 8 1.1DL+1.0W3
94. 1 1.1 7 1.0

STAAD SPACE

-- PAGE NO. 3

95. PERFORM ANALYSIS PRINT ALL

P R O B L E M S T A T I S T I C S

NUMBER OF JOINTS	28	NUMBER OF MEMBERS	28
NUMBER OF PLATES	3	NUMBER OF SOLIDS	0
NUMBER OF SURFACES	0	NUMBER OF SUPPORTS	6

SOLVER USED IS THE OUT-OF-CORE BASIC SOLVER

ORIGINAL/FINAL BAND-WIDTH=	25/	6/	39	DOF
TOTAL PRIMARY LOAD CASES =	4,	TOTAL DEGREES OF FREEDOM =	150	
TOTAL LOAD COMBINATION CASES =	4	SO FAR.		
SIZE OF STIFFNESS MATRIX =	6	DOUBLE KILO-WORDS		
REQRD/AVAIL. DISK SPACE =	12.1/	0.0	MB	

LOADING 2 LOADTYPE WIND TITLE W1

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	0.00	0.00	-0.05	0.00	0.00	0.00
6	0.00	0.00	-0.05	0.00	0.00	0.00
8	0.00	0.00	-0.05	0.00	0.00	0.00
11	0.00	0.00	-0.05	0.00	0.00	0.00
2	0.00	0.00	0.00	-0.03	0.00	0.00
6	0.00	0.00	0.00	-0.03	0.00	0.00
8	0.00	0.00	0.00	-0.03	0.00	0.00
11	0.00	0.00	0.00	-0.03	0.00	0.00
2	0.03	0.00	0.00	0.00	0.00	0.00
6	0.03	0.00	0.00	0.00	0.00	0.00
8	0.03	0.00	0.00	0.00	0.00	0.00
11	0.03	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	-0.02
6	0.00	0.00	0.00	0.00	0.00	-0.02
8	0.00	0.00	0.00	0.00	0.00	-0.02
11	0.00	0.00	0.00	0.00	0.00	-0.02

LOADING 1 LOADTYPE DEAD TITLE DL

SELFWEIGHT Y -1.000

ACTUAL WEIGHT OF THE STRUCTURE = 0.396 KIP

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	0.00	-0.01	0.00	0.00	0.00	0.00
6	0.00	-0.01	0.00	0.00	0.00	0.00
8	0.00	-0.01	0.00	0.00	0.00	0.00
11	0.00	-0.01	0.00	0.00	0.00	0.00
4	0.00	-0.03	0.00	0.00	0.00	0.00
9	0.00	-0.03	0.00	0.00	0.00	0.00

LOADING 3 LOADTYPE WIND TITLE W2

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
-------	---------	---------	---------	-------	-------	-------

STAAD SPACE -- PAGE NO. 5

4	0.00	0.00	-0.03	0.00	0.00	0.00
9	0.00	0.00	-0.03	0.00	0.00	0.00
4	0.00	0.00	0.00	-0.02	0.00	0.00
9	0.00	0.00	0.00	-0.02	0.00	0.00
4	0.03	0.00	0.00	0.00	0.00	0.00
9	0.03	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.00	0.00	-0.02
9	0.00	0.00	0.00	0.00	0.00	-0.02

LOADING 7 LOADTYPE WIND TITLE 0.75W3

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	0.00	0.00	-0.04	0.00	0.00	0.00
6	0.00	0.00	-0.04	0.00	0.00	0.00
8	0.00	0.00	-0.04	0.00	0.00	0.00
11	0.00	0.00	-0.04	0.00	0.00	0.00
2	0.00	0.00	0.00	-0.02	0.00	0.00
6	0.00	0.00	0.00	-0.02	0.00	0.00
8	0.00	0.00	0.00	-0.02	0.00	0.00
11	0.00	0.00	0.00	-0.02	0.00	0.00
2	0.02	0.00	0.00	0.00	0.00	0.00
6	0.02	0.00	0.00	0.00	0.00	0.00
8	0.02	0.00	0.00	0.00	0.00	0.00
11	0.02	0.00	0.00	0.00	0.00	0.00
2	0.00	0.00	0.00	0.00	0.00	-0.01
6	0.00	0.00	0.00	0.00	0.00	-0.01
8	0.00	0.00	0.00	0.00	0.00	-0.01
11	0.00	0.00	0.00	0.00	0.00	-0.01
4	0.00	0.00	-0.02	0.00	0.00	0.00
9	0.00	0.00	-0.02	0.00	0.00	0.00
4	0.00	0.00	0.00	-0.01	0.00	0.00
9	0.00	0.00	0.00	-0.01	0.00	0.00
4	0.02	0.00	0.00	0.00	0.00	0.00
9	0.02	0.00	0.00	0.00	0.00	0.00
4	0.00	0.00	0.00	0.00	0.00	-0.01
9	0.00	0.00	0.00	0.00	0.00	-0.01

*WARNING- ZERO STIFFNESS IN DIRECTION 6 AT JOINT 28 EQN.NO. 48
 LOADS APPLIED OR DISTRIBUTED HERE FROM ELEMENTS WILL BE IGNORED.
 THIS MAY BE DUE TO ALL MEMBERS AT THIS JOINT BEING RELEASED OR
 EFFECTIVELY RELEASED IN THIS DIRECTION.

*WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 12 EQN.NO. 56
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 4 EQN.NO. 61
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 9 EQN.NO. 79
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 13 EQN.NO. 83
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 26 EQN.NO. 98
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 15 EQN.NO. 107
 *WARNING- ZERO STIFFNESS IN DIRECTION 6 AT JOINT 29 EQN.NO. 120
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 14 EQN.NO. 125
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 16 EQN.NO. 140
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 27 EQN.NO. 143

Stiffness at the connections is expected since the plates are the major contributing factor. The warning is considered but not a cause for concern in the design.

*WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 17 EQN.NO. 149

FOR LOADING - 2

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
6	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
8	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02
11	2.77000E-02	0.00000E+00	-5.22000E-02	-3.24000E-02	0.00000E+00	-1.70000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.613718474E+00
Z = -0.200000006E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.620689705E+00
Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = 0.11
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = -0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.13 MY= 1.87 MZ= -0.07

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = -0.11
SUMMATION FORCE-Y = -0.00
SUMMATION FORCE-Z = 0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.13 MY= -1.87 MZ= 0.07

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)

MAXIMUMS AT NODE
X = 3.06516E-03 29
Y = 2.37086E-01 2
Z = -5.05808E-02 6
RX= -1.86232E-02 8
RY= 1.49978E-04 25
RZ= -3.07549E-03 2

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ	
							SUPPORT=1
12	0.00 -0.21	0.00 0.00	0.00 -0.07	0.00 -0.00	0.00 -0.00	0.00 0.00	111000
15	0.00 0.41	0.00 -0.00	0.00 -0.27	0.00 -0.00	0.00 0.00	0.00 0.00	111000
16	0.00 -0.14	0.00 0.00	0.00 0.17	0.00 -0.00	0.00 0.00	0.00 -0.00	111000

FOR LOADING - 1
APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	0.00000E+00	-2.33095E-02	0.00000E+00	0.00000E+00	0.00000E+00	-5.35938E-04
3	0.00000E+00	-3.69797E-02	0.00000E+00	-1.60781E-03	0.00000E+00	2.50551E-02
4	0.00000E+00	-2.96156E-02	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
5	0.00000E+00	-3.69797E-02	0.00000E+00	-1.60781E-03	0.00000E+00	-2.50551E-02
6	0.00000E+00	-2.33095E-02	0.00000E+00	0.00000E+00	0.00000E+00	5.35938E-04
7	0.00000E+00	-3.69797E-02	0.00000E+00	2.14375E-03	0.00000E+00	2.50551E-02
8	0.00000E+00	-2.33095E-02	0.00000E+00	0.00000E+00	0.00000E+00	-5.35938E-04
9	0.00000E+00	-2.96156E-02	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
10	0.00000E+00	-3.69797E-02	0.00000E+00	2.14375E-03	0.00000E+00	-2.50551E-02
11	0.00000E+00	-2.33095E-02	0.00000E+00	0.00000E+00	0.00000E+00	5.35938E-04
12	0.00000E+00	-5.62734E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
13	0.00000E+00	-4.82344E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
14	0.00000E+00	-1.60781E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
15	0.00000E+00	-5.62734E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
16	0.00000E+00	-4.82344E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
17	0.00000E+00	-1.60781E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
18	0.00000E+00	-3.08189E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.57250E-02
19	0.00000E+00	-3.08189E-02	0.00000E+00	0.00000E+00	0.00000E+00	-2.57250E-02
20	0.00000E+00	-1.15252E-02	0.00000E+00	0.00000E+00	0.00000E+00	1.07188E-03
21	0.00000E+00	-1.15252E-02	0.00000E+00	0.00000E+00	0.00000E+00	1.07188E-03
22	0.00000E+00	-1.15252E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03
23	0.00000E+00	-1.15252E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03
24	0.00000E+00	-3.08189E-02	0.00000E+00	0.00000E+00	0.00000E+00	2.57250E-02
25	0.00000E+00	-3.08189E-02	0.00000E+00	0.00000E+00	0.00000E+00	2.57250E-02
26	0.00000E+00	-4.01953E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
27	0.00000E+00	-4.01953E-03	0.00000E+00	0.00000E+00	0.00000E+00	0.00000E+00
28	0.00000E+00	-3.21562E-03	0.00000E+00	-5.35938E-04	0.00000E+00	0.00000E+00
29	0.00000E+00	-3.21562E-03	0.00000E+00	-5.35938E-04	0.00000E+00	0.00000E+00

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.113860572E+00
Z = -0.203795358E+01

STAAD SPACE

-- PAGE NO. 8

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = -0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -1.04 MY= 0.00 MZ= -5.08

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = 0.51
 SUMMATION FORCE-Z = -0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 1.04 MY= 0.00 MZ= 5.08

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)
 MAXIMUMS AT NODE
 X = -1.68429E-04 10
 Y = -3.46242E-01 6
 Z = -4.86043E-03 11
 RX= 5.81508E-03 19
 RY= 7.43473E-06 29
 RZ= 4.14787E-03 2

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/	
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ	
							SUPPORT=1
12	0.00	-0.01	0.00	0.00	0.00	0.00	
	-0.55	-0.24	-0.41	-0.00	-0.00	-0.00	111000
13	0.00	-0.00	0.00	0.00	0.00	0.00	
	0.17	0.00	0.49	-0.00	-0.00	-0.00	111000
15	0.00	-0.01	0.00	0.00	0.00	0.00	
	0.55	-0.24	-0.41	-0.00	0.00	0.00	111000
16	0.00	-0.00	0.00	0.00	0.00	0.00	
	-0.17	0.00	0.49	-0.00	0.00	0.00	111000

FOR LOADING - 3

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
4	2.77000E-02	0.00000E+00	-2.93000E-02	-1.73000E-02	0.00000E+00	-1.59000E-02
9	2.77000E-02	0.00000E+00	-2.93000E-02	-1.73000E-02	0.00000E+00	-1.59000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
 LOADTYPE WIND TITLE W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.574007281E+00
 Z = -0.200000006E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.590443686E+00
 Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 5.5399999E-02
 SUMMATION FORCE-Y = 0.0000000E+00
 SUMMATION FORCE-Z = -5.8600001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.03 MY= 0.48 MZ= -0.03

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -5.5399999E-02
 SUMMATION FORCE-Y = -2.0912092E-15
 SUMMATION FORCE-Z = 5.8600001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.00 MY= -0.48 MZ= 0.03

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)

MAXIMUMS AT NODE
 X = 8.99227E-04 28
 Y = -6.46038E-03 6
 Z = -1.97221E-03 11
 RX= 3.26410E-04 25
 RY= 2.16085E-05 7
 RZ= -6.07796E-05 4

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/	
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ	
							SUPPORT=1
15	0.00	0.00	0.00	0.00	0.00	0.00	
	0.06	-0.00	-0.13	-0.00	0.00	-0.00	111000
16	0.00	0.00	0.00	0.00	0.00	0.00	
	-0.04	0.00	0.10	-0.00	0.00	-0.00	111000

FOR LOADING - 7
 APPLIED JOINT EQUIVALENT LOADS
 JOINT FORCE-X FORCE-Y FORCE-Z MOM-X MOM-Y MOM-Z

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
2	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
4	2.10000E-02	0.00000E+00	-2.20000E-02	-1.30000E-02	0.00000E+00	-1.20000E-02
6	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
8	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02
9	2.10000E-02	0.00000E+00	-2.20000E-02	-1.30000E-02	0.00000E+00	-1.20000E-02
11	2.10000E-02	0.00000E+00	-3.90000E-02	-2.40000E-02	0.00000E+00	-1.30000E-02

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 7
LOADTYPE WIND TITLE 0.75W3

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.603174630E+00
Z = -0.200000006E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
Y = 0.609999991E+00
Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 7)

SUMMATION FORCE-X = 0.13
SUMMATION FORCE-Y = 0.00
SUMMATION FORCE-Z = -0.20

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.12 MY= 1.75 MZ= -0.08

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 7)

SUMMATION FORCE-X = -0.13
SUMMATION FORCE-Y = -0.00
SUMMATION FORCE-Z = 0.20

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.10 MY= -1.75 MZ= 0.08

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 7)

MAXIMUMS AT NODE

X = 2.86116E-03 29
Y = 1.79579E-01 2
Z = -3.93397E-02 6
RX= -1.39845E-02 8
RY= 1.25526E-04 25
RZ= -2.32052E-03 2

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/	
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ	
							SUPPORT=1
12	0.00	0.00	0.00	0.00	0.00	0.00	
	-0.11	0.01	-0.07	0.00	-0.00	0.00	111000
15	0.00	0.00	0.00	0.00	0.00	0.00	
	0.35	-0.01	-0.30	0.00	0.00	0.00	111000
16	0.00	0.00	0.00	0.00	0.00	0.00	
	-0.13	0.00	0.20	0.00	0.00	-0.00	111000

LOAD COMBINATION NO. 4
1.25DL

LOADING- 1.
FACTOR - 1.25

LOAD COMBINATION NO. 5
1.1DL+1.0W1

LOADING- 1. 2.
FACTOR - 1.10 1.00

LOAD COMBINATION NO. 6
1.1DL+1.0W2

LOADING- 1. 3.
FACTOR - 1.10 1.00

LOAD COMBINATION NO. 8
1.1DL+1.0W3

LOADING- 1. 7.
FACTOR - 1.10 1.00

***** END OF DATA FROM INTERNAL STORAGE *****

- 96. PARAMETER 1
- 97. CODE LRFD
- 98. CHECK CODE ALL

STAAD.Pro CODE CHECKING - (LRFD 3RD EDITION) v1.0

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE Noted)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
1	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.028	2
		0.06 T	0.12	-0.03	1.00
2	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.094	4
		0.00 C	-0.00	0.50	0.00
3	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.086	4
		0.05 C	0.00	0.45	0.50
4	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.094	4
		0.00 C	0.00	0.50	0.00
5	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.064	5
		0.03 C	0.15	0.19	2.00
6	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.067	5
		0.06 C	-0.13	0.22	2.00
7	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.027	5
		0.11 C	0.12	0.02	1.00
8	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.039	5
		1.06 C	-0.03	0.13	0.00
9	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.023	5
		0.77 C	-0.02	0.07	0.00
10	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.168	5
		0.21 C	-0.18	0.70	0.00
11	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.137	5
		0.25 T	-0.19	0.53	0.00
12	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.078	4
		0.00 C	-0.31	-0.11	0.00
13	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.019	4
		0.00 C	0.08	0.03	0.00
14	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.154	5
		0.26 T	-0.22	-0.59	0.00
15	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.100	8
		0.00 C	-0.37	0.16	0.00

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE NOTED)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
16	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.025	8
		0.00 C	0.09	-0.04	0.00
17	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.094	4
		0.00 C	0.00	0.50	7.00
18	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.162	5
		0.26 C	-0.18	0.66	7.00
19	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.086	4
		0.05 C	0.00	0.45	0.00
20	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.027	5
		0.77 C	-0.03	0.08	0.00
21	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.094	4
		0.00 C	-0.00	0.50	1.50
22	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.040	5
		1.09 C	-0.05	0.11	1.50
23	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.029	5
		0.11 T	0.12	0.03	0.00
24	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.033	5
		0.06 C	0.12	0.06	0.00
25	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS COMPRESS	0.000	4
		0.00 C	0.00	0.00	0.00
26	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS COMPRESS	0.000	4
		0.00 C	0.00	0.00	0.00
30	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.001	4
		0.00 C	0.00	0.00	0.00
31	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.001	4
		0.00 C	0.00	0.00	0.00

***** END OF TABULATED RESULT OF DESIGN *****

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE Noted)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					

99. PERFORM ANALYSIS PRINT STATICS CHECK

*WARNING- ZERO STIFFNESS IN DIRECTION 6 AT JOINT 28 EQN.NO. 48
 LOADS APPLIED OR DISTRIBUTED HERE FROM ELEMENTS WILL BE IGNORED.
 THIS MAY BE DUE TO ALL MEMBERS AT THIS JOINT BEING RELEASED OR
 EFFECTIVELY RELEASED IN THIS DIRECTION.

*WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 12 EQN.NO. 56
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 4 EQN.NO. 61
 *WARNING- ZERO STIFFNESS IN DIRECTION 4 AT JOINT 9 EQN.NO. 79
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 13 EQN.NO. 83
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 26 EQN.NO. 98
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 15 EQN.NO. 107
 *WARNING- ZERO STIFFNESS IN DIRECTION 6 AT JOINT 29 EQN.NO. 120
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 14 EQN.NO. 125
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 16 EQN.NO. 140
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 27 EQN.NO. 143
 *WARNING- ZERO STIFFNESS IN DIRECTION 5 AT JOINT 17 EQN.NO. 149

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
 LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.613718474E+00
 Z = -0.200000006E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.620689705E+00
 Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)
 SUMMATION FORCE-X = 0.11
 SUMMATION FORCE-Y = 0.00
 SUMMATION FORCE-Z = -0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.13 MY= 1.87 MZ= -0.07

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)
 SUMMATION FORCE-X = -0.11
 SUMMATION FORCE-Y = -0.00
 SUMMATION FORCE-Z = 0.21

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.13 MY= -1.87 MZ= 0.07

STAAD SPACE

-- PAGE NO. 16

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)
 MAXIMUMS AT NODE
 X = 3.06516E-03 29
 Y = 2.37086E-01 2
 Z = -5.05808E-02 6
 RX= -1.86232E-02 8
 RY= 1.49978E-04 25
 RZ= -3.07549E-03 2

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
 LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.113860572E+00
 Z = -0.203795358E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = -0.51
 SUMMATION FORCE-Z = 0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -1.04 MY= 0.00 MZ= -5.08

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
 SUMMATION FORCE-X = 0.00
 SUMMATION FORCE-Y = 0.51
 SUMMATION FORCE-Z = -0.00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 1.04 MY= 0.00 MZ= 5.08

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)
 MAXIMUMS AT NODE
 X = -1.68429E-04 10
 Y = -3.46242E-01 6
 Z = -4.86043E-03 11
 RX= 5.81508E-03 19
 RY= 7.43473E-06 29
 RZ= 4.14787E-03 2

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
 LOADTYPE WIND TITLE W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.574007281E+00
 Z = -0.200000006E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.590443686E+00
 Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 5.5399999E-02
 SUMMATION FORCE-Y = 0.0000000E+00
 SUMMATION FORCE-Z = -5.8600001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= -0.03 MY= 0.48 MZ= -0.03

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -5.5399999E-02
 SUMMATION FORCE-Y = -2.0912092E-15
 SUMMATION FORCE-Z = 5.8600001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
 MX= 0.00 MY= -0.48 MZ= 0.03

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)

MAXIMUMS	AT NODE
X = 8.99227E-04	28
Y = -6.46038E-03	6
Z = -1.97221E-03	11
RX= 3.26410E-04	25
RY= 2.16085E-05	7
RZ= -6.07796E-05	4

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 7
 LOADTYPE WIND TITLE 0.75W3

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.603174630E+00
 Z = -0.200000006E+01

STAAD SPACE

-- PAGE NO. 18

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
 (FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.100000003E+02
 Y = 0.609999991E+00
 Z = -0.200000006E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 7)

SUMMATION FORCE-X = 0.13
 SUMMATION FORCE-Y = 0.00
 SUMMATION FORCE-Z = -0.20

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= -0.12 MY= 1.75 MZ= -0.08

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 7)

SUMMATION FORCE-X = -0.13
 SUMMATION FORCE-Y = -0.00
 SUMMATION FORCE-Z = 0.20

SUMMATION OF MOMENTS AROUND THE ORIGIN-

MX= 0.10 MY= -1.75 MZ= 0.08

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 7)

MAXIMUMS AT NODE

X = 2.86116E-03 29
 Y = 1.79579E-01 2
 Z = -3.93397E-02 6
 RX= -1.39845E-02 8
 RY= 1.25526E-04 25
 RZ= -2.32052E-03 2

***** END OF DATA FROM INTERNAL STORAGE *****

100. FINISH

***** END OF THE STAAD.Pro RUN *****

**** DATE= JUL 19,2018 TIME= 13: 7:39 ****

```
*****
* For technical assistance on STAAD.Pro, please visit *
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Job No
148872000

Sheet No
1

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	05-Jun-18		

Project ID	
Project Name	

Structure Type | SPACE FRAME

Number of Nodes	28	Highest Node	29
Number of Elements	28	Highest Beam	31
Number of Plates	3	Highest Plate	34

Number of Basic Load Cases	4
Number of Combination Load Cases	4

Included in this printout are data for:

All	The Whole Structure
------------	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	2	W1
Primary	1	DL
Primary	3	W2
Primary	7	0.75W3
Combination	4	1.25DL
Combination	5	1.1DL+1.0W1
Combination	6	1.1DL+1.0W2
Combination	8	1.1DL+1.0W3

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	2	18	1.000	2	0
2	3	20	1.500	2	0
3	4	22	0.500	2	0
4	5	24	7.000	2	0
5	3	7	2.000	2	0
6	5	10	2.000	2	0
7	8	19	1.000	2	0
8	7	21	1.500	2	0
9	9	23	0.500	2	0
10	10	25	7.000	2	0
11	7	12	1.000	2	0



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Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
15	15	16	0.750	2	0
16	16	27	0.750	2	0
17	18	3	7.000	2	0
18	19	7	7.000	2	0
19	20	4	0.500	2	0
20	21	9	0.500	2	0
21	22	5	1.500	2	0
22	23	10	1.500	2	0
23	24	6	1.000	2	0
24	25	11	1.000	2	0
25	26	14	0.500	2	0
26	27	17	0.500	2	0
30	3	28	1.000	2	0
31	5	29	1.000	2	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
32	2	8	19	18	1
33	20	21	23	22	1
34	24	25	11	6	1

Materials

Mat	Name	E (kip/in ²)	ν	Density (kip/in ³)	α (/°F)
1	A500-GR.B	29E+3	0.300	0.000	6E-6
2	STEEL	29E+3	0.300	0.000	6E-6
3	STAINLESSSTEEL	28E+3	0.300	0.000	10E-6
4	ALUMINUM	10E+3	0.330	0.000	13E-6
5	CONCRETE	3.15E+3	0.170	0.000	5E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
12	Fixed	Fixed	Fixed	-	-	-
13	Fixed	Fixed	Fixed	-	-	-
15	Fixed	Fixed	Fixed	-	-	-
16	Fixed	Fixed	Fixed	-	-	-
26	Fixed	Fixed	Fixed	-	-	-
27	Fixed	Fixed	Fixed	-	-	-



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Primary Load Cases

Number	Name	Type
2	W1	Wind
1	DL	Dead
3	W2	Wind
7	0.75W3	Wind

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	1.25DL	1	DL	1.25
5	1.1DL+1.0W1	1	DL	1.10
		2	W1	1.00
6	1.1DL+1.0W2	1	DL	1.10
		3	W2	1.00
8	1.1DL+1.0W3	1	DL	1.10
		7	0.75W3	1.00

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	29	5:1.1DL+1.0W'	0.003	-0.039	-0.006	0.039	0.001	0.000	-0.000
Min X	11	5:1.1DL+1.0W'	-0.000	-0.362	-0.056	0.366	-0.011	0.000	-0.005
Max Y	2	2:W1	0.001	0.237	-0.043	0.241	-0.019	-0.000	-0.003
Min Y	2	4:1.25DL	0.000	-0.433	-0.006	0.433	0.007	-0.000	0.005
Max Z	2	3:W2	0.001	0.004	0.002	0.005	-0.000	0.000	-0.000
Min Z	6	5:1.1DL+1.0W'	0.002	-0.199	-0.056	0.207	-0.011	0.000	-0.002
Max rX	19	4:1.25DL	0.000	-0.208	-0.006	0.208	0.007	-0.000	0.004
Min rX	8	2:W1	0.001	-0.117	-0.043	0.125	-0.019	-0.000	0.002
Max rY	25	5:1.1DL+1.0W'	-0.000	-0.299	-0.055	0.304	-0.004	0.000	-0.005
Min rY	3	5:1.1DL+1.0W'	0.001	-0.020	-0.004	0.020	0.001	-0.000	0.001
Max rZ	2	4:1.25DL	0.000	-0.433	-0.006	0.433	0.007	-0.000	0.005
Min rZ	11	5:1.1DL+1.0W'	-0.000	-0.362	-0.056	0.366	-0.011	0.000	-0.005
Max Rst	2	4:1.25DL	0.000	-0.433	-0.006	0.433	0.007	-0.000	0.005



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Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Displacement Detail Summary

Displacements shown in italic indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	31	5:1.1DL+1.0W1	1.000	0.003	-0.039	-0.006	0.039
Min X	24	5:1.1DL+1.0W1	0.900	-0.001	-0.356	-0.056	0.360
Max Y	1	2:W1	0.000	0.001	0.237	-0.043	0.241
Min Y	1	4:1.25DL	0.000	0.000	-0.433	-0.006	0.433
Max Z	1	3:W2	0.000	0.001	0.004	0.002	0.005
Min Z	23	5:1.1DL+1.0W1	1.000	0.002	-0.199	-0.056	0.207
Max Rst	1	4:1.25DL	0.000	0.000	-0.433	-0.006	0.433

Beam End Displacement Summary

Displacements shown in italic indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	31	29	5:1.1DL+1.0W1	0.003	-0.039	-0.006	0.039
Min X	24	11	5:1.1DL+1.0W1	-0.001	-0.362	-0.056	0.366
Max Y	1	2	2:W1	0.001	0.237	-0.043	0.241
Min Y	1	2	4:1.25DL	0.000	-0.433	-0.006	0.433
Max Z	1	2	3:W2	0.001	0.004	0.002	0.005
Min Z	23	6	5:1.1DL+1.0W1	0.002	-0.199	-0.056	0.207
Max Rst	1	2	4:1.25DL	0.000	-0.433	-0.006	0.433

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for a beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	22	23	5:1.1DL+1.0W1	1.094	-0.019	-0.022	0.000	-0.195	0.891
Min Fx	21	22	2:W1	-0.400	-0.008	-0.010	0.000	-0.338	-2.777
Max Fy	11	7	5:1.1DL+1.0W1	-0.255	0.640	-0.077	-0.000	-2.248	6.385
Min Fy	14	10	5:1.1DL+1.0W1	-0.262	-0.751	-0.132	0.000	-2.652	-7.038
Max Fz	15	15	8:1.1DL+1.0W1	0.003	0.268	0.619	0.000	-4.455	1.930
Min Fz	24	25	2:W1	0.059	0.026	-0.183	0.000	1.432	0.346
Max Mx	24	25	5:1.1DL+1.0W1	0.059	0.057	-0.182	0.000	1.432	0.670
Min Mx	7	8	5:1.1DL+1.0W1	0.110	-0.049	0.183	-0.000	-0.778	-0.374
Max My	18	19	5:1.1DL+1.0W1	0.263	-0.067	-0.052	-0.000	2.207	0.226
Min My	14	15	8:1.1DL+1.0W1	-0.271	-0.696	-0.132	0.000	-4.455	1.930
Max Mz	10	10	5:1.1DL+1.0W1	0.207	0.117	0.052	0.000	-2.208	8.360
Min Mz	14	10	5:1.1DL+1.0W1	-0.262	-0.751	-0.132	0.000	-2.652	-7.038



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Job Title **Abutment Middle**

Part

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By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial			Shear			Torsion		Bending		
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)	Mx (kip'in)	My (kip'in)	Mz (kip'in)		
Max Fx	22	5:1.1DL+1.0W'	0.000	1.094	-0.019	-0.022	0.000	-0.195	0.891					
Min Fx	21	2:W1	0.000	-0.400	-0.008	-0.010	0.000	-0.338	-2.777					
Max Fy	11	5:1.1DL+1.0W'	0.000	-0.255	0.640	-0.077	-0.000	-2.248	6.385					
Min Fy	14	5:1.1DL+1.0W'	0.000	-0.262	-0.751	-0.132	0.000	-2.652	-7.038					
Max Fz	15	8:1.1DL+1.0W'	0.000	0.003	0.268	0.619	0.000	-4.455	1.930					
Min Fz	24	2:W1	0.000	0.059	0.026	-0.183	0.000	1.432	0.346					
Max Mx	24	5:1.1DL+1.0W'	0.000	0.059	0.057	-0.182	0.000	1.432	0.670					
Min Mx	7	5:1.1DL+1.0W'	0.000	0.110	-0.049	0.183	-0.000	-0.778	-0.374					
Max My	18	5:1.1DL+1.0W'	0.000	0.263	-0.067	-0.052	-0.000	2.207	0.226					
Min My	14	8:1.1DL+1.0W'	1.000	-0.271	-0.696	-0.132	0.000	-4.455	1.930					
Max Mz	10	5:1.1DL+1.0W'	0.000	0.207	0.117	0.052	0.000	-2.208	8.360					
Min Mz	14	5:1.1DL+1.0W'	0.000	-0.262	-0.751	-0.132	0.000	-2.652	-7.038					

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	2:W1	1.000	1.05E+3	1.000	2	-1.12E+3	1.000	4
	1:DL	1.000	160.776	1.000	3	-161.086	1.000	1
	3:W2	1.000	1.626	1.000	4	-1.565	1.000	2
	7:0.75W3	1.000	787.594	1.000	2	-834.897	1.000	4
	4:1.25DL	1.000	200.970	1.000	3	-201.358	1.000	1
	5:1.1DL+1.0W'	1.000	876.085	1.000	2	-940.197	1.000	1
	6:1.1DL+1.0W'	1.000	178.480	1.000	3	-178.759	1.000	1
	8:1.1DL+1.0W'	1.000	648.239	1.000	2	-695.884	1.000	1
2	2:W1	1.500	1.93E+3	1.500	1	-2.31E+3	1.500	3
	1:DL	1.500	2.94E+3	0.000	3	-2.94E+3	0.000	1
	3:W2	1.500	91.692	1.500	3	-86.137	1.500	1
	7:0.75W3	1.500	1.39E+3	0.000	1	-1.67E+3	0.000	3
	4:1.25DL	1.500	3.67E+3	0.000	3	-3.67E+3	0.000	1
	5:1.1DL+1.0W'	1.500	1.38E+3	1.500	4	-1.77E+3	1.500	2
	6:1.1DL+1.0W'	1.500	3.27E+3	0.000	3	-3.26E+3	0.000	1
	8:1.1DL+1.0W'	1.500	1.88E+3	0.000	3	-2.16E+3	0.000	1
3	2:W1	0.500	1.65E+3	0.000	1	-1.89E+3	0.000	3
	1:DL	0.500	2.68E+3	0.500	3	-2.64E+3	0.500	1
	3:W2	0.500	128.243	0.000	1	-108.643	0.000	4
	7:0.75W3	0.500	1.25E+3	0.500	2	-1.42E+3	0.500	4
	4:1.25DL	0.500	3.35E+3	0.500	3	-3.3E+3	0.500	1
	5:1.1DL+1.0W'	0.500	1.17E+3	0.500	3	-1.36E+3	0.500	1
	6:1.1DL+1.0W'	0.500	2.96E+3	0.500	3	-2.9E+3	0.500	1
	8:1.1DL+1.0W'	0.500	1.64E+3	0.500	3	-1.76E+3	0.500	1



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Job Title **Abutment Middle**

Part

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By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
4	2:W1	7.000	2.8E+3	0.000	1	-3.08E+3	0.000	3
	1:DL	7.000	2.94E+3	0.000	3	-2.94E+3	0.000	1
	3:W2	7.000	6.062	7.000	1	-5.352	7.000	3
	7:0.75W3	7.000	2.08E+3	0.000	1	-2.29E+3	0.000	3
	4:1.25DL	7.000	3.67E+3	0.000	3	-3.67E+3	0.000	1
	5:1.1DL+1.0W ₁	7.000	2.82E+3	0.000	3	-3.1E+3	0.000	1
	6:1.1DL+1.0W ₂	7.000	3.23E+3	0.000	3	-3.23E+3	0.000	1
	8:1.1DL+1.0W ₃	7.000	2.94E+3	0.000	3	-3.14E+3	0.000	1
5	2:W1	2.000	1.76E+3	2.000	2	-1.72E+3	2.000	4
	1:DL	2.000	1.81E+3	2.000	3	-1.81E+3	2.000	1
	3:W2	2.000	98.618	2.000	1	-90.611	2.000	3
	7:0.75W3	2.000	1.33E+3	2.000	2	-1.3E+3	2.000	4
	4:1.25DL	2.000	2.26E+3	2.000	3	-2.26E+3	2.000	1
	5:1.1DL+1.0W ₁	2.000	2.51E+3	2.000	3	-2.48E+3	2.000	1
	6:1.1DL+1.0W ₂	2.000	1.97E+3	2.000	3	-1.97E+3	2.000	1
	8:1.1DL+1.0W ₃	2.000	2.3E+3	2.000	3	-2.27E+3	2.000	1
6	2:W1	2.000	1.39E+3	2.000	1	-1.32E+3	2.000	3
	1:DL	2.000	1.81E+3	2.000	3	-1.81E+3	2.000	1
	3:W2	2.000	176.057	2.000	3	-153.567	2.000	1
	7:0.75W3	2.000	915.081	2.000	1	-848.599	2.000	3
	4:1.25DL	2.000	2.26E+3	2.000	3	-2.26E+3	2.000	1
	5:1.1DL+1.0W ₁	2.000	2.63E+3	2.000	4	-2.57E+3	2.000	2
	6:1.1DL+1.0W ₂	2.000	2.16E+3	2.000	3	-2.14E+3	2.000	1
	8:1.1DL+1.0W ₃	2.000	2.43E+3	2.000	4	-2.37E+3	2.000	2
7	2:W1	1.000	964.752	1.000	2	-847.752	1.000	1
	1:DL	1.000	179.603	1.000	3	-179.974	1.000	1
	3:W2	1.000	1.471	1.000	1	-1.592	1.000	3
	7:0.75W3	1.000	723.166	1.000	2	-635.542	1.000	1
	4:1.25DL	1.000	224.503	1.000	3	-224.967	1.000	1
	5:1.1DL+1.0W ₁	1.000	1.09E+3	1.000	3	-969.013	1.000	1
	6:1.1DL+1.0W ₂	1.000	198.106	1.000	3	-198.634	1.000	1
	8:1.1DL+1.0W ₃	1.000	857.234	1.000	3	-770.017	1.000	1
8	2:W1	1.500	903.879	1.500	4	-261.278	1.500	2
	1:DL	1.500	806.385	0.000	3	-372.389	0.000	1
	3:W2	1.500	89.999	1.500	3	-124.437	1.500	1
	7:0.75W3	1.500	692.976	0.000	1	-240.845	0.000	2
	4:1.25DL	1.500	1.01E+3	0.000	3	-465.487	0.000	1
	5:1.1DL+1.0W ₁	1.500	1.73E+3	0.000	3	-610.163	0.000	1
	6:1.1DL+1.0W ₂	1.500	974.857	0.000	3	-531.899	0.000	1
	8:1.1DL+1.0W ₃	1.500	1.58E+3	0.000	3	-650.473	0.000	1
9	2:W1	0.500	576.110	0.000	1	-124.477	0.000	2
	1:DL	0.500	467.898	0.500	4	-141.740	0.500	2
	3:W2	0.500	123.778	0.000	1	-115.078	0.000	4
	7:0.75W3	0.500	341.567	0.000	1			



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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	4:1.25DL	0.500	584.873	0.500	4	-177.175	0.500	2
	5:1.1DL+1.0W ₁	0.500	1.03E+3	0.000	1	-220.798	0.000	2
	6:1.1DL+1.0W ₂	0.500	430.391	0.500	3	-62.917	0.500	1
	8:1.1DL+1.0W ₃	0.500	796.663	0.000	1	-95.127	0.000	2
10	2:W1	7.000	3.3E+3	0.000	3	-3.08E+3	0.000	1
	1:DL	7.000	2.96E+3	0.000	3	-2.96E+3	0.000	1
	3:W2	7.000	5.576	0.000	1	-6.286	0.000	2
	7:0.75W3	7.000	2.46E+3	0.000	3	-2.3E+3	0.000	1
	4:1.25DL	7.000	3.7E+3	0.000	3	-3.7E+3	0.000	1
	5:1.1DL+1.0W ₁	7.000	6.55E+3	0.000	3	-6.33E+3	0.000	1
	6:1.1DL+1.0W ₂	7.000	3.26E+3	0.000	3	-3.26E+3	0.000	1
	8:1.1DL+1.0W ₃	7.000	5.71E+3	0.000	3	-5.55E+3	0.000	1
11	2:W1	1.000	1.87E+3	0.000	3	-1.86E+3	0.000	1
	1:DL	1.000	4.05E+3	0.000	3	-4.3E+3	0.000	1
	3:W2	1.000	190.471	1.000	4	-186.915	1.000	2
	7:0.75W3	1.000	1.38E+3	0.000	3	-1.37E+3	0.000	1
	4:1.25DL	1.000	5.06E+3	0.000	3	-5.37E+3	0.000	1
	5:1.1DL+1.0W ₁	1.000	5.13E+3	0.000	3	-5.4E+3	0.000	1
	6:1.1DL+1.0W ₂	1.000	4.33E+3	0.000	3	-4.6E+3	0.000	1
	8:1.1DL+1.0W ₃	1.000	4.86E+3	0.000	3	-5.12E+3	0.000	1
12	2:W1	0.750	134.805	0.000	1	-134.805	0.000	3
	1:DL	0.750	2.42E+3	0.000	1	-2.42E+3	0.000	2
	3:W2	0.750	188.693	0.000	3	-188.693	0.000	1
	7:0.75W3	0.750	44.078	0.000	3	-44.078	0.000	1
	4:1.25DL	0.750	3.02E+3	0.000	1	-3.02E+3	0.000	2
	5:1.1DL+1.0W ₁	0.750	2.72E+3	0.000	1	-2.72E+3	0.000	2
	6:1.1DL+1.0W ₂	0.750	2.58E+3	0.000	1	-2.58E+3	0.000	2
	8:1.1DL+1.0W ₃	0.750	2.64E+3	0.000	1	-2.64E+3	0.000	2
13	2:W1	0.750	33.701	0.000	3	-33.701	0.000	1
	1:DL	0.750	605.599	0.000	2	-603.047	0.000	1
	3:W2	0.750	47.173	0.000	1	-47.173	0.000	3
	7:0.75W3	0.750	11.020	0.000	1	-11.020	0.000	3
	4:1.25DL	0.750	756.999	0.000	2	-753.809	0.000	1
	5:1.1DL+1.0W ₁	0.750	681.865	0.000	2	-679.058	0.000	1
	6:1.1DL+1.0W ₂	0.750	646.730	0.000	2	-643.922	0.000	1
	8:1.1DL+1.0W ₃	0.750	661.363	0.000	2	-658.556	0.000	1
14	2:W1	1.000	2.02E+3	0.000	1	-2.02E+3	0.000	3
	1:DL	1.000	4.05E+3	0.000	1	-4.3E+3	0.000	3
	3:W2	1.000	509.331	1.000	4	-512.887	1.000	2
	7:0.75W3	1.000	1.5E+3	0.000	1	-1.51E+3	0.000	3
	4:1.25DL	1.000	5.06E+3	0.000	1	-5.37E+3	0.000	3
	5:1.1DL+1.0W ₁	1.000	5.77E+3	0.000	1	-6.05E+3	0.000	3
	6:1.1DL+1.0W ₂	1.000	4.58E+3	0.000	1	-4.86E+3	0.000	3
	8:1.1DL+1.0W ₃	1.000	5.53E+3	0.000	1	-5.81E+3	0.000	3



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File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
15	2:W1	0.750	1.13E+3	0.000	1	-1.13E+3	0.000	2
	1:DL	0.750	2.42E+3	0.000	1	-2.42E+3	0.000	2
	3:W2	0.750	511.109	0.000	1	-511.109	0.000	2
	7:0.75W3	0.750	1.23E+3	0.000	1	-1.23E+3	0.000	2
	4:1.25DL	0.750	3.02E+3	0.000	1	-3.02E+3	0.000	2
	5:1.1DL+1.0W ₁	0.750	3.79E+3	0.000	1	-3.78E+3	0.000	2
	6:1.1DL+1.0W ₂	0.750	3.17E+3	0.000	1	-3.17E+3	0.000	2
	8:1.1DL+1.0W ₃	0.750	3.9E+3	0.000	1	-3.89E+3	0.000	2
16	2:W1	0.750	281.823	0.000	2	-281.823	0.000	1
	1:DL	0.750	605.599	0.000	2	-603.047	0.000	1
	3:W2	0.750	127.777	0.000	2	-127.777	0.000	1
	7:0.75W3	0.750	308.700	0.000	2	-308.700	0.000	1
	4:1.25DL	0.750	756.999	0.000	2	-753.809	0.000	1
	5:1.1DL+1.0W ₁	0.750	947.983	0.000	2	-945.175	0.000	1
	6:1.1DL+1.0W ₂	0.750	793.937	0.000	2	-791.129	0.000	1
	8:1.1DL+1.0W ₃	0.750	974.859	0.000	2	-972.052	0.000	1
17	2:W1	7.000	3.07E+3	7.000	1	-3.29E+3	7.000	3
	1:DL	7.000	2.94E+3	7.000	3	-2.94E+3	7.000	1
	3:W2	7.000	2.401	0.000	1	-2.156	0.000	2
	7:0.75W3	7.000	2.28E+3	7.000	1	-2.45E+3	7.000	3
	4:1.25DL	7.000	3.67E+3	7.000	3	-3.67E+3	7.000	1
	5:1.1DL+1.0W ₁	7.000	2.59E+3	7.000	4	-2.81E+3	7.000	2
	6:1.1DL+1.0W ₂	7.000	3.23E+3	7.000	3	-3.23E+3	7.000	1
	8:1.1DL+1.0W ₃	7.000	2.76E+3	7.000	4	-2.93E+3	7.000	2
18	2:W1	7.000	3.07E+3	7.000	4	-2.8E+3	7.000	2
	1:DL	7.000	2.96E+3	7.000	3	-2.96E+3	7.000	1
	3:W2	7.000	2.257	7.000	1	-2.501	7.000	3
	7:0.75W3	7.000	2.28E+3	7.000	4	-2.08E+3	7.000	2
	4:1.25DL	7.000	3.7E+3	7.000	3	-3.7E+3	7.000	1
	5:1.1DL+1.0W ₁	7.000	6.33E+3	7.000	4	-6.05E+3	7.000	2
	6:1.1DL+1.0W ₂	7.000	3.25E+3	7.000	3	-3.25E+3	7.000	1
	8:1.1DL+1.0W ₃	7.000	5.54E+3	7.000	4	-5.33E+3	7.000	2
19	2:W1	0.500	1.76E+3	0.000	1	-2E+3	0.000	3
	1:DL	0.500	2.68E+3	0.000	3	-2.64E+3	0.000	1
	3:W2	0.500	113.584	0.500	3	-123.297	0.500	1
	7:0.75W3	0.500	1.3E+3	0.000	1	-1.48E+3	0.000	3
	4:1.25DL	0.500	3.35E+3	0.000	3	-3.3E+3	0.000	1
	5:1.1DL+1.0W ₁	0.500	1.16E+3	0.000	3	-1.35E+3	0.000	1
	6:1.1DL+1.0W ₂	0.500	3.01E+3	0.500	3	-2.97E+3	0.500	1
	8:1.1DL+1.0W ₃	0.500	1.66E+3	0.000	3	-1.8E+3	0.000	1
20	2:W1	0.500	673.976	0.000	1	-222.343	0.000	2
	1:DL	0.500	467.898	0.000	3	-141.740	0.000	1
	3:W2	0.500	107.802	0.500	3	-128.414	0.500	1
	7:0.75W3	0.500	564.360	0.000	1	-243.820	0.000	2



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File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
	4:1.25DL	0.500	584.873	0.000	3	-177.175	0.000	1
	5:1.1DL+1.0W ₁	0.500	1.19E+3	0.000	1	-378.256	0.000	2
	6:1.1DL+1.0W ₂	0.500	596.751	0.000	3	-258.589	0.000	1
	8:1.1DL+1.0W ₃	0.500	1.08E+3	0.000	3	-399.734	0.000	1
21	2:W1	1.500	1.71E+3	1.500	1	-2.13E+3	1.500	3
	1:DL	1.500	2.94E+3	1.500	3	-2.94E+3	1.500	1
	3:W2	1.500	175.035	0.000	2	-158.921	0.000	1
	7:0.75W3	1.500	1.35E+3	1.500	1	-1.66E+3	1.500	3
	4:1.25DL	1.500	3.67E+3	1.500	3	-3.67E+3	1.500	1
	5:1.1DL+1.0W ₁	1.500	1.74E+3	1.500	4	-2.16E+3	1.500	2
	6:1.1DL+1.0W ₂	1.500	3.35E+3	1.500	4	-3.33E+3	1.500	2
	8:1.1DL+1.0W ₃	1.500	2.22E+3	1.500	4	-2.52E+3	1.500	2
22	2:W1	1.500	861.628	1.500	4	-181.519	1.500	2
	1:DL	1.500	806.385	1.500	4	-372.389	1.500	2
	3:W2	1.500	195.310	0.000	2	-181.682	0.000	1
	7:0.75W3	1.500	680.939	1.500	4	-163.933	1.500	2
	4:1.25DL	1.500	1.01E+3	1.500	4	-465.487	1.500	2
	5:1.1DL+1.0W ₁	1.500	1.75E+3	1.500	4	-591.148	1.500	2
	6:1.1DL+1.0W ₂	1.500	939.182	1.500	4	-448.158	1.500	2
	8:1.1DL+1.0W ₃	1.500	1.57E+3	1.500	4	-573.561	1.500	2
23	2:W1	1.000	840.439	0.000	2	-957.853	0.000	1
	1:DL	1.000	160.776	0.000	3	-161.086	0.000	1
	3:W2	1.000	3.832	0.000	1	-3.640	0.000	2
	7:0.75W3	1.000	627.663	0.000	2	-715.535	0.000	1
	4:1.25DL	1.000	200.970	0.000	3	-201.358	0.000	1
	5:1.1DL+1.0W ₁	1.000	1.02E+3	0.000	2	-1.13E+3	0.000	1
	6:1.1DL+1.0W ₂	1.000	179.747	0.000	3	-179.895	0.000	1
	8:1.1DL+1.0W ₃	1.000	802.905	0.000	2	-891.118	0.000	1
24	2:W1	1.000	1.12E+3	0.000	2	-1.05E+3	0.000	1
	1:DL	1.000	179.603	0.000	3	-179.974	0.000	1
	3:W2	1.000	3.411	0.000	1	-3.748	0.000	2
	7:0.75W3	1.000	832.632	0.000	2	-786.365	0.000	1
	4:1.25DL	1.000	224.503	0.000	3	-224.967	0.000	1
	5:1.1DL+1.0W ₁	1.000	1.31E+3	0.000	2	-1.25E+3	0.000	1
	6:1.1DL+1.0W ₂	1.000	200.974	0.000	3	-201.719	0.000	1
	8:1.1DL+1.0W ₃	1.000	1.03E+3	0.000	2	-984.330	0.000	1
25	2:W1	0.500	0.000	0.000	3	-0.000	0.000	1
	1:DL	0.500	1.701	0.000	1	-0.000	0.500	3
	3:W2	0.500	0.000	0.000	3	-0.000	0.000	1
	7:0.75W3	0.500	0.000	0.000	3	-0.000	0.000	1
	4:1.25DL	0.500	2.127	0.000	1	-0.000	0.500	3
	5:1.1DL+1.0W ₁	0.500	1.872	0.000	1	-0.000	0.500	3
	6:1.1DL+1.0W ₂	0.500	1.872	0.000	1	-0.000	0.500	3
	8:1.1DL+1.0W ₃	0.500	1.872	0.000	1	-0.000	0.500	3



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Beam Combined Axial and Bending Stresses Summary Cont...

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
26	2:W1	0.500	0.000	0.458	3	-0.000	0.458	1
	1:DL	0.500	1.701	0.000	1	-0.000	0.500	2
	3:W2	0.500	0.000	0.500	2	-0.000	0.500	4
	7:0.75W3	0.500	0.000	0.500	3	-0.000	0.500	1
	4:1.25DL	0.500	2.127	0.000	1	-0.000	0.500	2
	5:1.1DL+1.0W ₁ '	0.500	1.872	0.000	1	-0.000	0.500	2
	6:1.1DL+1.0W ₂ '	0.500	1.872	0.000	1	-0.000	0.500	2
	8:1.1DL+1.0W ₃ '	0.500	1.872	0.000	1	-0.000	0.500	2
30	2:W1	1.000	0.000	0.000	1	-0.000	0.000	3
	1:DL	1.000	23.529	0.000	3	-23.529	0.000	1
	3:W2	1.000	0.000	0.000	1	-0.000	0.000	2
	7:0.75W3	1.000	0.000	0.917	4	-0.000	0.917	2
	4:1.25DL	1.000	29.411	0.000	3	-29.411	0.000	1
	5:1.1DL+1.0W ₁ '	1.000	25.882	0.000	3	-25.882	0.000	1
	6:1.1DL+1.0W ₂ '	1.000	25.882	0.000	3	-25.882	0.000	1
	8:1.1DL+1.0W ₃ '	1.000	25.882	0.000	3	-25.882	0.000	1
31	2:W1	1.000	0.000	1.000	1	-0.000	1.000	2
	1:DL	1.000	23.529	0.000	3	-23.529	0.000	1
	3:W2	1.000	0.000	0.917	1	-0.000	0.917	3
	7:0.75W3	1.000	0.000	1.000	1	-0.000	1.000	2
	4:1.25DL	1.000	29.411	0.000	3	-29.411	0.000	1
	5:1.1DL+1.0W ₁ '	1.000	25.882	0.000	3	-25.882	0.000	1
	6:1.1DL+1.0W ₂ '	1.000	25.882	0.000	3	-25.882	0.000	1
	8:1.1DL+1.0W ₃ '	1.000	25.882	0.000	3	-25.882	0.000	1

Plate Center Stress Summary

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Max Qx	32	3:W2	0.000	0.000	-0.003	-0.009	0.077	0.000	0.000	0.030
Min Qx	32	2:W1	-10.800	0.000	-0.044	-0.850	-78.517	0.000	0.107	11.817
Max Qy	34	4:1.25DL	-0.000	0.006	-0.042	-0.134	-0.032	-0.000	-0.088	0.799
Min Qy	32	4:1.25DL	-0.000	-0.006	-0.042	-0.134	0.032	-0.000	-0.088	-0.799
Max Sx	32	3:W2	0.000	0.000	-0.003	-0.009	0.077	0.000	0.000	0.030
Min Sx	33	5:1.1DL+1.0W ₁ '	-0.000	-0.000	-5.564	-18.260	-11.815	-0.000	-0.727	0.044
Max Sy	34	2:W1	-10.800	-0.000	-0.026	0.610	78.225	0.000	-0.107	-11.680
Min Sy	33	5:1.1DL+1.0W ₁ '	-0.000	-0.000	-5.564	-18.260	-11.815	-0.000	-0.727	0.044
Max Sxy	34	2:W1	-10.800	-0.000	-0.026	0.610	78.225	0.000	-0.107	-11.680
Min Sxy	32	2:W1	-10.800	0.000	-0.044	-0.850	-78.517	0.000	0.107	11.817
Max Mx	33	2:W1	-0.000	-0.000	-2.284	-6.867	-11.815	0.000	0.633	0.044
Min Mx	33	4:1.25DL	-0.000	0.000	-3.728	-12.947	0.000	-0.000	-1.545	-0.000
Max My	33	2:W1	-0.000	-0.000	-2.284	-6.867	-11.815	0.000	0.633	0.044



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Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Plate Center Stress Summary Cont...

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Min My	33	4:1.25DL	-0.000	0.000	-3.728	-12.947	0.000	-0.000	-1.545	-0.000
Max Mxy	32	2:W1	-10.800	0.000	-0.044	-0.850	-78.517	0.000	0.107	11.817
Min Mxy	34	2:W1	-10.800	-0.000	-0.026	0.610	78.225	0.000	-0.107	-11.680

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	12	5:1.1DL+1.0W1	0.820	0.265	0.517	0.000	0.000	0.000
Min FX	15	5:1.1DL+1.0W1	-1.025	0.272	0.721	0.000	0.000	0.000
Max FY	12	4:1.25DL	0.694	0.305	0.509	0.000	0.000	0.000
Min FY	12	7:0.75W3	0.110	-0.005	0.071	0.000	0.000	0.000
Max FZ	15	8:1.1DL+1.0W3	-0.964	0.273	0.750	0.000	0.000	0.000
Min FZ	16	8:1.1DL+1.0W3	0.322	0.005	-0.743	0.000	0.000	0.000
Max MX	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000
Min MX	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000
Max MY	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000
Min MY	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000
Max MZ	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000
Min MZ	12	2:W1	0.209	-0.003	0.069	0.000	0.000	0.000



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Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 1 Check 1

```

*****
MEMBER 1 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH
KL/R-Y= 10.52
KL/R-Z= 10.52
UNL = 12.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.1 0.0 0.2 0.1 0.0
LOCATION 0.0 1.0 0.0 1.0 1.0
LOADING 5 4 2 2 2
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.028 2
0.06 T 0.12 -0.03 1.00
*****
1 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Ref

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 2 Check 1

```

*****
MEMBER 2 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FEET)
IN KIP INCH | L4
*****
KL/R-Y= 15.78 |
KL/R-Z= 15.78 |
UNL = 18.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.4
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.4 0.0 0.0 0.1 0.5
LOCATION 0.0 0.0 0.0 1.5 0.0
LOADING 2 4 5 5 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.094 4
0.00 C -0.00 0.50 0.00
*****
2 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Ref

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 3 Check 1

```

*****
MEMBER 3 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
0.4 (KIP-FEET)
PARAMETER
IN KIP INCH
-----
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
-----
L4 L4 L4
L4 L4
L4
L4 L4
L4
-----
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
-----
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.0 0.0 0.0 0.4
LOCATION 0.0 0.5 0.0 0.0 0.5
LOADING 2 8 2 6 4
-----
*****
*
* DESIGN SUMMARY (KIP-FEET)
*
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.086 4
0.05 C 0.00 0.45 0.50
*
*****
3 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 4 Check 1

```

*****
MEMBER 4 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER 0.5 (KIP-FEET)
IN KIP INCH | L4
+ L4
+ L4
+ L4
+ L4
+ L4 L4
+ L4 L5
+ 0.0
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.3 0.1 0.1 0.2 0.5
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 4 2 2 4

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.094 4
0.00 C 0.00 0.50 0.00
*****
4 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 5 Check 1

```

*****
MEMBER 5 *
DESIGN CODE *
LRFD 2001 *
*****

|<---LENGTH (FT)= 2.00 --->|

*****
PROPERTY IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER          0.3 (KIP-FEET)
IN KIP  INCH      L4  L4  L4  L4  CAPACITIES
IN KIP  INCH     IN KIP  INCH
KL/R-Y= 21.04 |         L4         PNC=0.5650E+2
KL/R-Z= 21.04 +         L4         pnc=0.2987E-1
UNL   = 24.00 |         L4  L4     PNT=0.6124E+2
CB    = 1.00 +         L4         pnt=0.0000E+0
PHIC  = 0.00 |         L4         MNZ=0.6383E+2
PHIB  = 0.90 +  L4  L4         mnz=0.2248E+1
FYLD  = 36.00 |L4         MNY=0.6383E+2
NSF   = 1.00 +-----|         mny=0.1843E+1
DFE   = 0.00 -0.0          VN =0.2030E+2
dff   = 0.00          vN =0.9899E-1

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
          AXIAL      SHEAR-Y      SHEAR-Z      MOMENT-Y      MOMENT-Z
VALUE      0.0        0.2         0.2         0.2         0.3
LOCATION     0.0        2.0         0.0         0.0         2.0
LOADING    2          4          2          2          4

*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/    CRITICAL COND/    RATIO/    LOADING/
FX          MY               MZ        LOCATION
-----
PASS       HSS FLEX+AXL           0.064     5
0.03 C    0.15                  0.19     2.00

*****
5 ST  HSST3X3X0.188          (AISC SECTIONS)

```




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Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

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Steel Design (Track 2) Beam 6 Check 1

```

*****
MEMBER 6 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 2.00 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
PARAMETER 0.3 (KIP-FEET)
IN KIP INCH
-----
KL/R-Y= 21.04 |
KL/R-Z= 21.04 +
UNL = 24.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
-----
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
-----
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.2 0.1 0.1 0.3
LOCATION 0.0 2.0 0.0 0.0 2.0
LOADING 7 4 2 2 4
-----
*****
*
* DESIGN SUMMARY (KIP-FEET)
*
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
-----
PASS HSS FLEX+AXL 0.067 5
0.06 C -0.13 0.22 2.00
*
*****
6 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 7 Check 1

```

*****
MEMBER 7 *
DESIGN CODE *
LRFD 2001 *
*****

|<---LENGTH (FT)= 1.00 --->|

Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER 0.0 (KIP-FOOT)
IN KIP INCH |L5
+ L2 L4
KL/R-Y= 10.52 |
KL/R-Z= 10.52 + L2 L4
UNL = 12.00 |
CB = 1.00 + L2 L4
PHIC = 0.00 |
PHIB = 0.90 + L4
FYLD = 36.00 |
NSF = 1.00 +-----+-----+-----+-----+-----+
DFE = 0.00 0.0
dff = 0.00

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.2 0.1 0.0
LOCATION 0.0 1.0 0.0 1.0 0.0
LOADING 2 5 2 2 5

*****
*
* DESIGN SUMMARY (KIP-FOOT)
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.027 5
0.11 C 0.12 0.02 1.00
*
*****
7 ST HSST3X3X0.188 (AISC SECTIONS)

```



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3

Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 8 Check 1

```

*****
MEMBER 8 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH | L5
CAPACITIES
IN KIP INCH
-----
KL/R-Y= 15.78 |
KL/R-Z= 15.78 |
UNL = 18.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.1
dff = 0.00
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 1.1 0.0 0.0 0.0 0.1
LOCATION 0.0 0.0 0.0 1.5 0.0
LOADING 5 5 6 2 5
*****
DESIGN SUMMARY (KIP-FEET)
-----
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.039 5
1.06 C -0.03 0.13 0.00
*****
8 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 9 Check 1

```

*****
MEMBER 9 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.8 0.0 0.0 0.0 0.1
LOCATION 0.0 0.5 0.0 0.0 0.5
LOADING 5 4 2 5 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.023 5
0.77 C -0.02 0.07 0.00
*****
9 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job Title **Abutment Middle**

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Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 10 Check 1

```

*****
MEMBER 10 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FEET)
IN KIP INCH | L5
*****
KL/R-Y= 73.63 |
KL/R-Z= 73.63 +
UNL = 84.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.0
dfe = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.2 0.1 0.1 0.2 0.7
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 5 5 5 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.168 5
0.21 C -0.18 0.70 0.00
*****
10 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
22

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 11 Check 1

```

*****
MEMBER 11 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FEET)
IN KIP INCH | L5
*****
KL/R-Y= 10.52 |
KL/R-Z= 10.52 +
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.3 0.6 0.1 0.3 0.5
LOCATION 1.0 0.0 0.0 0.0 0.0
LOADING 4 5 2 4 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.137 5
0.25 T -0.19 0.53 0.00
*****
11 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
23

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 12 Check 1

```

*****
MEMBER 12 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.75 --->|
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1

PARAMETER 0.1 (KIP-FEET)
IN KIP INCH L5
CAPACITIES
IN KIP INCH
KL/R-Y= 7.89
KL/R-Z= 7.89
UNL = 9.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE LOCATION LOADING
0.0 0.0 4
0.2 0.0 5
0.5 0.0 4
0.3 0.0 4
0.1 0.0 5

*****
DESIGN SUMMARY (KIP-FEET)
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
PASS HSS FLEX+AXL 0.078 4
0.00 C -0.31 -0.11 0.00
*****
12 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 13 Check 1

```

*****
MEMBER 13 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.75 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH |L5
*****
KL/R-Y= 7.89 |
KL/R-Z= 7.89 +
UNL = 9.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.1 0.1 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 4 5 4 4 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.019 4
0.00 C 0.08 0.03 0.00
*****
13 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 14 Check 1

```

*****
MEMBER 14 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.6 (KIP-FEET)
IN KIP INCH | L5
*****
KL/R-Y= 10.52 |
KL/R-Z= 10.52 |
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 |
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.3 0.8 0.1 0.4 0.6
LOCATION 1.0 0.0 0.0 1.0 0.0
LOADING 4 5 2 8 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.154 5
0.26 T -0.22 -0.59 0.00
*****
14 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 15 Check 1

```

*****
MEMBER 15 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.75 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.2 (KIP-FEET)
IN KIP INCH L5
*****
KL/R-Y= 7.89
KL/R-Z= 7.89
UNL = 9.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.3 0.6 0.4 0.2
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 4 5 8 8 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.100 8
0.00 C -0.37 0.16 0.00
*****
15 ST HSST3X3X0.188 (AISC SECTIONS)

```



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148872000

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Rev
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Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 16 Check 1

```

*****
MEMBER 16 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.75 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH |L5
*****
KL/R-Y= 7.89 |
KL/R-Z= 7.89 +
UNL = 9.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.1 0.1 0.1 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 4 5 8 8 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.025 8
0.00 C 0.09 -0.04 0.00
*****
16 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 17 Check 1

```

*****
MEMBER 17 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.5 (KIP-FEET)
IN KIP INCH
KL/R-Y= 73.63
KL/R-Z= 73.63
UNL = 84.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.1 0.1 0.2 0.5
LOCATION 0.0 7.0 0.0 0.0 7.0
LOADING 2 4 2 2 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.094 4
0.00 C 0.00 0.50 7.00
*****
17 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 18 Check 1

```

*****
MEMBER 18 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 7.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.7 (KIP-FOOT)
IN KIP INCH
KL/R-Y= 73.63
KL/R-Z= 73.63
UNL = 84.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FOOT)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.3 0.1 0.1 0.2 0.7
LOCATION 0.0 7.0 0.0 0.0 7.0
LOADING 2 5 5 5 5
*****
DESIGN SUMMARY (KIP-FOOT)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.162 5
0.26 C -0.18 0.66 7.00
*****
18 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

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Rev
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Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 19 Check 1

```

*****
MEMBER 19 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.4 (KIP-FEET)
IN KIP INCH | L4
*****
KL/R-Y= 5.26 |
KL/R-Z= 5.26 |
UNL = 6.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 0.4
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.2 0.0 0.0 0.0 0.4
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 4 7 2 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.086 4
0.05 C 0.00 0.45 0.00
*****
19 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 20 Check 1

```

*****
MEMBER 20 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH L5
*****
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.8 0.0 0.0 0.0 0.1
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 5 5 7 5 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.027 5
0.77 C -0.03 0.08 0.00
*****
20 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
32

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 21 Check 1

```

*****
MEMBER 21 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

PARAMETER	0.5 (KIP-FEET)				
KL/R-Y=	15.78				
KL/R-Z=	15.78				
UNL =	18.00				
CB =	1.00				
PHIC =	0.00				
PHIB =	0.90				
FYLD =	36.00				
NSF =	1.00				
DFE =	0.00				
dff =	0.00				

```

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----

```

	AXIAL	SHEAR-Y	SHEAR-Z	MOMENT-Y	MOMENT-Z
VALUE	-0.4	0.0	0.0	0.0	0.5
LOCATION	0.0	1.5	0.0	1.5	1.5
LOADING	2	8	7	8	4

```

*****
DESIGN SUMMARY (KIP-FEET)
-----

```

RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
PASS 0.00 C	HSS FLEX+AXL -0.00	0.094 0.50	4 1.50

```

*****
21 ST HSST3X3X0.188 (AISC SECTIONS)

```




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Job No
148872000

Sheet No
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Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 22 Check 1

```

*****
MEMBER 22 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH
KL/R-Y= 15.78
KL/R-Z= 15.78
UNL = 18.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 1.1 0.0 0.0 0.0 0.1
LOCATION 0.0 1.5 0.0 1.5 1.5
LOADING 5 4 8 8 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.040 5
1.09 C -0.05 0.11 1.50
*****
22 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
34

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 23 Check 1

```

*****
MEMBER 23 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH
KL/R-Y= 10.52
KL/R-Z= 10.52
UNL = 12.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE -0.1 0.0 0.2 0.1 0.0
LOCATION 0.0 0.0 0.0 0.0 1.0
LOADING 5 4 2 2 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.029 5
0.11 T 0.12 0.03 0.00
*****
23 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
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Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 24 Check 1

```

*****
MEMBER 24 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.1 (KIP-FEET)
IN KIP INCH | L5
*****
KL/R-Y= 10.52 |
KL/R-Z= 10.52 |
UNL = 12.00 |
CB = 1.00 +
PHIC = 0.00 |
PHIB = 0.90 +
FYLD = 36.00 |
NSF = 1.00 +
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.1 0.1 0.2 0.1 0.1
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 2 5 2 2 5
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS FLEX+AXL 0.033 5
0.06 C 0.12 0.06 0.00
*****
24 ST HSST3X3X0.188 (AISC SECTIONS)

```



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
36

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 25 Check 1

```

*****
MEMBER 25 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
0.0 (KIP-FEET)
PARAMETER |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 CAPACITIES
IN KIP INCH |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 IN KIP INCH
-----
KL/R-Y= 5.26 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 PNC=0.5775E+2
KL/R-Z= 5.26 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 pnc=0.4020E-2
UNL = 6.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 PNT=0.6124E+2
CB = 1.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 pnt=0.0000E+0
PHIC = 0.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 MNZ=0.6383E+2
PHIB = 0.90 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 mnz=0.0000E+0
FYLD = 36.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 MNY=0.6383E+2
NSF = 1.00 |-----| mny=0.0000E+0
DFE = 0.00 0.0 VN =0.2030E+2
dff = 0.00 vn =0.0000E+0
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.0 0.0 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 4 0 0 0 0
*****
*
* DESIGN SUMMARY (KIP-FEET)
*
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS COMPRESS 0.000 4
0.00 C 0.00 0.00 0.00
*
*****
25 ST HSST3X3X0.188 (AISC SECTIONS)

```



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
37

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 26 Check 1

```

*****
MEMBER 26 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
Y
|
PROPERTIES
IN INCH UNIT
-----
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
-----
0.0 (KIP-FEET)
PARAMETER |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 CAPACITIES
IN KIP INCH |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 IN KIP INCH
-----
KL/R-Y= 5.26 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 PNC=0.5775E+2
KL/R-Z= 5.26 +L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 pnc=0.4020E-2
UNL = 6.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 PNT=0.6124E+2
CB = 1.00 +L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 pnt=0.0000E+0
PHIC = 0.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 MNZ=0.6383E+2
PHIB = 0.90 +L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 mnz=0.0000E+0
FYLD = 36.00 |L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 L0 MNY=0.6383E+2
NSF = 1.00 +-----+-----+-----+-----+-----+-----+-----+-----+-----+-----+
DFE = 0.00 0.0 VN =0.2030E+2
dff = 0.00 vn =0.0000E+0
-----
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
-----
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
-----
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.0 0.0 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 4 0 0 0 0
*****
*
* DESIGN SUMMARY (KIP-FEET)
*
*
* RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS COMPRESS 0.000 4
0.00 C 0.00 0.00 0.00
*
*****
26 ST HSST3X3X0.188 (AISC SECTIONS)

```



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
38

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 30 Check 1

```

*****
MEMBER 30 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH | L4
*****
KL/R-Y= 10.52 | L4
KL/R-Z= 10.52 + L4
UNL = 12.00 | L4
CB = 1.00 +
PHIC = 0.00 | L4 L4
PHIB = 0.90 + L4
FYLD = 36.00 | L4 L4 L0
NSF = 1.00 +-----+
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.0 0.0 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 0 4 0 0 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS BEND Z 0.001 4
0.00 C 0.00 0.00 0.00
*****
30 ST HSST3X3X0.188 (AISC SECTIONS)

```



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CONNECTED User: Ivonne Rios

Job No
148872000

Sheet No
39

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Steel Design (Track 2) Beam 31 Check 1

```

*****
MEMBER 31 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.00 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH | L4
*****
KL/R-Y= 10.52 | L4
KL/R-Z= 10.52 + L4
UNL = 12.00 | L4
CB = 1.00 +
PHIC = 0.00 | L4 L4
PHIB = 0.90 + L4
FYLD = 36.00 | L4 L4 L0
NSF = 1.00 +-----+-----+-----+-----+-----+-----+
DFE = 0.00 -0.0
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
*****
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.0 0.0 0.0
LOCATION 0.0 0.0 0.0 0.0 0.0
LOADING 0 4 0 0 4
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
*****
PASS HSS BEND Z 0.001 4
0.00 C 0.00 0.00 0.00
*****
31 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
40

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.028	1.000	0.028	HSS FLEX+A	2	1.890	2.460	2.460	4.030
2	HSST3X3X0	HSST3X3X0	0.094	1.000	0.094	HSS FLEX+A	4	1.890	2.460	2.460	4.030
3	HSST3X3X0	HSST3X3X0	0.086	1.000	0.086	HSS FLEX+A	4	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.094	1.000	0.094	HSS FLEX+A	4	1.890	2.460	2.460	4.030
5	HSST3X3X0	HSST3X3X0	0.064	1.000	0.064	HSS FLEX+A	5	1.890	2.460	2.460	4.030
6	HSST3X3X0	HSST3X3X0	0.067	1.000	0.067	HSS FLEX+A	5	1.890	2.460	2.460	4.030
7	HSST3X3X0	HSST3X3X0	0.027	1.000	0.027	HSS FLEX+A	5	1.890	2.460	2.460	4.030
8	HSST3X3X0	HSST3X3X0	0.039	1.000	0.039	HSS FLEX+A	5	1.890	2.460	2.460	4.030
9	HSST3X3X0	HSST3X3X0	0.023	1.000	0.023	HSS FLEX+A	5	1.890	2.460	2.460	4.030
10	HSST3X3X0	HSST3X3X0	0.168	1.000	0.168	HSS FLEX+A	5	1.890	2.460	2.460	4.030
11	HSST3X3X0	HSST3X3X0	0.137	1.000	0.137	HSS FLEX+A	5	1.890	2.460	2.460	4.030
12	HSST3X3X0	HSST3X3X0	0.078	1.000	0.078	HSS FLEX+A	4	1.890	2.460	2.460	4.030
13	HSST3X3X0	HSST3X3X0	0.019	1.000	0.019	HSS FLEX+A	4	1.890	2.460	2.460	4.030
14	HSST3X3X0	HSST3X3X0	0.154	1.000	0.154	HSS FLEX+A	5	1.890	2.460	2.460	4.030
15	HSST3X3X0	HSST3X3X0	0.100	1.000	0.100	HSS FLEX+A	8	1.890	2.460	2.460	4.030
16	HSST3X3X0	HSST3X3X0	0.025	1.000	0.025	HSS FLEX+A	8	1.890	2.460	2.460	4.030
17	HSST3X3X0	HSST3X3X0	0.094	1.000	0.094	HSS FLEX+A	4	1.890	2.460	2.460	4.030
18	HSST3X3X0	HSST3X3X0	0.162	1.000	0.162	HSS FLEX+A	5	1.890	2.460	2.460	4.030
19	HSST3X3X0	HSST3X3X0	0.086	1.000	0.086	HSS FLEX+A	4	1.890	2.460	2.460	4.030
20	HSST3X3X0	HSST3X3X0	0.027	1.000	0.027	HSS FLEX+A	5	1.890	2.460	2.460	4.030
21	HSST3X3X0	HSST3X3X0	0.094	1.000	0.094	HSS FLEX+A	4	1.890	2.460	2.460	4.030
22	HSST3X3X0	HSST3X3X0	0.040	1.000	0.040	HSS FLEX+A	5	1.890	2.460	2.460	4.030
23	HSST3X3X0	HSST3X3X0	0.029	1.000	0.029	HSS FLEX+A	5	1.890	2.460	2.460	4.030
24	HSST3X3X0	HSST3X3X0	0.033	1.000	0.033	HSS FLEX+A	5	1.890	2.460	2.460	4.030
25	HSST3X3X0	HSST3X3X0	0.000	1.000	0.000	HSS COMPR	4	1.890	2.460	2.460	4.030
26	HSST3X3X0	HSST3X3X0	0.000	1.000	0.000	HSS COMPR	4	1.890	2.460	2.460	4.030
30	HSST3X3X0	HSST3X3X0	0.001	1.000	0.001	HSS BEND Z	4	1.890	2.460	2.460	4.030
31	HSST3X3X0	HSST3X3X0	0.001	1.000	0.001	HSS BEND Z	4	1.890	2.460	2.460	4.030

Failed Members

There is no data of this type.



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Job No
148872000

Sheet No
41

Rev
3

Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

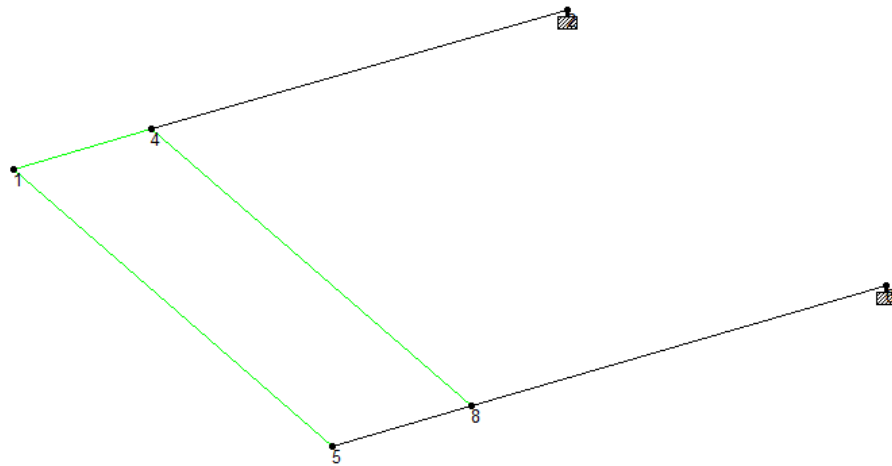
Statics Check Results

L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
2:W1	Loads	0.111	0.000	-0.209	-1.555	22.397	-0.816
2:W1	Reactions	-0.111	-0.000	0.209	1.555	-22.397	0.816
	Difference	0.000	-0.000	-0.000	0.000	-0.000	-0.000
1:DL	Loads	0.000	-0.508	0.000	-12.432	0.000	-61.002
1:DL	Reactions	0.000	0.508	-0.000	12.432	0.000	61.002
	Difference	0.000	0.000	-0.000	0.000	0.000	-0.000
3:W2	Loads	0.055	0.000	-0.059	-0.415	5.702	-0.382
3:W2	Reactions	-0.055	-0.000	0.059	0.000	-5.702	0.382
	Difference	0.000	-0.000	-0.000	-0.415	0.000	-0.000
7:0.75W3	Loads	0.126	0.000	-0.200	-1.464	20.976	-0.912
7:0.75W3	Reactions	-0.126	-0.000	0.200	1.152	-20.976	0.912
	Difference	0.000	-0.000	-0.000	-0.312	-0.000	-0.000

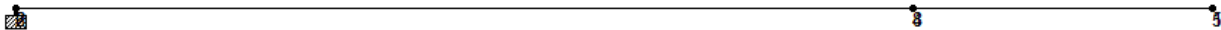
MSE Wall

The following structure spacing was accommodated from analyzing the THEA contract plans reinforcement for the retaining wall . It was concluded that the HSS arm would be welded to a square plate, with four bolts connecting the plate with the barrier. According to the structures index 5025 for the year 2000 the rebar spacing of 8" O.C will allow enough room for the plate connection.

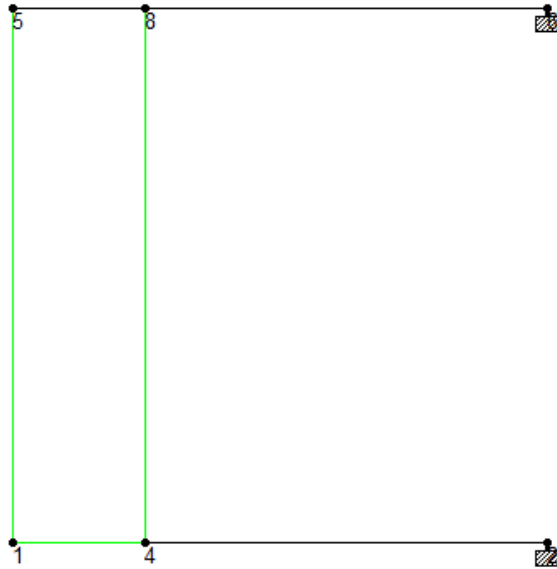
3D View-Length:



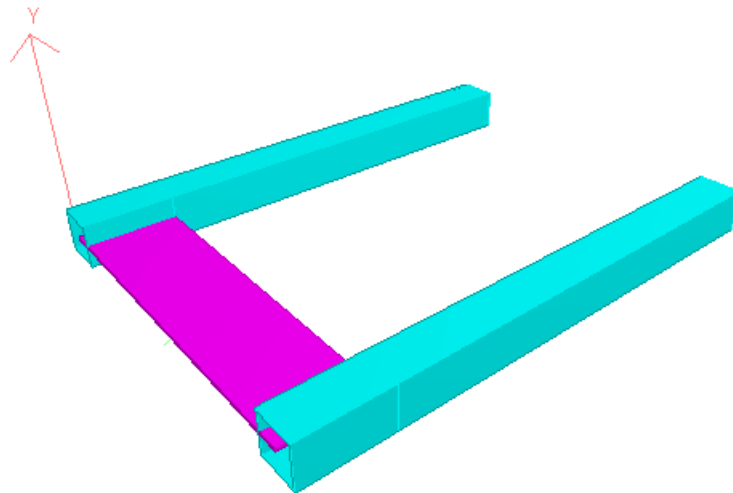
Side View:



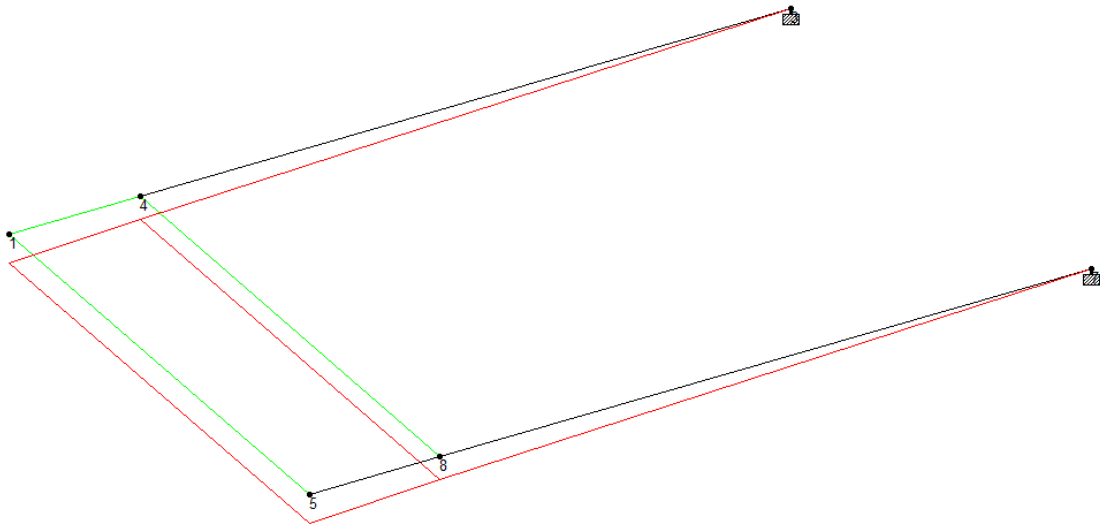
Plan View:



3D View:

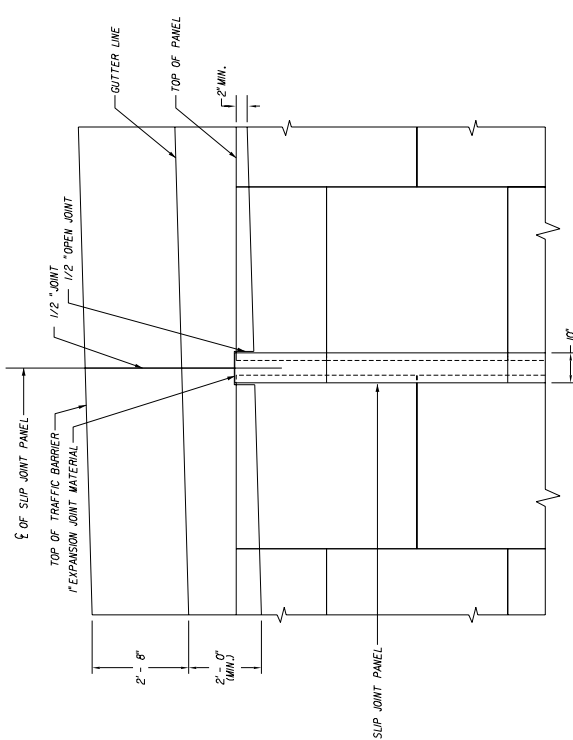


Deflection:

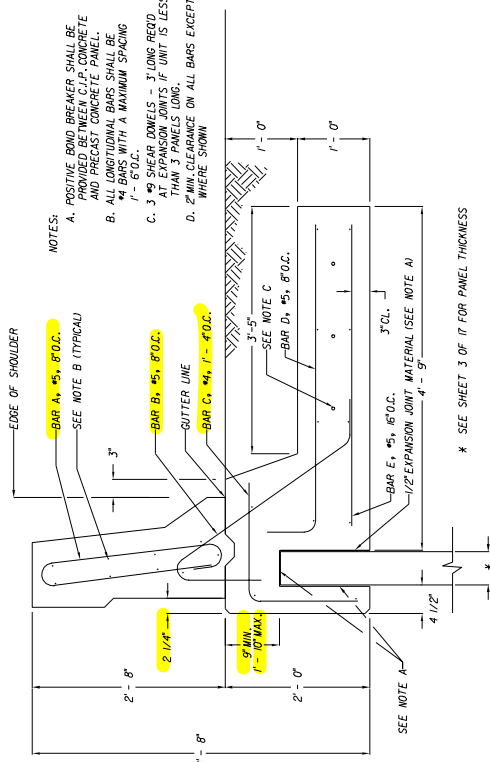




Existing Structural Plans

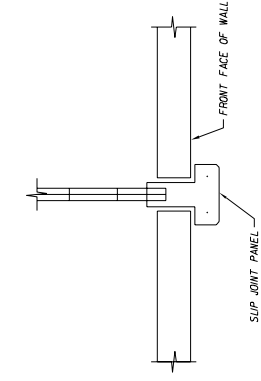
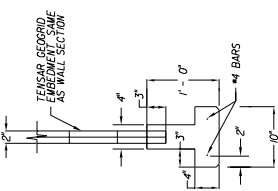


C.I.P. TRAFFIC BARRIER
OVER SLIP JOINT PANEL

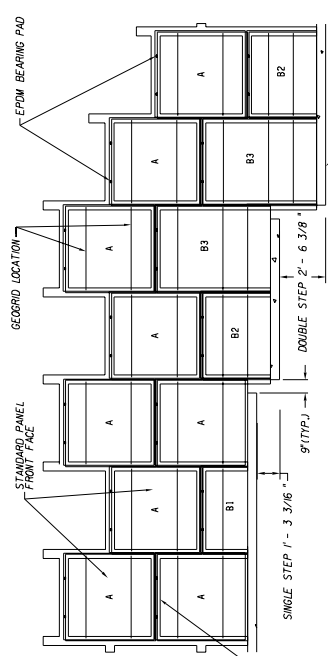


C.I.P. CONCRETE TRAFFIC BARRIER
NOT TO SCALE

* SEE SHEET 3 OF 17 FOR PANEL THICKNESS



SLIP JOINT DETAIL
NOT TO SCALE



TYPICAL LEVELING PAD STEP DETAIL
NOT TO SCALE

THIS SYSTEM MAY BE USED IN ALL ENVIRONMENTS.

STATE OF FLORIDA DEPARTMENT OF TRANSPORTATION ROAD DESIGN		RETAINING WALL SYSTEM TENSAR EARTH TECHNOLOGIES MSE RETAINING WALL	
Names	Date	Approved By	
Designed By	JMS	8/14/98	State Structures Design Engineer
Drawn By			Index No.
Checked By			00
			13 of 17
			5025



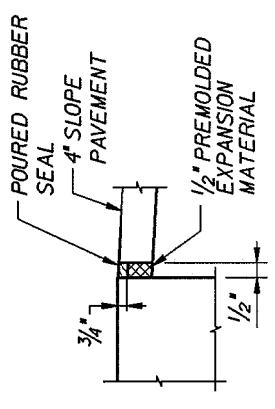
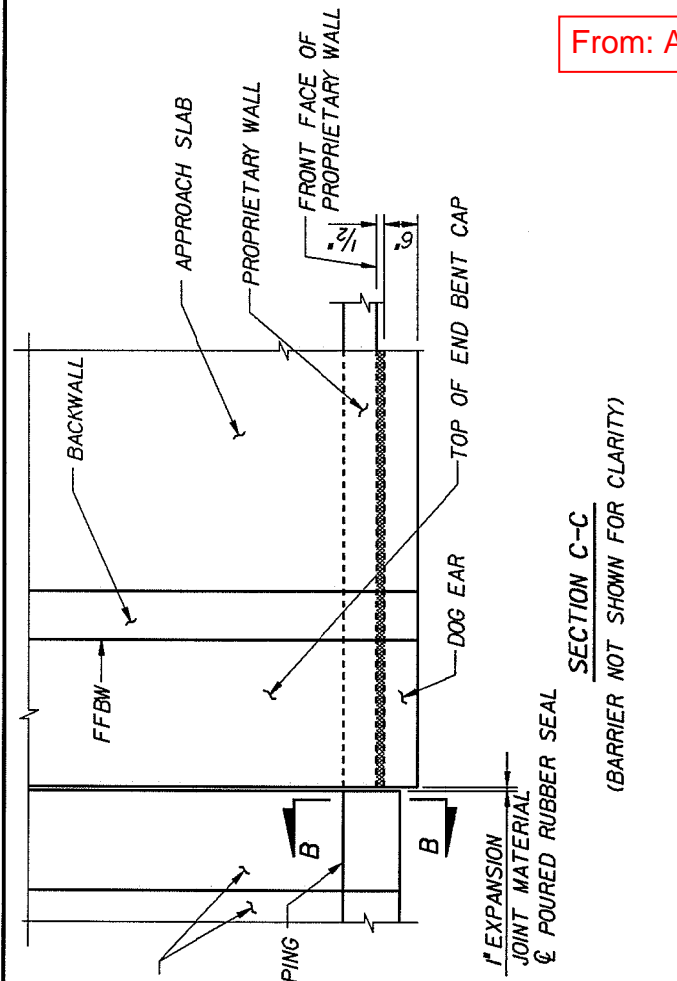
TENSAR
EARTH TECHNOLOGIES, INC.
3750 B
Lakelake Center, Suite 450
Atlanta, GA 30328
(404) 250-1290

THIS DESIGN IS BASED UPON SPECIFIC PROPERTIES OF TENSAR GEOTEXTILES AND GEOTEXTILES WHICH HAVE BEEN PROVIDED BY TENSAR EARTH TECHNOLOGIES, INC. FOR PRELIMINARY DESIGN PURPOSES AND SHALL NOT BE USED FOR FINAL DESIGN OR CONSTRUCTION.

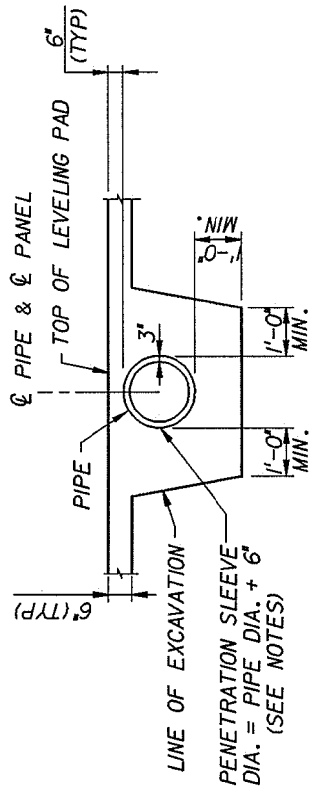
THIS DRAWING, DESIGN NOTES AND ASSOCIATED CALCULATIONS HAVE BEEN PREPARED BY TENSAR EARTH TECHNOLOGIES, INC. FOR PRELIMINARY DESIGN PURPOSES AND SHALL NOT BE USED FOR FINAL DESIGN OR CONSTRUCTION.

© 1998, TENSAR EARTH TECHNOLOGIES, INC.

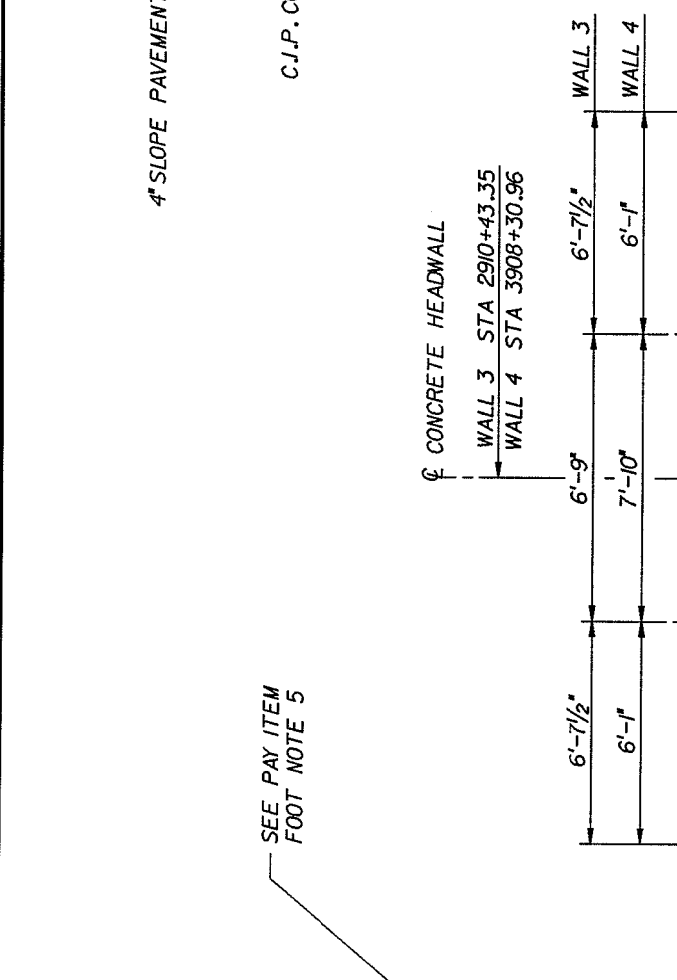
From: As-Built



NOTE: THIS DETAIL IS ALSO APPLICABLE BETWEEN SLOPE PAVEMENT AND END BENT CAP.



- NOTES:
1. FILL PENETRATION SLEEVE WITH CONCRETE FILL AFTER PIPE HAS BEEN SET AND BLOCKED.
 2. PIPE SHALL NOT BE PLACED DIRECTLY BENEATH THE JOINT OF A BOTTOM PANEL.
 3. CONCRETE ENCASEMENT AND CONCRETE FILL SHALL BE INCLUDED IN THE UNIT BID PRICE FOR RETAINING WALLS.

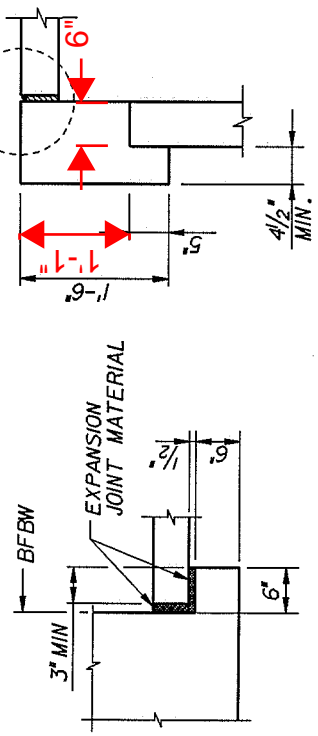


TYPICAL SECTION (SHOWING TYPICAL COPING AND BARRIER DIMENSIONS)

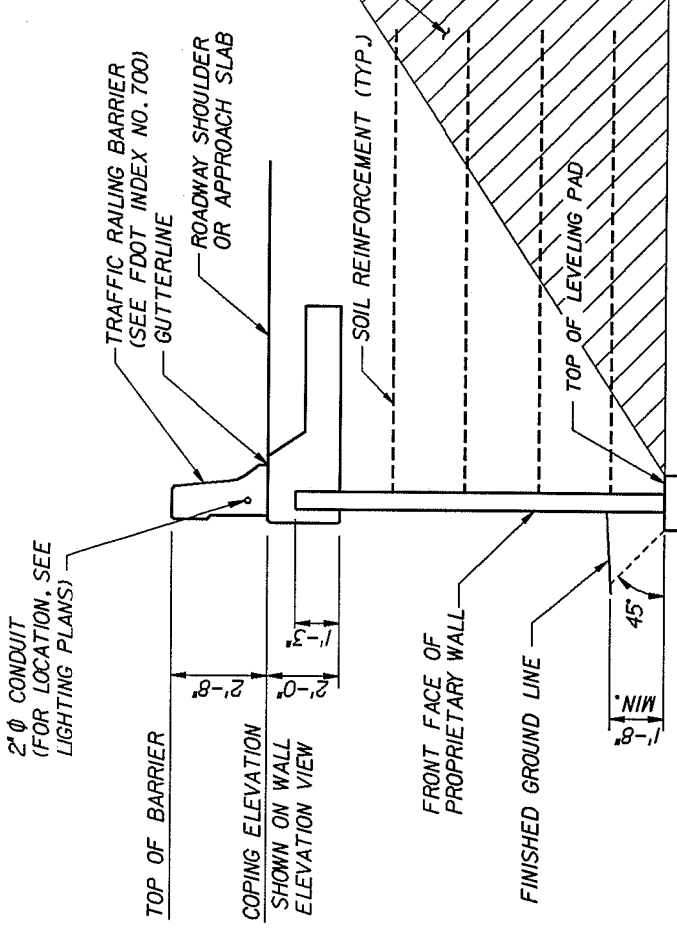
NOTES:
1. TYPICAL WALL DETAILS SHOWN ON THESE DRAWINGS MAY BE MODIFIED TO SUIT THE INDIVIDUAL WALL COMPANY'S DETAILS.

- NOTES:
1. HEADWALL MAY BE PRECAST OR C.J.P. CONCRETE.
 2. DESIGN AND DETAILS SHALL BE SUBMITTED WITH SHOP DRAWINGS FOR APPROVAL.
 3. HEADWALL DETAILS SHALL BE SIGNED AND SEALED BY A REGISTERED PROFESSIONAL ENGINEER.
 4. VOID SHALL BE FILLED WITH CLASS I CONCRETE.

HEADWALL



SECTION B-B



ELEVATION VIEW AT END BENT

REVISIONS		REVISED		DESCRIPTION	
DATE	BY	DATE	BY	DESCRIPTION	

ENGINEER OF RECORD:	TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY
Parsons Brinkerhoff	EXPRESSWAY AUTHORITY
Quade & Douglas, Inc.	COUNTY
5405 West Cypress St. Suite 300	HILLSBOROUGH
Tampa, Florida 33607	SR 618
ROAD NO.	CONSTRUCTION PROJECT NO.
SR 618	51.40.02

DATE	BY	DATE	BY	DESCRIPTION



STAAD Analysis

```

*****
*
*          STAAD.Pro V8i SELECTseries6          *
*          Version  20.07.11.70                *
*          Proprietary Program of              *
*          Bentley Systems, Inc.                *
*          Date=    JUL 19, 2018                *
*          Time=    13: 4:13                    *
*
*          USER ID: Kimley-Horn and Associates  *
*****
    
```

1. STAAD SPACE
- INPUT FILE: \\kimley-horn.com\FL_ORL\ORL_Structures_Projects-Structures\148872000 THEA Lighting Proje.. .STD
2. START JOB INFORMATION
3. ENGINEER DATE 19-JUN-18
4. JOB NAME RETAINING WALL 2
5. JOB CLIENT THEA
6. JOB NO 148872000
7. JOB REV 3
8. ENGINEER NAME IERM
9. END JOB INFORMATION
10. INPUT WIDTH 79
11. UNIT FEET KIP
12. JOINT COORDINATES
13. 1 0 0 0; 2 2 0 0; 4 0.5 0 0; 5 0 0 2; 6 2 0 2; 8 0.5 0 2
14. MEMBER INCIDENCES
15. 1 1 4; 3 4 2; 4 5 8; 5 8 6
16. ELEMENT INCIDENCES SHELL
17. 6 8 4 1 5
18. ELEMENT PROPERTY
19. 6 THICKNESS 0.020833
20. DEFINE MATERIAL START
21. ISOTROPIC STEEL
22. E 4.176E+006
23. POISSON 0.3
24. DENSITY 0.489024
25. ALPHA 6E-006
26. DAMP 0.03
27. TYPE STEEL
28. STRENGTH FY 5184 FU 8352 RY 1.5 RT 1.2
29. ISOTROPIC CONCRETE
30. E 453600
31. POISSON 0.17
32. DENSITY 0.150336
33. ALPHA 5E-006
34. DAMP 0.05
35. TYPE CONCRETE
36. STRENGTH FCU 576
37. ISOTROPIC A500-GR.B
38. E 4.176E+006

STAAD SPACE

-- PAGE NO. 2

39. POISSON 0.3
 40. DENSITY 0.49
 41. ALPHA 6E-006
 42. DAMP 0.03
 43. G 1.6128E-006
 44. TYPE STEEL
 45. STRENGTH FY 6624 FU 8352 RY 1.1 RT 1.2
 46. END DEFINE MATERIAL
 47. MEMBER PROPERTY AMERICAN
 48. 5 TABLE ST HSST3X3X0.188
 49. 3 TABLE ST HSST3X3X0.188
 50. 1 TABLE ST HSST3X3X0.188
 51. 4 TABLE ST HSST3X3X0.188
 52. CONSTANTS
 53. MATERIAL STEEL MEMB 6
 54. MATERIAL A500-GR.B MEMB 1 3 TO 5
 55. SUPPORTS
 56. 2 6 FIXED
 57. LOAD 1 LOADTYPE DEAD TITLE DL
 58. SELFWEIGHT Y -1 LIST ALL
 59. JOINT LOAD
 60. 1 5 FY -0.015
 61. LOAD 2 LOADTYPE WIND TITLE W1
 62. JOINT LOAD
 63. 1 5 FZ -0.0261
 64. 1 5 MX -0.0162
 65. 1 5 FX 0.014
 66. 1 5 MZ -0.008
 67. LOAD 3 LOADTYPE WIND TITLE 0.75W2
 68. JOINT LOAD
 69. 1 5 FZ -0.019
 70. 1 5 MX -0.012
 71. 1 5 FX 0.011
 72. 1 5 MZ 0.006
 73. LOAD COMB 4 1.25DL
 74. 1 1.25
 75. LOAD COMB 5 1.1DL+1.0W1
 76. 1 1.1 2 1.0
 77. LOAD COMB 6 1.1DL+1.0W2
 78. 1 1.1 3 1.0
 79. PERFORM ANALYSIS PRINT ALL

P R O B L E M S T A T I S T I C S

NUMBER OF JOINTS	6	NUMBER OF MEMBERS	4
NUMBER OF PLATES	1	NUMBER OF SOLIDS	0
NUMBER OF SURFACES	0	NUMBER OF SUPPORTS	2

STAAD SPACE

-- PAGE NO. 3

SOLVER USED IS THE OUT-OF-CORE BASIC SOLVER

ORIGINAL/FINAL BAND-WIDTH= 5/ 5/ 24 DOF
TOTAL PRIMARY LOAD CASES = 3, TOTAL DEGREES OF FREEDOM = 24
TOTAL LOAD COMBINATION CASES = 3 SO FAR.
SIZE OF STIFFNESS MATRIX = 1 DOUBLE KILO-WORDS
REQRD/AVAIL. DISK SPACE = 12.0/ 0.0 MB

STAAD SPACE

-- PAGE NO. 4

LOADING 1 LOADTYPE DEAD TITLE DL

SELFWEIGHT Y -1.000

ACTUAL WEIGHT OF THE STRUCTURE = 0.036 KIP

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	-0.01	0.00	0.00	0.00	0.00
5	0.00	-0.01	0.00	0.00	0.00	0.00

LOADING 2 LOADTYPE WIND TITLE W1

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.03	0.00	0.00	0.00
5	0.00	0.00	-0.03	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.02	0.00	0.00
5	0.00	0.00	0.00	-0.02	0.00	0.00
1	0.01	0.00	0.00	0.00	0.00	0.00
5	0.01	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	-0.01
5	0.00	0.00	0.00	0.00	0.00	-0.01

LOADING 3 LOADTYPE WIND TITLE 0.75W2

JOINT LOAD - UNIT KIP FEET

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00	0.00	-0.02	0.00	0.00	0.00
5	0.00	0.00	-0.02	0.00	0.00	0.00
1	0.00	0.00	0.00	-0.01	0.00	0.00
5	0.00	0.00	0.00	-0.01	0.00	0.00
1	0.01	0.00	0.00	0.00	0.00	0.00
5	0.01	0.00	0.00	0.00	0.00	0.00
1	0.00	0.00	0.00	0.00	0.00	0.01
5	0.00	0.00	0.00	0.00	0.00	0.01

FOR LOADING - 1

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
-------	---------	---------	---------	-------	-------	-------

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	0.00000E+00	-1.91548E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.33984E-04
2	0.00000E+00	-4.82344E-03	0.00000E+00	0.00000E+00	0.00000E+00	1.20586E-03
4	0.00000E+00	-8.97821E-03	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03
5	0.00000E+00	-1.91548E-02	0.00000E+00	0.00000E+00	0.00000E+00	-1.33984E-04
6	0.00000E+00	-4.82344E-03	0.00000E+00	0.00000E+00	0.00000E+00	1.20586E-03
8	0.00000E+00	-8.97821E-03	0.00000E+00	0.00000E+00	0.00000E+00	-1.07188E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 1
LOADTYPE DEAD TITLE DL

CENTER OF FORCE BASED ON Y FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.428929498E+00
Y = 0.000000000E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.0000000E+00
SUMMATION FORCE-Y = -6.5912836E-02
SUMMATION FORCE-Z = 0.0000000E+00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 6.5912838E-02 MY= 0.0000000E+00 MZ= -2.8271960E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 1)
SUMMATION FORCE-X = 0.0000000E+00
SUMMATION FORCE-Y = 6.5912836E-02
SUMMATION FORCE-Z = 0.0000000E+00

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -6.5912838E-02 MY= 0.0000000E+00 MZ= 2.8271960E-02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 1)

MAXIMUMS	AT NODE
X = 0.00000E+00	0
Y = -1.54897E-03	5
Z = 0.00000E+00	0
RX= 3.36931E-06	4
RY= 0.00000E+00	0
RZ= 9.38999E-05	5

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/	EXT FY/	EXT FZ/	EXT MX/	EXT MY/	EXT MZ/
	INT FX	INT FY	INT FZ	INT MX	INT MY	INT MZ

SUPPORT=1

FOR LOADING - 2

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	1.40000E-02	0.00000E+00	-2.61000E-02	-1.62000E-02	0.00000E+00	-8.00000E-03
5	1.40000E-02	0.00000E+00	-2.61000E-02	-1.62000E-02	0.00000E+00	-8.00000E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 2
LOADTYPE WIND TITLE W1

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.571428576E+00
Z = 0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.620689705E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = 2.8000001E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -5.2200001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -3.2400003E-02 MY= 2.8000002E-02 MZ= -1.6000001E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 2)

SUMMATION FORCE-X = -2.8000001E-02
SUMMATION FORCE-Y = -2.4286129E-17
SUMMATION FORCE-Z = 5.2200001E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 3.2400003E-02 MY= -2.8000002E-02 MZ= 1.6000001E-02

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 2)

MAXIMUMS	AT NODE
X = 1.73499E-05	1
Y = 1.10496E-03	5
Z = -2.63671E-04	1
RX= -1.94190E-03	1
RY= -7.76191E-06	8
RZ= -7.15585E-05	5

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
----	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUPPORT=1

FOR LOADING - 3

APPLIED JOINT EQUIVALENT LOADS

JOINT	FORCE-X	FORCE-Y	FORCE-Z	MOM-X	MOM-Y	MOM-Z
1	1.10000E-02	0.00000E+00	-1.90000E-02	-1.20000E-02	0.00000E+00	6.00000E-03
5	1.10000E-02	0.00000E+00	-1.90000E-02	-1.20000E-02	0.00000E+00	6.00000E-03

STATIC LOAD/REACTION/EQUILIBRIUM SUMMARY FOR CASE NO. 3
LOADTYPE WIND TITLE 0.75W2

CENTER OF FORCE BASED ON X FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = -0.545454541E+00
Z = 0.100000003E+01

CENTER OF FORCE BASED ON Z FORCES ONLY (FEET).
(FORCES IN NON-GLOBAL DIRECTIONS WILL INVALIDATE RESULTS)

X = 0.000000000E+00
Y = 0.631578959E+00
Z = 0.100000003E+01

***TOTAL APPLIED LOAD (KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = 2.2000000E-02
SUMMATION FORCE-Y = 0.0000000E+00
SUMMATION FORCE-Z = -3.7999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= -2.4000000E-02 MY= 2.2000001E-02 MZ= 1.2000000E-02

***TOTAL REACTION LOAD(KIP FEET) SUMMARY (LOADING 3)

SUMMATION FORCE-X = -2.2000000E-02
SUMMATION FORCE-Y = -1.5612511E-16
SUMMATION FORCE-Z = 3.7999999E-02

SUMMATION OF MOMENTS AROUND THE ORIGIN-
MX= 2.4000000E-02 MY= -2.2000001E-02 MZ= -1.2000000E-02

STAAD SPACE

-- PAGE NO. 8

MAXIMUM DISPLACEMENTS (INCH /RADIANS) (LOADING 3)
 MAXIMUMS AT NODE
 X = 1.29772E-05 1
 Y = -8.22073E-04 1
 Z = -1.91973E-04 1
 RX= -1.43849E-03 5
 RY= -5.65413E-06 8
 RZ= 5.33049E-05 1

EXTERNAL AND INTERNAL JOINT LOAD SUMMARY (KIP FEET)-

JT	EXT FX/ INT FX	EXT FY/ INT FY	EXT FZ/ INT FZ	EXT MX/ INT MX	EXT MY/ INT MY	EXT MZ/ INT MZ
----	-------------------	-------------------	-------------------	-------------------	-------------------	-------------------

SUPPORT=1

LOAD COMBINATION NO. 4
 1.25DL

LOADING- 1.
 FACTOR - 1.25

LOAD COMBINATION NO. 5
 1.1DL+1.0W1

LOADING- 1. 2.
 FACTOR - 1.10 1.00

LOAD COMBINATION NO. 6
 1.1DL+1.0W2

LOADING- 1. 3.
 FACTOR - 1.10 1.00

***** END OF DATA FROM INTERNAL STORAGE *****

80. PARAMETER 2
 81. CODE LRFD
 82. CHECK CODE ALL

STAAD.Pro CODE CHECKING - (LRFD 3RD EDITION) v1.0

ALL UNITS ARE - KIP FEET (UNLESS OTHERWISE Noted)

MEMBER	TABLE	RESULT/ FX	CRITICAL COND/ MY	RATIO/ MZ	LOADING/ LOCATION
=====					
1	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.006	6
		0.02 C	0.01	0.02	0.50
3	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.019	6
		0.03 C	-0.02	0.08	1.50
4	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS FLEX+AXL	0.005	2
		0.00 T	0.02	-0.01	0.50
5	ST	HSST3X3X0.188	(AISC SECTIONS)		
		PASS	HSS BEND Z	0.012	4
		0.00 C	0.00	0.06	1.50

***** END OF TABULATED RESULT OF DESIGN *****

83. FINISH

***** END OF THE STAAD.Pro RUN *****

**** DATE= JUL 19,2018 TIME= 13: 4:15 ****

* For technical assistance on STAAD.Pro, please visit *
* <http://selectservices.bentley.com/en-US/> *
* * * * *
* Details about additional assistance from *
* Bentley and Partners can be found at program menu *
* Help->Technical Support *
* * * * *
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* <http://www.bentley.com> *



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Job No
148872000

Sheet No
1

Rev
3

Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Job Information

	Engineer	Checked	Approved
Name:	IERM		
Date:	19-Jun-18		

Project ID	
Project Name	

Structure Type	SPACE FRAME
-----------------------	-------------

Number of Nodes	6	Highest Node	8
Number of Elements	4	Highest Beam	5
Number of Plates	1	Highest Plate	6

Number of Basic Load Cases	3
Number of Combination Load Cases	3

Included in this printout are data for:

All	The Whole Structure
------------	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	W1
Primary	3	0.75W2
Combination	4	1.25DL
Combination	5	1.1DL+1.0W1
Combination	6	1.1DL+1.0W2

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	4	0.500	4	0
3	4	2	1.500	3	0
4	5	8	0.500	5	0
5	8	6	1.500	2	0

Plates

Plate	Node A	Node B	Node C	Node D	Property
6	8	4	1	5	1



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Job No
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Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (/°F)
1	A500-GR.B	29E+3	0.300	0.000	6E-6
2	STEEL	29E+3	0.300	0.000	6E-6
3	STAINLESSSTEEL	28E+3	0.300	0.000	10E-6
4	ALUMINUM	10E+3	0.330	0.000	13E-6
5	CONCRETE	3.15E+3	0.170	0.000	5E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
2	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed
6	Fixed	Fixed	Fixed	Fixed	Fixed	Fixed

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	W1	Wind
3	0.75W2	Wind

Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
4	1.25DL	1	DL	1.25
5	1.1DL+1.0W1	1	DL	1.10
		2	W1	1.00
6	1.1DL+1.0W2	1	DL	1.10
		3	0.75W2	1.00



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Job No
148872000

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Job Title Retaining Wall 2

Part

Ref

By IERM Date 19-Jun-18 Chd

Client THEA

File THEA4- Retaining WallHC Date/Time 19-Jul-2018 11:20

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	1	2:W1	0.000	-0.000	-0.000	0.000	-0.002	-0.000	0.000
Min X	5	2:W1	-0.000	0.001	-0.000	0.001	-0.002	-0.000	-0.000
Max Y	5	2:W1	-0.000	0.001	-0.000	0.001	-0.002	-0.000	-0.000
Min Y	1	6:1.1DL+1.0W ₂	0.000	-0.003	-0.000	0.003	-0.001	-0.000	0.000
Max Z	1	1:DL	0.000	-0.002	0.000	0.002	0.000	0.000	0.000
Min Z	1	2:W1	0.000	-0.000	-0.000	0.000	-0.002	-0.000	0.000
Max rX	8	2:W1	-0.000	0.001	-0.000	0.001	0.001	-0.000	-0.000
Min rX	1	2:W1	0.000	-0.000	-0.000	0.000	-0.002	-0.000	0.000
Max rY	1	1:DL	0.000	-0.002	0.000	0.002	0.000	0.000	0.000
Min rY	8	2:W1	-0.000	0.001	-0.000	0.001	0.001	-0.000	-0.000
Max rZ	1	6:1.1DL+1.0W ₂	0.000	-0.003	-0.000	0.003	-0.001	-0.000	0.000
Min rZ	5	2:W1	-0.000	0.001	-0.000	0.001	-0.002	-0.000	-0.000
Max Rst	1	6:1.1DL+1.0W ₂	0.000	-0.003	-0.000	0.003	-0.001	-0.000	0.000

Beam Displacement Detail Summary

Displacements shown in *italic* indicate the presence of an offset

	Beam	L/C	d (ft)	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	1	2:W1	0.000	0.000	-0.000	-0.000	0.000
Min X	4	2:W1	0.150	-0.000	0.001	-0.000	0.001
Max Y	4	2:W1	0.000	0.000	0.001	-0.000	0.001
Min Y	1	6:1.1DL+1.0W ₂	0.000	0.000	-0.003	-0.000	0.003
Max Z	1	1:DL	0.000	0.000	-0.002	0.000	0.002
Min Z	1	2:W1	0.000	0.000	-0.000	-0.000	0.000
Max Rst	1	6:1.1DL+1.0W ₂	0.000	0.000	-0.003	-0.000	0.003

Beam End Displacement Summary

Displacements shown in *italic* indicate the presence of an offset

	Beam	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)
Max X	1	1	2:W1	0.000	-0.000	-0.000	0.000
Min X	4	8	2:W1	-0.000	0.001	-0.000	0.001
Max Y	4	5	2:W1	0.000	0.001	-0.000	0.001
Min Y	1	1	6:1.1DL+1.0W ₂	0.000	-0.003	-0.000	0.003
Max Z	1	1	1:DL	0.000	-0.002	0.000	0.002
Min Z	1	1	2:W1	0.000	-0.000	-0.000	0.000
Max Rst	1	1	6:1.1DL+1.0W ₂	0.000	-0.003	-0.000	0.003



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Job No
148872000

Sheet No
4

Rev
3

Job Title Retaining Wall 2

Part

Ref

By IERM Date 19-Jun-18 Chd

Client THEA

File THEA4- Retaining WallHC Date/Time 19-Jul-2018 11:20

Beam End Force Summary

The signs of the forces at end B of each beam have been reversed. For example: this means that the Min Fx entry gives the largest tension value for an beam.

	Beam	Node	L/C	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	3	4	2:W1	0.044	-0.016	-0.026	0.000	0.205	-0.081
Min Fx	5	8	2:W1	-0.016	0.016	-0.026	0.000	0.204	-0.111
Max Fy	5	8	2:W1	-0.016	0.016	-0.026	0.000	0.204	-0.111
Min Fy	3	2	5:1.1DL+1.0W1	0.044	-0.052	-0.026	0.000	-0.266	0.894
Max Fz	1	1	2:W1	0.026	-0.015	0.034	-0.000	-0.021	-0.154
Min Fz	3	4	2:W1	0.044	-0.016	-0.026	0.000	0.205	-0.081
Max Mx	5	8	2:W1	-0.016	0.016	-0.026	0.000	0.204	-0.111
Min Mx	1	1	5:1.1DL+1.0W1	0.026	-0.034	0.034	-0.000	-0.021	-0.155
Max My	3	4	2:W1	0.044	-0.016	-0.026	0.000	0.205	-0.081
Min My	3	2	2:W1	0.044	-0.016	-0.026	0.000	-0.266	0.210
Max Mz	3	2	6:1.1DL+1.0W2	0.033	-0.048	-0.019	0.000	-0.194	0.982
Min Mz	5	6	2:W1	-0.016	0.016	-0.026	0.000	-0.265	-0.402

Beam Force Detail Summary

Sign convention as diagrams:- positive above line, negative below line except Fx where positive is compression. Distance d is given from beam end A.

	Beam	L/C	d (ft)	Axial	Shear		Torsion	Bending	
				Fx (kip)	Fy (kip)	Fz (kip)	Mx (kip'in)	My (kip'in)	Mz (kip'in)
Max Fx	3	2:W1	0.000	0.044	-0.016	-0.026	0.000	0.205	-0.081
Min Fx	5	2:W1	0.000	-0.016	0.016	-0.026	0.000	0.204	-0.111
Max Fy	5	2:W1	0.000	-0.016	0.016	-0.026	0.000	0.204	-0.111
Min Fy	3	5:1.1DL+1.0W1	1.500	0.044	-0.052	-0.026	0.000	-0.266	0.894
Max Fz	1	2:W1	0.000	0.026	-0.015	0.034	-0.000	-0.021	-0.154
Min Fz	3	2:W1	0.000	0.044	-0.016	-0.026	0.000	0.205	-0.081
Max Mx	5	2:W1	0.000	-0.016	0.016	-0.026	0.000	0.204	-0.111
Min Mx	1	5:1.1DL+1.0W1	0.000	0.026	-0.034	0.034	-0.000	-0.021	-0.155
Max My	3	2:W1	0.000	0.044	-0.016	-0.026	0.000	0.205	-0.081
Min My	3	2:W1	1.500	0.044	-0.016	-0.026	0.000	-0.266	0.210
Max Mz	3	6:1.1DL+1.0W2	1.500	0.033	-0.048	-0.019	0.000	-0.194	0.982
Min Mz	5	2:W1	1.500	-0.016	0.016	-0.026	0.000	-0.265	-0.402



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Job Title Retaining Wall 2

Part

Ref

By IERM Date 19-Jun-18 Chd

Client THEA

File THEA4- Retaining WallHC Date/Time 19-Jul-2018 11:20

Beam Combined Axial and Bending Stresses Summary

Beam	L/C	Length (ft)	Max Comp			Max Tens		
			Stress (psi)	d (ft)	Corner	Stress (psi)	d (ft)	Corner
1	1:DL	0.500	69.858	0.500	3	-69.858	0.500	1
	2:W1	0.500	164.766	0.500	2	-136.995	0.500	4
	3:0.75W2	0.500	149.820	0.500	3	-128.816	0.500	1
	4:1.25DL	0.500	87.323	0.500	3	-87.323	0.500	1
	5:1.1DL+1.0W1	0.500	163.855	0.500	3	-136.084	0.500	1
	6:1.1DL+1.0W2	0.500	226.664	0.500	3	-205.660	0.500	1
3	1:DL	1.500	378.855	1.500	3	-378.855	1.500	1
	2:W1	1.500	313.516	1.500	4	-266.867	1.500	2
	3:0.75W2	1.500	317.570	1.500	4	-282.756	1.500	2
	4:1.25DL	1.500	473.569	1.500	3	-473.569	1.500	1
	5:1.1DL+1.0W1	1.500	730.256	1.500	4	-683.608	1.500	2
	6:1.1DL+1.0W2	1.500	734.310	1.500	4	-699.496	1.500	2
4	1:DL	0.500	69.858	0.500	3	-69.858	0.500	1
	2:W1	0.500	193.742	0.500	2	-194.237	0.500	4
	3:0.75W2	0.500	114.514	0.500	3	-114.086	0.500	1
	4:1.25DL	0.500	87.323	0.500	3	-87.323	0.500	1
	5:1.1DL+1.0W1	0.500	116.898	0.500	2	-117.393	0.500	1
	6:1.1DL+1.0W2	0.500	191.358	0.500	3	-190.930	0.500	1
5	1:DL	1.500	378.855	1.500	3	-378.855	1.500	1
	2:W1	1.500	398.303	1.500	1	-415.322	1.500	3
	3:0.75W2	1.500	206.236	1.500	1	-217.769	1.500	3
	4:1.25DL	1.500	473.569	1.500	3	-473.569	1.500	1
	5:1.1DL+1.0W1	1.500	324.636	1.500	4	-341.655	1.500	2
	6:1.1DL+1.0W2	1.500	434.237	1.500	4	-445.771	1.500	2

Plate Center Stress Summary

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Max Qx	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Min Qx	6	4:1.25DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.037	-0.000
Max Qy	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Min Qy	6	4:1.25DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.037	-0.000
Max Sx	6	1:DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.029	-0.000
Min Sx	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Max Sy	6	1:DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.029	-0.000
Min Sy	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Max Sxy	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Min Sxy	6	1:DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.029	-0.000
Max Mx	6	6:1.1DL+1.0W2	8.000	-0.001	-0.036	-0.291	14.600	0.000	0.070	5.103
Min Mx	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Max My	6	6:1.1DL+1.0W2	8.000	-0.001	-0.036	-0.291	14.600	0.000	0.070	5.103



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148872000

Sheet No
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Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Plate Center Stress Summary Cont...

	Plate	L/C	Shear		Membrane			Bending		
			Qx (psi)	Qy (psi)	Sx (psi)	Sy (psi)	Sxy (psi)	Mx (lb·in/in)	My (lb·in/in)	Mxy (lb·in/in)
Min My	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Max Mxy	6	2:W1	10.800	0.000	-0.046	-0.371	20.055	-0.000	-0.050	6.889
Min Mxy	6	4:1.25DL	-0.000	-0.001	0.000	0.000	0.000	0.000	0.037	-0.000

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
Max FX	6	2:W1	0.016	-0.016	0.026	-0.000	0.265	0.402
Min FX	2	2:W1	-0.044	0.016	0.026	-0.000	0.266	-0.210
Max FY	2	5:1.1DL+1.0W1	-0.044	0.052	0.026	-0.000	0.266	-0.894
Min FY	6	2:W1	0.016	-0.016	0.026	-0.000	0.265	0.402
Max FZ	2	2:W1	-0.044	0.016	0.026	-0.000	0.266	-0.210
Min FZ	2	1:DL	0.000	0.033	0.000	-0.000	0.000	-0.621
Max MX	6	4:1.25DL	0.000	0.041	0.000	0.000	0.000	-0.777
Min MX	6	2:W1	0.016	-0.016	0.026	-0.000	0.265	0.402
Max MY	2	2:W1	-0.044	0.016	0.026	-0.000	0.266	-0.210
Min MY	2	1:DL	0.000	0.033	0.000	-0.000	0.000	-0.621
Max MZ	6	2:W1	0.016	-0.016	0.026	-0.000	0.265	0.402
Min MZ	2	6:1.1DL+1.0W2	-0.033	0.048	0.019	-0.000	0.194	-0.982

Reactions

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kip)	FY (kip)	FZ (kip)	MX (kip·in)	MY (kip·in)	MZ (kip·in)
2	1:DL	0.000	0.033	0.000	-0.000	0.000	-0.621
	2:W1	-0.044	0.016	0.026	-0.000	0.266	-0.210
	3:0.75W2	-0.033	0.012	0.019	-0.000	0.194	-0.299
	4:1.25DL	0.000	0.041	0.000	-0.000	0.000	-0.777
	5:1.1DL+1.0W1	-0.044	0.052	0.026	-0.000	0.266	-0.894
	6:1.1DL+1.0W2	-0.033	0.048	0.019	-0.000	0.194	-0.982
6	1:DL	0.000	0.033	0.000	0.000	0.000	-0.621
	2:W1	0.016	-0.016	0.026	-0.000	0.265	0.402
	3:0.75W2	0.011	-0.012	0.019	-0.000	0.193	0.155
	4:1.25DL	0.000	0.041	0.000	0.000	0.000	-0.777
	5:1.1DL+1.0W1	0.016	0.020	0.026	-0.000	0.265	-0.281
	6:1.1DL+1.0W2	0.011	0.024	0.019	-0.000	0.193	-0.529



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Sheet No
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Rev
3

Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Steel Design (Track 2) Beam 1 Check 1

```

*****
MEMBER 1 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PROPERTY
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
PARAMETER 0.0 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL SHEAR-Y SHEAR-Z MOMENT-Y MOMENT-Z
VALUE 0.0 0.0 0.0 0.0 0.0
LOCATION 0.0 0.5 0.0 0.5 0.5
LOADING 2 5 2 2 6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
PASS HSS FLEX+AXL 0.006 6
0.02 C 0.01 0.02 0.50
*****
1 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Steel Design (Track 2) Beam 3 Check 1

```

*****
MEMBER 3 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

PARAMETER	IN KIP	INCH	UNIT
KL/R-Y=	15.78		L6
KL/R-Z=	15.78		L6
UNL =	18.00		L6
CB =	1.00		L6
PHIC =	0.00		L6
PHIB =	0.90		L6
FYLD =	36.00		L6
NSF =	1.00		
DFE =	0.00	0.0	
dff =	0.00		

```

*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

PROPERTY	VALUE
AX	0.1890E+1
AY	0.1044E+1
AZ	0.1044E+1
PY	0.1970E+1
PZ	0.1970E+1
RY	0.1141E+1
RZ	0.1141E+1

```

*****
CAPACITIES
IN KIP INCH
*****
PNC=0.5708E+2
pnc=0.3290E-1
PNT=0.6124E+2
pnt=0.0000E+0
MNZ=0.6383E+2
mnz=0.9822E+0
MNY=0.6383E+2
mny=0.1935E+0
VN =0.2030E+2
vn =0.4825E-1

```

ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)

MAX FORCE/ MOMENT SUMMARY (KIP-FEET)

	AXIAL	SHEAR-Y	SHEAR-Z	MOMENT-Y	MOMENT-Z
VALUE	0.0	0.1	0.0	0.0	0.1
LOCATION	0.0	1.5	0.0	1.5	1.5
LOADING	2	5	2	2	6

```

*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/ CRITICAL COND/ RATIO/ LOADING/
FX MY MZ LOCATION
=====
PASS HSS FLEX+AXL 0.019 6
0.03 C -0.02 0.08 1.50
*****

```

3 ST HSST3X3X0.188 (AISC SECTIONS)



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Job No
148872000

Sheet No
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Rev
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Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Steel Design (Track 2) Beam 4 Check 1

```

*****
MEMBER 4 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 0.50 --->|
*****
PARAMETER          0.0 (KIP-FEET)
IN KIP INCH
KL/R-Y= 5.26
KL/R-Z= 5.26
UNL = 6.00
CB = 1.00
PHIC = 0.00
PHIB = 0.90
FYLD = 36.00
NSF = 1.00
DFE = 0.00
dff = 0.00
*****
AISC SECTIONS
ST HSST3X3X0.188
*****
PROPERTIES
IN INCH UNIT
AX=0.1890E+1
AY=0.1044E+1
AZ=0.1044E+1
PY=0.1970E+1
PZ=0.1970E+1
RY=0.1141E+1
RZ=0.1141E+1
*****
CAPACITIES
IN KIP INCH
PNC=0.5775E+2
pnc=0.0000E+0
PNT=0.6124E+2
pnt=0.4678E-3
MNZ=0.6383E+2
mnz=0.1270E+0
MNY=0.6383E+2
mny=0.1911E+0
VN =0.2030E+2
vn =0.1507E-1
*****
ABSOLUTE MZ ENVELOPE
(WITH LOAD NO.)
MAX FORCE/ MOMENT SUMMARY (KIP-FEET)
*****
AXIAL      SHEAR-Y      SHEAR-Z      MOMENT-Y      MOMENT-Z
VALUE      -0.0              0.0              0.0              0.0              0.0
LOCATION     0.0              0.5              0.0              0.5              0.5
LOADING    2                4                2                2                6
*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/      CRITICAL COND/      RATIO/      LOADING/
FX           MY                   MZ           LOCATION
*****
PASS         HSS FLEX+AXL        0.005        2
0.00 T       0.02                -0.01        0.50
*****
4 ST HSST3X3X0.188 (AISC SECTIONS)

```



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Job No
148872000

Sheet No
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Rev
3

Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Steel Design (Track 2) Beam 5 Check 1

```

*****
MEMBER 5 *
DESIGN CODE *
LRFD 2001 *
*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

PARAMETER	IN KIP	INCH				
KL/R-Y=	15.78					
KL/R-Z=	15.78					
UNL =	18.00					
CB =	1.00					
PHIC =	0.00					
PHIB =	0.90					
FYLD =	36.00					
NSF =	1.00					
DFE =	0.00					
dff =	0.00					

```

*****
|<---LENGTH (FT)= 1.50 --->|
*****

```

AXIAL	SHEAR-Y	SHEAR-Z	MOMENT-Y	MOMENT-Z
VALUE	-0.0	0.0	0.0	0.1
LOCATION	0.0	1.5	0.0	1.5
LOADING	2	4	2	4

```

*****
DESIGN SUMMARY (KIP-FEET)
*****
RESULT/          CRITICAL COND/          RATIO/          LOADING/
FX              MY              MZ              LOCATION
=====
PASS           HSS BEND Z           0.012           4
0.00 C         0.00                 0.06            1.50
*****

```

5 ST HSST3X3X0.188 (AISC SECTIONS)



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Job No
148872000

Sheet No
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Rev
3

Job Title Retaining Wall 2

Part

Ref

By IERM Date 19-Jun-18 Chd

Client THEA

File THEA4- Retaining WallHC Date/Time 19-Jul-2018 11:20

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Allowable		Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
			Ratio	Ratio							
1	HSST3X3X0	HSST3X3X0	0.006	1.000	0.006	HSS FLEX+A	6	1.890	2.460	2.460	4.030
3	HSST3X3X0	HSST3X3X0	0.019	1.000	0.019	HSS FLEX+A	6	1.890	2.460	2.460	4.030
4	HSST3X3X0	HSST3X3X0	0.005	1.000	0.005	HSS FLEX+A	2	1.890	2.460	2.460	4.030
5	HSST3X3X0	HSST3X3X0	0.012	1.000	0.012	HSS BEND Z	4	1.890	2.460	2.460	4.030

Failed Members

There is no data of this type.

Statics Check Results

L/C		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1:DL	Loads	0.000	-0.066	0.000	0.791	0.000	-0.339
1:DL	Reactions	0.000	0.066	0.000	-0.791	0.000	0.339
	Difference	0.000	-0.000	0.000	0.000	0.000	-0.000
2:W1	Loads	0.028	0.000	-0.052	-0.389	0.336	-0.192
2:W1	Reactions	-0.028	-0.000	0.052	0.389	-0.336	0.192
	Difference	0.000	-0.000	-0.000	-0.000	0.000	0.000
3:0.75W2	Loads	0.022	0.000	-0.038	-0.288	0.264	0.144
3:0.75W2	Reactions	-0.022	-0.000	0.038	0.288	-0.264	-0.144
	Difference	0.000	-0.000	-0.000	-0.000	0.000	-0.000

Deflection

From the LTS 2017 Interim Revisions 10.4.2.2 the deflection allowed for a horizontal support is $L/150$. From Table 3 the greatest service load deflection, DL, is lower than the allowable, LTS.

Table 3:

Component	Beam	Span (ft)	Service (in)	LTS ($L/150$)	Check
MSE Wall	3	1.5	0	0.12	OK



STAAD Deflections



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Job No
148872000

Sheet No
1

Rev
3

Job Title **Pier Analysis**

Part

Ref

By **IERM** Date **05--Jun-18** Chd

Client **THEA**

File **THEA1.1-Pier.std**

Date/Time **19-Jul-2018 12:13**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
10	0.052	2.917	5	1630	-0.000	-0.075	-0.026
21	0.047	4.083	5	1803	0.001	-0.073	-0.022
10	0.046	2.917	8	1821	0.000	-0.067	-0.022
21	0.042	4.083	8	1984	0.001	-0.067	-0.017
21	0.035	4.083	4	2425	0.000	-0.054	-0.007
10	0.035	2.917	4	2425	-0.000	-0.054	-0.007
20	0.034	4.083	4	2457	0.000	-0.138	-0.007
4	0.034	2.917	4	2457	-0.000	-0.138	-0.007
10	0.030	2.917	6	2755	0.000	-0.046	-0.007
21	0.030	4.083	6	2757	0.001	-0.048	-0.005
20	0.030	4.083	6	2791	0.001	-0.120	-0.005
4	0.030	2.917	6	2793	0.001	-0.126	-0.007
4	0.018	2.917	8	4608	0.002	-0.091	-0.022
10	0.016	2.917	7	5355	0.000	-0.020	-0.016
20	0.016	4.083	7	5376	0.002	0.050	-0.011
20	0.015	4.083	8	5782	0.002	-0.071	-0.017
4	0.014	2.917	5	5984	0.002	-0.075	-0.027
4	0.012	2.917	7	7031	0.002	0.031	-0.017
21	0.012	4.083	7	7067	0.001	-0.020	-0.011
20	0.009	4.667	5	8886	0.001	-0.047	-0.017
2	0.003	0.750	4	5566	0.000	-0.016	-0.006
24	0.003	0.750	4	5566	-0.000	-0.016	-0.006
2	0.003	0.750	6	6280	0.001	-0.014	-0.006
24	0.003	0.750	6	6371	0.001	-0.016	-0.007
14	0.002	0.665	8	8253	0.001	-0.000	-0.002
14	0.002	0.665	5	8393	0.001	-0.000	-0.002
6	0.002	1.167	4	12746	-0.000	-0.010	-0.007
5	0.002	1.167	4	12746	0.000	-0.010	-0.007
11	0.002	0.665	4	9031	-0.001	-0.000	-0.002
14	0.002	0.665	4	9046	0.001	-0.000	-0.002
14	0.002	0.665	6	9219	0.001	-0.000	-0.002
24	0.002	0.750	8	10544	0.002	-0.021	-0.007
6	0.002	1.167	6	14069	0.000	-0.010	-0.007
2	0.002	0.750	8	11046	0.002	-0.017	-0.005
11	0.002	0.554	5	9909	-0.001	-0.000	-0.002
5	0.002	1.167	6	14924	0.001	-0.009	-0.006
11	0.002	0.665	8	9986	-0.000	-0.000	-0.001
11	0.002	0.665	6	10075	-0.000	-0.000	-0.001
6	0.001	1.167	8	16262	0.001	-0.011	-0.008
6	0.001	1.167	5	17639	0.001	-0.010	-0.007
24	0.001	0.750	5	13452	0.002	-0.021	-0.006
5	0.001	1.167	8	19297	0.001	-0.008	-0.006
2	0.001	0.750	7	14490	0.002	-0.003	0.000
2	0.001	0.750	5	15018	0.002	-0.018	-0.005
24	0.001	0.750	7	15474	0.002	-0.007	-0.001



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Job No
148872000

Sheet No
2

Rev
3

Job Title **Pier Analysis**

Part

Ref

By **IERM** Date **05--Jun-18** Chd

Client **THEA**

File **THEA1.1-Pier.std**

Date/Time **19-Jul-2018 12:13**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
5	0.001	1.167	5	20815	0.001	-0.008	-0.005
8	0.001	0.750	5	20967	0.001	0.003	-0.005
8	0.001	0.750	8	22173	0.001	0.003	-0.005
25	0.001	0.750	5	24726	0.000	0.003	-0.006
25	0.001	0.750	8	29743	0.000	0.002	-0.007
8	0.001	0.750	6	32121	0.000	0.002	-0.006
8	0.001	0.750	4	32493	0.000	0.002	-0.007
25	0.001	0.750	4	32493	-0.000	0.002	-0.007
5	0.000	1.167	7	57186	0.001	0.001	0.000
25	0.000	0.750	6	43511	0.000	0.002	-0.007
14	0.000	0.665	7	41340	0.000	-0.000	-0.001
8	0.000	0.750	7	51121	0.001	0.001	0.000
22	0.000	0.250	4	17812	0.000	-0.008	-0.006
3	0.000	0.250	4	17812	-0.000	-0.008	-0.006
11	0.000	0.554	7	47987	0.000	0.000	-0.000
22	0.000	0.250	6	19887	0.001	-0.008	-0.006
3	0.000	0.250	6	20601	0.001	-0.008	-0.007
6	0.000	1.333	7	113942	0.001	-0.001	-0.002
25	0.000	0.875	7	94232	0.001	0.001	-0.001
22	0.000	0.250	8	35808	0.002	-0.014	-0.006
3	0.000	0.250	8	37011	0.002	-0.015	-0.006
27	0.000	0.333	5	88692	-0.000	-0.324	-0.057
3	0.000	0.250	7	44638	0.002	-0.008	-0.000
22	0.000	0.250	7	46495	0.002	-0.008	-0.000
26	0.000	0.417	5	94446	0.002	-0.187	-0.058
3	0.000	0.250	5	49869	0.002	-0.017	-0.005
22	0.000	0.250	5	51145	0.002	-0.016	-0.005
27	0.000	0.417	8	113327	0.000	-0.295	-0.047
1	0.000	0.667	5	115401	0.001	-0.132	-0.048
26	0.000	0.417	8	118347	0.002	-0.235	-0.047
7	0.000	0.667	5	120711	0.001	-0.306	-0.048
1	0.000	0.667	7	141000	0.002	0.162	-0.030
27	0.000	0.333	7	142572	0.000	-0.092	-0.040
7	0.000	0.667	7	147374	0.001	-0.080	-0.030
26	0.000	0.333	7	147779	0.002	0.114	-0.040
1	0.000	0.667	8	155976	0.002	-0.184	-0.036
7	0.000	0.667	8	157097	0.001	-0.279	-0.036
23	0.000	0.250	5	86846	0.001	0.005	-0.005
23	0.000	0.250	8	92990	0.001	0.004	-0.006
9	0.000	0.250	5	93200	0.000	0.005	-0.005
9	0.000	0.250	8	116422	0.001	0.004	-0.006
15	0.000	0.105	5	110100	-0.000	-0.000	0.000
15	0.000	0.105	8	110100	-0.000	-0.000	0.000
7	0.000	0.583	4	266605	0.000	-0.230	-0.007
27	0.000	0.417	4	266693	-0.000	-0.230	-0.007



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Job No
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Sheet No
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Rev
3

Job Title **Pier Analysis**

Part

Ref

By **IERM** Date **05--Jun-18** Chd

Client **THEA**

File **THEA1.1-Pier.std**

Date/Time **19-Jul-2018 12:13**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
23	0.000	0.250	6	144893	0.000	0.003	-0.006
23	0.000	0.250	4	149434	0.000	0.003	-0.006
1	0.000	0.583	4	298962	0.000	-0.398	-0.007
26	0.000	0.417	4	298962	-0.000	-0.398	-0.007
27	0.000	0.417	6	301463	0.000	-0.200	-0.009
9	0.000	0.250	4	150801	-0.000	0.003	-0.006
7	0.000	0.583	6	303984	0.000	-0.204	-0.004
12	0.000	0.175	5	132120	0.000	-0.000	0.000
1	0.000	0.583	6	338634	0.001	-0.346	-0.004
26	0.000	0.417	6	340674	0.001	-0.358	-0.009
15	0.000	0.070	4	165150	-0.000	-0.000	0.000
16	0.000	0.125	8	294912	0.000	-0.000	0.000
12	0.000	0.140	8	165150	0.000	-0.000	0.000
15	0.000	0.070	6	165150	-0.000	-0.000	0.000
16	0.000	0.125	5	294912	0.000	-0.000	0.000
16	0.000	0.250	6	294912	0.000	-0.000	0.000
12	0.000	0.105	4	165150	0.000	-0.000	0.000
23	0.000	0.250	7	199474	0.001	0.001	-0.000
9	0.000	0.250	6	210266	0.000	0.003	-0.007
13	0.000	0.188	4	393216	-0.000	-0.000	0.000
13	0.000	0.313	8	393216	-0.000	-0.000	0.000
12	0.000	0.105	6	220200	0.000	-0.000	0.000
13	0.000	0.188	5	393216	-0.000	-0.000	0.000
9	0.000	0.250	7	363007	0.001	0.001	-0.000
31	0.000	0.750	8	781218	0.003	-0.041	-0.008
16	0.000	0.125	7	589824	0.000	-0.000	0.000
16	0.000	0.063	4	589824	0.000	-0.000	0.000
15	0.000	0.035	7	330301	-0.000	-0.000	0.000
13	0.000	0.188	6	589824	-0.000	-0.000	0.000
31	0.000	0.833	4	938431	0.000	-0.044	-0.007
29	0.000	0.458	4	524288	-0.000	-0.000	0.000
29	0.000	0.458	6	524288	-0.000	-0.000	0.000
31	0.000	0.417	7	1048576	0.003	-0.003	-0.002
29	0.000	0.417	7	589823	-0.000	-0.000	0.000
31	0.000	0.500	6	1454716	0.001	-0.037	-0.007
31	0.000	0.333	5	1968286	0.002	-0.032	-0.007
30	0.000	0.667	6	2149366	0.001	-0.036	-0.006
28	0.000	0.292	8	1179647	0.000	-0.000	0.000
29	0.000	0.042	8	1179647	0.000	-0.000	0.000
28	0.000	0.333	6	1179647	0.000	-0.000	0.000
28	0.000	0.333	5	1179647	0.000	-0.000	0.000
29	0.000	0.042	5	1179647	0.000	-0.000	0.000
30	0.000	0.500	8	2430076	0.002	-0.029	-0.006
30	0.000	0.333	4	3141637	-0.000	-0.035	-0.007
28	0.000	0.250	4	1572864	0.000	-0.000	0.000



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Job No
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Sheet No
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3

Job Title Pier Analysis

Part

Ref

By IERM Date 05--Jun-18 Chd

Client THEA

File THEA1.1-Pier.std

Date/Time 19-Jul-2018 12:13

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
30	0.000	0.500	7	314572	0.002	0.005	0.000
30	0.000	0.333	5	357186	0.001	-0.025	-0.005
12	0.000	0.000	7	0	0.000	0.000	0.000
28	0.000	0.000	7	0	0.000	0.000	0.000
13	0.000	0.000	7	0	0.000	0.000	0.000



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Job No
148872000

Sheet No
1

Rev
3

Job Title **Straddle Bent - Sides**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-Si** Date/Time **19-Jul-2018 11:27**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
9	0.002	1.458	4	12090	0.000	-0.003	0.000
8	0.002	1.458	4	12090	0.000	-0.003	0.000
8	0.002	1.458	5	13193	0.000	-0.003	-0.001
8	0.002	1.458	6	13323	0.000	-0.003	-0.001
9	0.002	1.458	6	17928	-0.000	-0.002	-0.001
9	0.002	1.458	5	19877	-0.000	-0.002	-0.001
9	0.001	1.458	3	56483	-0.000	0.000	-0.001
8	0.000	1.875	3	145781	0.000	-0.000	-0.000
4	0.000	0.292	5	277563	-0.000	-0.009	-0.002
1	0.000	0.292	5	306942	0.000	-0.013	-0.002
4	0.000	0.292	3	325401	-0.000	0.003	-0.002
1	0.000	0.292	3	341911	0.000	-0.001	-0.002
4	0.000	0.333	6	357166	-0.000	-0.009	-0.002
1	0.000	0.292	6	402637	0.000	-0.013	-0.002
1	0.000	0.292	4	469010	0.000	-0.014	0.000
4	0.000	0.292	4	469010	0.000	-0.014	0.000



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Job No
148872000

Sheet No
1

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
12	0.051	2.917	6	1641	0.006	-0.154	-0.021
20	0.046	4.083	6	1815	0.006	-0.149	-0.021
19	0.034	4.083	5	2441	0.000	-0.111	0.000
20	0.034	4.083	5	2441	0.000	-0.111	0.000
4	0.034	2.917	5	2441	-0.000	-0.111	0.000
12	0.034	2.917	5	2441	-0.000	-0.111	0.000
12	0.030	2.917	7	2773	0.002	-0.097	-0.000
20	0.030	4.083	7	2773	0.002	-0.097	-0.000
19	0.030	4.083	7	2774	0.002	-0.098	-0.000
4	0.030	2.917	7	2774	0.002	-0.098	-0.000
12	0.016	2.917	4	5391	0.006	-0.042	-0.016
19	0.016	4.083	4	5392	0.006	0.042	-0.016
4	0.014	2.917	6	5851	0.006	-0.046	-0.021
20	0.012	4.083	4	7101	0.006	-0.037	-0.016
4	0.012	2.917	4	7101	0.006	0.037	-0.016
19	0.010	4.667	6	8618	0.006	-0.031	-0.016
24	0.005	0.750	6	3936	0.006	0.019	-0.003
10	0.004	0.750	6	4063	0.006	0.019	-0.003
24	0.003	0.750	5	5470	-0.000	0.014	0.000
22	0.003	0.750	5	5470	-0.000	0.014	0.000
10	0.003	0.750	5	5470	-0.000	0.014	0.000
2	0.003	0.750	5	5470	-0.000	0.014	0.000
2	0.003	0.750	7	6149	0.002	0.012	-0.001
22	0.003	0.750	7	6191	0.002	0.012	-0.001
10	0.003	0.750	7	6242	0.002	0.012	-0.001
24	0.003	0.750	7	6286	0.002	0.012	-0.001
22	0.001	0.750	6	12955	0.006	0.005	-0.003
2	0.001	0.750	4	14495	0.006	-0.005	-0.002
24	0.001	0.750	4	14496	0.006	0.005	-0.002
2	0.001	0.750	6	14499	0.006	0.005	-0.003
15	0.001	1.250	6	29013	0.001	-0.000	-0.001
14	0.001	1.750	6	30220	0.001	-0.000	-0.001
16	0.001	1.250	6	30346	0.001	-0.000	-0.001
13	0.001	1.750	6	31546	0.001	-0.000	-0.001
15	0.001	1.250	4	31709	0.001	-0.000	-0.001
14	0.001	1.750	4	31924	0.001	0.000	-0.001
10	0.001	0.750	4	16050	0.006	0.005	-0.002
22	0.001	0.750	4	16050	0.006	-0.005	-0.002
16	0.001	1.250	4	32656	0.001	-0.000	-0.001
13	0.001	1.750	4	32890	0.001	0.000	-0.001
11	0.000	0.250	6	12302	0.006	0.031	-0.002
23	0.000	0.250	6	12384	0.006	0.031	-0.002
11	0.000	0.250	5	17111	-0.000	0.022	0.000
3	0.000	0.250	5	17111	-0.000	0.022	0.000
23	0.000	0.250	5	17111	-0.000	0.022	0.000



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Job No
148872000

Sheet No
2

Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
21	0.000	0.250	5	17111	-0.000	0.022	0.000
16	0.000	1.250	7	107760	0.000	-0.000	-0.000
15	0.000	1.250	7	109416	0.000	-0.000	-0.000
3	0.000	0.250	7	19050	0.002	0.020	-0.001
21	0.000	0.250	7	19096	0.002	0.020	-0.001
13	0.000	1.250	7	116348	0.001	-0.000	-0.000
14	0.000	1.250	7	116557	0.001	-0.000	-0.000
11	0.000	0.250	7	19806	0.002	0.019	-0.001
23	0.000	0.250	7	19854	0.002	0.019	-0.001
15	0.000	2.000	5	176395	0.000	-0.000	0.000
16	0.000	2.000	5	176395	0.000	-0.000	0.000
13	0.000	1.000	5	176947	0.000	-0.000	-0.000
14	0.000	1.000	5	176947	0.000	-0.000	-0.000
3	0.000	0.250	6	45136	0.006	0.008	-0.002
26	0.000	0.333	6	91851	0.006	-0.522	-0.049
25	0.000	0.417	6	92494	0.007	-0.155	-0.049
21	0.000	0.250	6	46247	0.006	0.008	-0.002
11	0.000	0.250	4	46884	0.006	0.008	-0.002
21	0.000	0.250	4	46886	0.006	-0.008	-0.002
3	0.000	0.250	4	47593	0.006	-0.008	-0.002
23	0.000	0.250	4	47610	0.006	0.008	-0.002
17	0.000	0.333	6	100576	0.006	0.000	-0.003
17	0.000	0.500	5	104895	0.000	0.000	0.000
18	0.000	0.500	5	104895	0.000	0.000	0.000
1	0.000	0.667	6	115917	0.006	-0.127	-0.049
17	0.000	0.500	7	117090	0.002	0.000	-0.000
18	0.000	0.417	6	120112	0.006	0.000	-0.003
9	0.000	0.667	6	120414	0.007	-0.496	-0.049
18	0.000	0.500	7	121024	0.002	0.000	-0.000
8	0.000	0.250	6	62501	0.006	-0.000	-0.003
6	0.000	0.292	6	67412	0.006	-0.000	-0.003
5	0.000	0.292	6	69526	0.006	-0.000	-0.003
1	0.000	0.667	4	142208	0.005	0.146	-0.037
26	0.000	0.333	4	144340	0.005	-0.146	-0.037
7	0.000	0.167	6	72788	0.006	-0.000	-0.003
9	0.000	0.667	4	145921	0.006	-0.125	-0.037
25	0.000	0.333	4	146412	0.006	0.125	-0.037
7	0.000	0.250	4	87217	0.006	-0.000	-0.003
5	0.000	0.292	4	91206	0.006	-0.000	-0.003
6	0.000	0.208	4	91424	0.006	0.000	-0.003
8	0.000	0.208	4	97790	0.006	0.000	-0.003
17	0.000	0.250	4	258043	0.006	0.000	-0.003
25	0.000	0.417	5	281970	-0.000	-0.374	0.000
9	0.000	0.583	5	281970	0.000	-0.374	0.000
1	0.000	0.583	5	281970	0.000	-0.374	0.000



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Job No
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Sheet No
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Rev
3

Job Title **Straddle Bent - Middle**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA2.1-StraddleBent-M** Date/Time **19-Jul-2018 08:31**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
26	0.000	0.417	5	281970	-0.000	-0.374	0.000
18	0.000	0.750	4	296433	0.006	0.000	-0.003
9	0.000	0.583	7	319705	0.002	-0.328	-0.000
26	0.000	0.417	7	319832	0.002	-0.327	-0.000
1	0.000	0.583	7	320838	0.002	-0.331	-0.000
25	0.000	0.417	7	320964	0.002	-0.331	-0.000
5	0.000	0.292	5	243337	0.000	-0.000	-0.000
7	0.000	0.292	5	243337	0.000	-0.000	-0.000
6	0.000	0.208	5	243337	0.000	-0.000	0.000
8	0.000	0.208	5	243337	0.000	-0.000	0.000
8	0.000	0.208	7	243986	0.002	-0.000	-0.000
7	0.000	0.292	7	260488	0.002	-0.000	-0.000
6	0.000	0.208	7	270853	0.002	-0.000	-0.000
5	0.000	0.292	7	282259	0.002	-0.000	-0.000



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Job Title **Abutment-Sides**

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By **IERM** Date **19-Jun-18** Chd

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File **THEA3- AbutmentSides.s** Date/Time **19-Jul-2018 13:26**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
9	0.001	1.458	4	29971	0.000	-0.001	0.000
8	0.001	1.458	4	29971	0.000	-0.001	0.000
8	0.001	1.458	5	31926	0.000	-0.001	-0.000
8	0.001	1.458	6	32764	0.000	-0.001	-0.000
9	0.001	1.458	6	49301	-0.000	-0.001	-0.000
9	0.001	1.458	5	56551	-0.000	-0.001	-0.000
9	0.000	1.458	3	108890	-0.000	0.000	-0.000
8	0.000	1.875	3	486952	0.000	-0.000	-0.000
4	0.000	0.292	5	826150	-0.000	-0.003	-0.001
4	0.000	0.292	3	915293	-0.000	0.001	-0.000
1	0.000	0.250	3	932096	0.000	-0.000	-0.000
1	0.000	0.250	5	106160	0.000	-0.006	-0.001
4	0.000	0.208	6	121879	-0.000	-0.004	-0.000
1	0.000	0.292	6	142999	0.000	-0.005	-0.000
1	0.000	0.292	4	148656	0.000	-0.006	0.000
4	0.000	0.292	4	148656	0.000	-0.006	0.000



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Job Title **Abutment Middle**

Part

Ref

By **IERM** Date **05-Jun-18** Chd

Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
10	0.052	2.917	5	1630	-0.000	-0.073	-0.025
18	0.047	4.083	5	1803	0.001	-0.070	-0.021
10	0.046	2.917	8	1820	-0.000	-0.065	-0.020
18	0.042	4.083	8	1984	0.001	-0.064	-0.016
18	0.035	4.083	4	2425	0.000	-0.052	-0.006
10	0.035	2.917	4	2425	-0.000	-0.052	-0.006
17	0.034	4.083	4	2457	0.000	-0.137	-0.006
4	0.034	2.917	4	2457	-0.000	-0.137	-0.006
10	0.030	2.917	6	2755	0.000	-0.045	-0.006
18	0.030	4.083	6	2756	0.000	-0.046	-0.004
17	0.030	4.083	6	2792	0.001	-0.118	-0.004
4	0.030	2.917	6	2793	0.001	-0.124	-0.006
4	0.018	2.917	8	4609	0.002	-0.088	-0.020
10	0.016	2.917	7	5355	0.000	-0.020	-0.015
17	0.016	4.083	7	5374	0.001	0.050	-0.012
17	0.015	4.083	8	5786	0.001	-0.070	-0.016
4	0.014	2.917	5	5986	0.001	-0.072	-0.025
4	0.012	2.917	7	7032	0.002	0.032	-0.016
18	0.012	4.083	7	7063	0.001	-0.019	-0.012
17	0.009	4.667	5	8895	0.001	-0.046	-0.016
2	0.003	0.750	4	5566	0.000	-0.014	-0.005
21	0.003	0.750	4	5566	-0.000	-0.014	-0.005
2	0.003	0.750	6	6280	0.001	-0.013	-0.005
21	0.003	0.750	6	6372	0.001	-0.014	-0.005
5	0.002	1.167	4	12746	0.000	-0.010	-0.005
6	0.002	1.167	4	12746	-0.000	-0.010	-0.005
21	0.002	0.750	8	10539	0.001	-0.019	-0.005
6	0.002	1.167	6	14066	0.000	-0.009	-0.005
2	0.002	0.750	8	11042	0.001	-0.015	-0.004
5	0.002	1.167	6	14924	0.001	-0.009	-0.005
6	0.001	1.167	8	16258	0.001	-0.010	-0.006
6	0.001	1.167	5	17650	0.000	-0.009	-0.006
21	0.001	0.750	5	13438	0.001	-0.019	-0.005
5	0.001	1.167	8	19309	0.001	-0.007	-0.004
2	0.001	0.750	7	14485	0.001	-0.003	0.001
2	0.001	0.750	5	14999	0.001	-0.016	-0.004
21	0.001	0.750	7	15467	0.001	-0.006	-0.000
5	0.001	1.167	5	20827	0.001	-0.007	-0.004
14	0.001	0.500	5	11060	0.001	-0.000	-0.002
14	0.001	0.500	8	11079	0.001	-0.000	-0.002
11	0.001	0.500	4	11626	-0.000	-0.000	-0.002
14	0.001	0.500	4	11626	0.000	-0.000	-0.002
14	0.001	0.500	6	12251	0.000	-0.000	-0.002
11	0.001	0.417	5	12709	-0.000	-0.000	-0.002
11	0.001	0.417	8	12933	-0.000	-0.000	-0.002



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Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
11	0.001	0.500	6	13147	-0.000	-0.000	-0.002
8	0.001	0.750	5	24349	0.001	0.003	-0.004
8	0.001	0.750	8	25886	0.001	0.002	-0.004
22	0.001	0.750	5	27400	0.000	0.002	-0.005
22	0.001	0.750	8	33037	0.000	0.002	-0.005
8	0.000	0.750	6	37522	0.000	0.002	-0.005
22	0.000	0.750	4	37615	-0.000	0.002	-0.005
8	0.000	0.750	4	37617	0.000	0.002	-0.005
5	0.000	1.333	7	57128	0.001	0.001	0.000
22	0.000	0.750	6	49819	0.000	0.001	-0.005
3	0.000	0.250	4	17812	-0.000	-0.006	-0.005
19	0.000	0.250	4	17812	0.000	-0.006	-0.005
8	0.000	0.750	7	58670	0.000	0.001	0.001
19	0.000	0.250	6	19886	0.001	-0.006	-0.005
3	0.000	0.250	6	20599	0.001	-0.007	-0.005
15	0.000	0.313	8	32907	-0.000	-0.000	0.000
15	0.000	0.313	5	34221	-0.000	-0.000	0.000
15	0.000	0.313	6	39056	-0.000	-0.000	0.000
15	0.000	0.250	4	40970	-0.000	-0.000	0.000
12	0.000	0.313	4	40970	0.000	-0.000	0.000
11	0.000	0.417	7	55397	0.000	0.000	0.000
6	0.000	1.500	7	115652	0.001	-0.001	-0.001
14	0.000	0.417	7	57959	0.000	-0.000	-0.001
12	0.000	0.250	5	46189	0.000	-0.000	0.000
12	0.000	0.250	6	46296	0.000	-0.000	0.000
22	0.000	0.750	7	93130	0.000	0.001	-0.000
12	0.000	0.250	8	46629	0.000	-0.000	0.000
19	0.000	0.250	8	35814	0.001	-0.012	-0.004
3	0.000	0.250	8	37005	0.001	-0.013	-0.005
3	0.000	0.250	7	44640	0.001	-0.008	0.000
24	0.000	0.417	5	89898	-0.000	-0.325	-0.055
19	0.000	0.250	7	46485	0.001	-0.007	0.000
23	0.000	0.417	5	94338	0.002	-0.183	-0.055
3	0.000	0.250	5	49871	0.001	-0.015	-0.004
19	0.000	0.250	5	51163	0.001	-0.014	-0.004
24	0.000	0.417	8	113768	-0.000	-0.291	-0.044
1	0.000	0.667	5	116090	0.001	-0.132	-0.048
23	0.000	0.417	8	117509	0.002	-0.232	-0.044
7	0.000	0.667	5	120720	0.001	-0.300	-0.048
16	0.000	0.313	8	104987	0.000	-0.000	-0.000
1	0.000	0.667	7	140482	0.001	0.161	-0.031
24	0.000	0.333	7	140654	-0.000	-0.091	-0.039
7	0.000	0.667	7	145351	0.001	-0.078	-0.031
15	0.000	0.250	7	109058	-0.000	-0.000	0.000
16	0.000	0.313	5	109527	0.000	-0.000	-0.000



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File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
23	0.000	0.333	7	148287	0.002	0.116	-0.039
1	0.000	0.667	8	157273	0.001	-0.183	-0.036
16	0.000	0.313	4	119775	0.000	-0.000	-0.000
16	0.000	0.250	6	119775	0.000	-0.000	-0.000
7	0.000	0.667	8	159738	0.001	-0.274	-0.036
13	0.000	0.313	4	124345	-0.000	-0.000	-0.000
13	0.000	0.313	8	138067	-0.000	-0.000	-0.000
13	0.000	0.313	6	143053	-0.000	-0.000	-0.000
13	0.000	0.250	5	146036	-0.000	-0.000	-0.000
20	0.000	0.250	5	101285	0.000	0.004	-0.004
9	0.000	0.250	5	110458	0.000	0.004	-0.004
20	0.000	0.250	8	111048	0.000	0.003	-0.004
7	0.000	0.583	4	266230	0.000	-0.226	-0.006
24	0.000	0.417	4	266230	-0.000	-0.226	-0.006
9	0.000	0.250	8	141945	0.000	0.003	-0.005
23	0.000	0.417	4	299312	-0.000	-0.397	-0.006
1	0.000	0.583	4	299312	0.000	-0.397	-0.006
24	0.000	0.417	6	301951	0.000	-0.197	-0.007
7	0.000	0.583	6	303230	0.000	-0.200	-0.004
1	0.000	0.583	6	339229	0.001	-0.345	-0.004
23	0.000	0.417	6	341089	0.001	-0.355	-0.007
20	0.000	0.250	6	176973	0.000	0.002	-0.005
9	0.000	0.250	4	188035	-0.000	0.002	-0.005
20	0.000	0.250	4	190781	0.000	0.002	-0.005
16	0.000	0.250	7	327175	0.000	-0.000	-0.000
20	0.000	0.250	7	228047	0.000	0.001	0.000
9	0.000	0.250	6	280054	0.000	0.002	-0.005
9	0.000	0.250	7	414572	0.000	0.001	0.000
31	0.000	0.583	8	101907	0.002	-0.035	-0.006
26	0.000	0.458	4	517154	-0.000	-0.000	0.000
31	0.000	0.750	6	103629	0.001	-0.039	-0.005
31	0.000	0.917	5	104713	0.003	-0.038	-0.006
26	0.000	0.417	7	585269	-0.000	-0.000	0.000
31	0.000	0.917	4	134425	0.000	-0.043	-0.005
26	0.000	0.417	6	746074	-0.000	-0.000	0.000
30	0.000	0.833	8	185507	0.001	-0.031	-0.004
30	0.000	0.833	5	185510	0.000	-0.029	-0.004
30	0.000	0.917	4	208249	-0.000	-0.043	-0.005
30	0.000	0.750	7	209715	0.001	0.006	0.000
26	0.000	0.292	8	108074	-0.000	-0.000	0.000
25	0.000	0.417	8	110453	0.000	-0.000	0.000
26	0.000	0.208	5	112595	-0.000	-0.000	0.000
25	0.000	0.333	5	114442	0.000	-0.000	0.000
25	0.000	0.458	6	115944	0.000	-0.000	0.000
25	0.000	0.333	4	117964	0.000	-0.000	0.000



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Job Title **Abutment Middle**

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Client **THEA**

File **THEA3 - AbutmentMiddle** Date/Time **19-Jul-2018 11:06**

Cont...

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
31	0.000	0.083	7	235929€	0.002	-0.002	-0.001
30	0.000	0.500	6	242978€	0.001	-0.032	-0.005
12	0.000	0.000	7	0	0.000	0.000	0.000
13	0.000	0.000	7	0	0.000	0.000	0.000
25	0.000	0.000	7	0	0.000	0.000	0.000



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Sheet No
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Rev
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Job Title **Retaining Wall 2**

Part

Ref

By **IERM** Date **19-Jun-18** Chd

Client **THEA**

File **THEA4- Retaining WallHC** Date/Time **19-Jul-2018 11:20**

Beam	Max Disp (in)	Location (ft)	L/C	L/Displ	Global X (in)	Global Y (in)	Global Z (in)
3	0.000	0.875	6	54505	0.000	-0.000	-0.000
3	0.000	0.875	5	68636	0.000	-0.000	-0.000
5	0.000	0.875	4	71615	-0.000	-0.000	0.000
3	0.000	0.875	4	71615	-0.000	-0.000	0.000
5	0.000	0.875	6	93336	-0.000	-0.000	-0.000
3	0.000	0.875	3	163654	0.000	-0.000	-0.000
5	0.000	0.875	5	226956	-0.000	-0.000	-0.000
5	0.000	1.250	3	481906	-0.000	0.000	-0.000
4	0.000	0.292	6	598223	-0.000	-0.001	-0.000
1	0.000	0.292	6	687820	0.000	-0.002	-0.000
4	0.000	0.208	3	857749	-0.000	0.000	-0.000
4	0.000	0.208	5	922813	-0.000	-0.001	-0.000
1	0.000	0.250	5	1006317	0.000	-0.002	-0.000
1	0.000	0.292	3	1094606	0.000	-0.001	-0.000
1	0.000	0.292	4	1342177	0.000	-0.002	0.000
4	0.000	0.292	4	1342177	0.000	-0.002	0.000



Weld Connection Design

Summary:

The following calculation demonstrates the AISC 14th edition check for the welds at the plates and the HSS member check. The weld was checked for the Dyno Drum HO since it has a higher load than the SO.

The following weld calculations are based on:

1. AISC LRFD Manual 14th edition
2. Analyzed as a simply supported beam with fixed connections at both ends
3. The loads orientation are based off the weld

Load Combinations:

1. 1.4DL
4. 1.2DL+1.0W

Luminaire (Dyno Drum HO):

Fz: 1.4(30 lb) = 42 lb

Fx: 1.0(52.2 lb) = 52.2 lb

Fy: 1.0*(27.7 lb) = 27.7 lb

M = PL/8 L = 3ft (From Pier)

My: ((42 lb)*(3ft))/8+(1.24'/2*12")*(52.2lb) = -404.1 lb*in = -0.404 kip*in

Mx: -(1.24'/2*12")*(27.7lb) = -206.08 lb*in = 0.206 kip*in

Mz: None

Flexure Check:

Plate A36 Fy=36 ksi t=1/4"

f = Mc/I P = 42 lb

I = bh³/12 = 12"*(0.25")³/12 = 0.01562 in⁴

c = 0.25"/2 = 0.125"

f = (0.404 kip*in)*(0.125")/(0.01562 in⁴) = 0.323 ksi < 36 ksi OK

Assumed: Weld design for HO Dyno Drum is used for SO of a less weight.

Available Strength of Weld:

AISC (EQ 8-1)

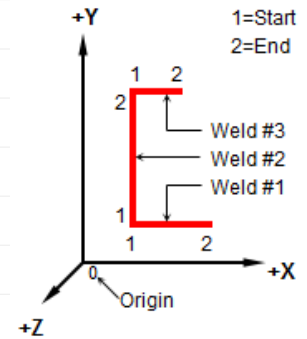
Estimating that the weld is 3/16" since the HSS thickness is 3/16".

AISC(J2-2b-a)

0.75*Rn = 1.392*D*L L=4" (Length of weld estimated)

Rn = 1.392*(3")*(4")= 16.7 kips

0.75*16.7 kip= 12.5 kips > Pu = 0.042 lb, Pu = 0.0522 lb OK



AISC (Table 3-23)



Connection Design
Straddle Bent Middle
Abutment Sides
MSE Wall

A. SPECIFICATIONS :

1. GENERAL SPECIFICATIONS:
 - a. Florida Department of Transportation Standard Specifications for Road and Bridge Construction (2000 Edition) and Supplements Thereto.
 - b. Brandon Parkway, Project Specific, Special Provisions.
2. DESIGN SPECIFICATIONS:
 - a. AASHTO Standard Specifications for Highway Bridges, 19th Edition, 1996, thru 1999 Interims.
 - b. AASHTO Standard Specifications for Design and Construction of Segmental Concrete Bridges, Second Edition, 1999.
 - c. CEB-FIP "Model Code for Concrete Structures", Third Edition, 1978, Appendix E: Time Dependent Behavior of Concrete, Creep and Shrinkage.

B. DESIGN LOADINGS :

1. DEAD LOADS :
 - a. Unit weight of reinforced concrete: 150 pcf.
 - b. Future wearing surface: 15 pcf.
 - c. Exterior Concrete Barriers: 620 p.l.f. (Each)
 - d. Utilities : 150 p.lf (Longitudinal)
20 p.lf (Transverse)
2. LIVE LOADS : IPer AASHTO
 - a. HS20-44 with impact:
 - b. 47'-0" Wide Box - Three (3) Design Lanes
 - c. 59'-0" Wide Box - Four (4) Design Lanes
 - d. Alternate Military Loading (Single Vehicle)
 - e. Design Speed: 65 mph
3. WIND LOADS : As Per AASHTO
4. THERMAL FORCES : Ambient Temperature + 70 °F
 - For Design:
 - Temperature Rise + 30 °F
 - Temperature Fall - 40 °F
 - For sizing bearings and joints: Temperature Rise and Fall as per AASHTO.

Differential Temperature for Continuous Structures:
 In Accordance With AASHTO Guide Specifications for Thermal Effects in Concrete Bridge Superstructure and AASHTO Guide Specifications for Concrete Segmental Bridges.

Load Combinations as Follows:
 (1) Dead load + full differential temperature
 (2) Dead load + live load + half differential temperature

6. CREEP AND SHRINKAGE : Strains are calculated in accordance with the CEB-FIP Model Code
1. Mean Annual Relative Humidity for Design: 75%.
2. Minimum Age of Precast Elements at Erection: 28 Days.

7. EARTHQUAKE : Seismic Performance Category A - in accordance with AASHTO.
8. ERECTION LOADS : in Accordance With AASHTO Guide Specification for Segmental Concrete Bridges. See erection drawings and specifications.

C. ENVIRONMENT :

1. SUBSTRUCTURE: Moderately Aggressive.
2. SUPERSTRUCTURE: (A) Slightly Aggressive, (B) PT Tendon Grouting Exposure. Contractor to use an Enhanced Grout as Described in the Specifications.

D. MATERIALS :

1. CONCRETE : I28 Day Specified Compressive Strength, f'c :
 - a. Drilled Shafts: Class IV Drilled Shafts (4,500 psi).
 - b. Pier: 162 to 161 use Class VI (8,500 psi concrete) and Piers: Class IV (6,500 psi).
 - c. Superstructure and Straddle Bent Beam - Box Girder, Straddle Bent Beam and C.I.P. Joints: Class V (Special) (6,000 psi).
 - d. CIP Barriers and Parapets: Class IIIa (4,500 psi).
 - e. 3/4" Chamfers to be provided on all exposed concrete edges (Unless Otherwise Noted).
 - f. 1/4" maximum aggregate size shall be used for all precast components.

E. ALLOWABLE STRESSES / LOADS :

1. REINFORCED CONCRETE : As per AASHTO
 - a. Transverse concrete stress : 3√f'c, tension
0.40f'c, compression
 - b. Longitudinal concrete stress : 0 psi, compression (Type A Epoxy Joints)
0.60f'c, compression (All Service Load Combinations)
0.45f'c, compression (Dead Load & Post-tensioning)
2. PRESTRESSED CONCRETE :
 - a. Principal concrete stress : 4√f'c, tension

F. CONSTRUCTION :

1. All construction schematic drawings are represented as an aid to the Contractor in developing a segmental construction procedure and are not to be considered working drawings. All details of contractor's construction shall be approved by the Engineers for review and approval prior to implementation.
2. The contractor shall be solely responsible for the means and methods of construction.
3. Protection of Existing I-75 Loop, Ramp 'D' Structure shall be Provided in Accordance with FDOT Specifications, Section 455-1.1.

G. PAY ITEM NOTES :

1. Item No. 110-3 includes the removal and disposal of existing Eastbound and Westbound bridge structures including but not limited to bridge deck, concrete slabs, wingwalls, and slope pavement. Refer to General Plan and Elevation drawing of the Lee Roy Selmon Crossspan Expressway, Reversible Lanes Bridge, Existing and Proposed Eastbound and Westbound, 38th St. Bridge (Bridge #100452) approximate deck area to be removed 9180 sq. ft.
2. Removal and replacement of existing Slope Pavement, Barriers and Walls at Cross Streets and Railroads, including, but not limited to: barricading (specifically related to slope pavements and barriers of cross streets and railroads), and replacement of Slope Pavement, Barriers, Walls and clean-up, shall be paid for separately and shall be incidental to the cost of the Drilled Shafts.
3. Removal and replacement of existing surfaces and elements that are disturbed due to construction operations including, but not limited to: (specifically related to areas disturbed by piers and not included in overall MOT Plan), temporary signage (if required), restoration of surfaces and elements to their original condition to the design of the Drilled Shafts.
4. Temporary containment and channeling of drainage runoff from new elevated roadway to prevent spillage to active lanes below shall be provided until permanent barrier walls constructed. Materials and methods of construction shall be subject to the review and approval of Engineer. Temporary containment materials, installation and subsequent removal/disposal shall be paid for separately and shall be incidental to the overall cost of the Project.

H. STRUCTURE NUMBERS :

1. Structure No. 100800 includes Abutment 124 through Abutment 173.
2. Structure No. 100806 includes Abutment 1 through Abutment 123.
3. Structure No. 100812 includes Abutment 201 through Abutment 225.

I. ABBREVIATIONS :

Abb.	Meaning	Abb.	Meaning
Abut.	Abutment	L.S.	Lump Sum
B.F.	Back Face	Max.	Maximum
Bas.	Baseline	Min.	Minimum
Bot.	Bottom	M.H.W.	Mean High Water
Brg.	Bearing	M.L.W.	Mean Low Water
C.J.	Closure Joint	O.F.	Outside Face
Cl.	Clear	P.C.	Point of Curve
¢	Centerline	P.G.L.	Profile Grade Line
Cts.	Centers	P.I.	Point of Intersection
Cu. Yds.	Cubic Yards	P.T.	Point of Tangent
D.	Delta	P.V.C.	Point of Vertical Curve
∆	Expansion Bearing	P.V.I.	Point of Vertical Intersection
E	Each	P.R.C.T.	Point of Reverse Curve
E.E.	Each End	R	Radius
E.F.	Each Face	Rdwy.	Roadway
E.J.	Expansion Joint	S.H.	Shoulder
E.W.	Each Way	Spa.	Space
F	Fixed Bearing	Sq. Yds.	Square Yards
F.F.	Front Face	Sta.	Station
F.F.B.W.	Front Face Back Wall	Symm.	Symmetrical
I.F.	Inside Face	T	Tangent Length
Lbs.	Pounds	Typ.	Typical
L.F.	Linear Foot		

J. GENERAL NOTES :

STRUCTURE NOS. 100800, 100806 & 100812

TAMPA - HILLSBOROUGH COUNTY EXPRESSWAY AUTHORITY		PROJECT NAME	
FORM NO. S.R. 618	COUNTY HILLSBOROUGH	CONSTRUCTION PROJECT NO. THCEA 5140.01	DATE 1-8

REVISIONS		ENGINEER OF RECORD	
DATE	BY	DATE	NAME
		12-13-02	J.M.F.
		12-13-02	AWK
		12-13-02	WJP
		12-13-02	AWK
			J. Rodriguez

LOGO		SEAL	

1. STRUCTURE NOS. 100800 includes Abutment 124 through Abutment 173.
 2. Structure No. 100806 includes Abutment 1 through Abutment 123.
 3. Structure No. 100812 includes Abutment 201 through Abutment 225.

STRUCTURE NOS. 100800, 100806 & 100812
 SEGMENTAL BRIDGES BETWEEN TWIGGS ST & 78TH ST AND GATEWAY BRIDGE



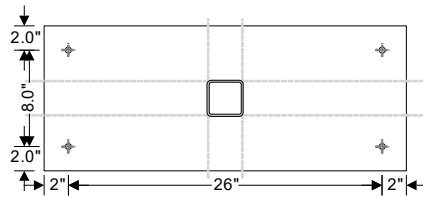
Undercut Anchor Tedds Design

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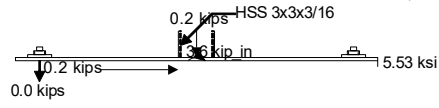
COLUMN BASE PLATE DESIGN

In accordance with AISC Steel Design Guide 1 and AISC 360-10

Tedds calculation version 2.1.02



Plan on baseplate



Elevation on baseplate

Bolt diameter - 0.5"
Bolt embedment - 4.0"
Flange/base weld - 0.2"
Web/base weld - 0.2"

Design forces and moments

Axial force	$P_u = 0.2$ kips (Compression)
Bending moment	$M_u = 3.6$ kip_in
Shear force	$F_v = 0.2$ kips
Eccentricity	$e = \text{ABS}(M_u / P_u) = 23.571$ in
Anchor bolt to center of plate	$f = N/2 - e_1 = 13.000$ in

Column details

Column section	HSS 3x3x3/16
Depth	$d = 3.000$ in
Breadth	$b_f = 3.000$ in
Thickness	$t = 0.174$ in

Baseplate details

Depth	$N = 30.000$ in
Breadth	$B = 12.000$ in
Thickness	$t_p = 0.250$ in
Design strength	$F_y = 36.0$ ksi

Foundation geometry

Member thickness	$h_a = 36.000$ in
Dist center of baseplate to left edge foundation	$x_{ce1} = 24.000$ in
Dist center of baseplate to right edge foundation	$x_{ce2} = 24.000$ in
Dist center of baseplate to bot edge foundation	$y_{ce1} = 30.000$ in
Dist center of baseplate to top edge foundation	$y_{ce2} = 15.000$ in

Holding down bolt and anchor plate details

Total number of bolts	$N_{\text{bolt}} = 4$
Bolt diameter	$d_o = 0.500$ in
Bolt spacing	$s_{\text{bolt}} = 8.000$ in
Edge distance	$e_1 = 2.000$ in
Minimum tensile strength, base plate	$F_y = 36$ ksi
Minimum tensile strength, column	$F_{y\text{Col}} = 50$ ksi
Compressive strength of concrete	$f'_c = 5$ ksi

Strength reduction factors

Compression	$\phi_c = 0.65$
Flexure	$\phi_b = 0.90$

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Weld shear

$$\phi_v = 0.75$$

Plate cantilever dimensions

Area of base plate

$$A_1 = B \times N = 360.000 \text{ in}^2$$

Maximum area of supporting surface

$$A_2 = (N + 2 \times l_{\min}) \times (B + 2 \times l_{\min}) = 1440.000 \text{ in}^2$$

Nominal strength of concrete under base plate

$$P_p = 0.85 \times f'_c \times A_1 \times \min(\sqrt{A_2 / A_1}, 2) = 3060.0 \text{ kips}$$

Bending line cantilever distance m

$$m = (N - 0.95 \times d) / 2 = 13.575 \text{ in}$$

Bending line cantilever distance n

$$n = (B - 0.95 \times b_f) / 2 = 4.575 \text{ in}$$

Maximum bending line cantilever

$$l = \max(m, n) = 13.575 \text{ in}$$

Check eccentricity

Maximum bearing stress

$$f_{p,\max} = 0.85 \times f'_c \times \phi_c \times \min(\sqrt{A_2 / A_1}, 2) = 5.52 \text{ ksi}$$

Maximum bearing pressure

$$q_{\max} = f_{p,\max} \times B = 66.3 \text{ kips/in}$$

Critical eccentricity

$$e_{\text{crit}} = N / 2 - P_u / (2 \times q_{\max}) = 14.999 \text{ in}$$

e > e_{crit} so loads cannot be resisted by bearing alone. Therefore consider as a large moment

Plate dimensions adequate as $(f + N/2)^2 \geq (2 \times P_u \times (e + f)) / q_{\max}$ and a real solution for bearing length exists

Bearing length - quadratic solution 1

$$Y_1 = (f + N/2) + \sqrt{((f + N/2)^2 - (2 \times P_u \times (e + f)) / q_{\max})} = 55.997 \text{ in}$$

Bearing length - quadratic solution 2

$$Y_2 = (f + N/2) - \sqrt{((f + N/2)^2 - (2 \times P_u \times (e + f)) / q_{\max})} = 0.003 \text{ in}$$

Bearing length

$$Y = \min(Y_1, Y_2) = 0.003 \text{ in}$$

Tension force in bolts

$$T_u = q_{\max} \times Y - P_u = 0.0 \text{ kips}$$

Max tension in single bolt

$$T_{\text{rod}} = T_u / (N_{\text{bolt}} / 2) = 0.0 \text{ kips}$$

Base plate yielding limit at bearing interface

Required plate thickness

$$t_{p,\text{req}} = \sqrt{((4 \times f_{p,\max} \times Y \times (1 - Y/2)) / (\phi_b \times F_y))} = 0.168 \text{ in}$$

PASS - Thickness of plate exceeds required thickness

Base plate yielding limit at tension interface

Distance from bolt CL to plate bending lines

$$x = \text{abs}(m - e_1) = 11.575 \text{ in}$$

Plate thickness required

$$t_{p,\text{req}} = 2.11 \times \sqrt{((T_u \times x) / (B \times F_y))} = 0.075 \text{ in}$$

PASS - Thickness of plate exceeds required thickness

Combined tension and bending in anchor bolts

Gross cross sectional area of anchor

$$A_{\text{bolt}} = \pi \times d_a^2 / 4 = 0.196 \text{ in}^2$$

Thickness of washer

$$t_{\text{wash}} = 0.250 \text{ in}$$

Shear stress in anchor

$$f_v = F_v / (N_{\text{boltV}} \times A_{\text{bolt}}) = 0.45 \text{ ksi}$$

Lever arm

$$z = t_p + t_{\text{wash}} / 2 = 0.375 \text{ in}$$

Bending in anchor

$$M_l = F_v \times z / N_{\text{boltV}} = 0.00 \text{ kips_ft}$$

Plastic modulus of anchor

$$Z_{\text{bolt}} = d_a^3 / 6 = 0.021 \text{ in}^3$$

Stress in anchor due to bending

$$f_{\text{tb}} = M_l / Z_{\text{bolt}} = 1.6 \text{ ksi}$$

Axial stress in anchor

$$f_{\text{ta}} = T_{\text{rod}} / A_{\text{bolt}} = 0.1 \text{ ksi}$$

Tensile stress in anchor

$$f_t = f_{\text{tb}} + f_{\text{ta}} = 1.7 \text{ ksi}$$

Nominal tensile stress of anchor (Table J3.2)

$$F_{\text{nt}} = 0.75 \times f_{\text{uta}} = 43.5 \text{ ksi}$$

Nominal shear stress of anchor (Table J3.2)

$$F_{\text{nv}} = 0.45 \times f_{\text{uta}} = 26.1 \text{ ksi}$$

Tensile stress of anchor

$$\phi F_{\text{nt}} = \phi \times F_{\text{nt}} = 32.6 \text{ ksi}$$

Modified tensile stress (Eqn J3-3a)

$$\phi F'_{\text{nt}} = \min(\phi \times (1.3 \times F_{\text{nt}} - (F_{\text{nt}} / (\phi \times F_{\text{nv}})) \times f_v), \phi F_{\text{nt}}) = 32.6 \text{ ksi}$$

PASS - Combined shear and bending resistance of rods exceed tensile stress in rods

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Tension weld

Tension flange weld leg length

$$t_{wf} = 0.1875 \text{ in}$$

Effective flange weld width

$$l_{T_{weld,eff}} = l_{T_{weld,eff,ud}} = 2 \text{ in}$$

Tensile load per inch

$$R_{wf} = T_{rod} / l_{T_{weld,eff}} = 0.0 \text{ kips/in}$$

Electrode classification number

$$F_{EXX} = 70.0 \text{ ksi}$$

Design weld stress

$$\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(90\text{deg}))^{1.5}) = 47.250 \text{ ksi}$$

Design strength of weld per in

$$\phi R_{nf} = \phi F_{nw} \times t_{wf} / \sqrt{2} = 6.3 \text{ kips/in}$$

PASS - Available strength of weld exceeds force in tension weld

Local stress on flange

$$f_{T,local} = (T_{rod}) / (l_{T_{weld,eff}} \times t_r) = 0.068 \text{ ksi}$$

Column flange allowable stress

$$F_{yCol} / 1.67 = 29.940 \text{ ksi}$$

PASS - Local column capacity exceeds local column stress

Shear weld

Shear web weld leg length

$$t_{ww} = 0.1875 \text{ in}$$

Shear web weld force per in

$$R_{wf} = F_v / (2 \times (d - 2 \times t)) = 0.033 \text{ kips/in}$$

Electrode classification number

$$F_{EXX} = 70.0 \text{ ksi}$$

Design weld stress

$$\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(0\text{deg}))^{1.5}) = 31.500 \text{ ksi}$$

Design strength of weld per in

$$\phi R_{nl} = \phi F_{nw} \times t_{ww} / \sqrt{2} = 4.2 \text{ kips/in}$$

PASS - Available strength of shear weld exceeds force in shear weld

ANCHOR BOLT DESIGN

In accordance with ACI318-11

Tedds calculation version 2.1.02

Anchor bolt geometry

Type of anchor bolt

Cast-in headed end bolt anchor

Diameter of anchor bolt

$$d_a = 0.5 \text{ in}$$

Number of bolts in x direction

$$N_{boltx} = 2$$

Number of bolts in y direction

$$N_{bolty} = 2$$

Total number of bolts

$$n_{total} = (N_{boltx} \times 2) + (N_{bolty} - 2) \times 2 = 4$$

Total number of bolts in tension

$$n_{tens} = (N_{boltN} \times 2) + (N_{bolty} - 2) = 2$$

Spacing of bolts in x direction

$$s_{boltx} = 26 \text{ in}$$

Spacing of bolts in y direction

$$s_{bolty} = 8 \text{ in}$$

Number of threads per inch

$$n_t = 13$$

Effective cross-sectional area of anchor

$$A_{se} = \pi / 4 \times (d_a - 0.9743 \text{ in} / n_t)^2 = 0.142 \text{ in}^2$$

Embedded depth of each anchor bolt

$$h_{ef} = 4 \text{ in}$$

Material details

Minimum yield strength of steel

$$f_{ya} = 36 \text{ ksi}$$

Nominal tensile strength of steel

$$f_{uta} = 58 \text{ ksi}$$

Compressive strength of concrete

$$f_c = 5 \text{ ksi}$$

Concrete modification factor

$$\lambda = 1.00$$

Modification factor for cast-in anchor concrete failure

$$\lambda_a = 1.0 \times \lambda = 1.00$$

Strength reduction factors

Tension of steel element

$$\phi_{t,s} = 0.75$$

Shear of steel element

$$\phi_{v,s} = 0.65$$

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Concrete tension $\phi_{t,c} = 0.65$
Concrete shear $\phi_{v,c} = 0.70$
Concrete tension for pullout $\phi_{t,cB} = 0.70$
Concrete shear for pryout $\phi_{v,cB} = 0.70$

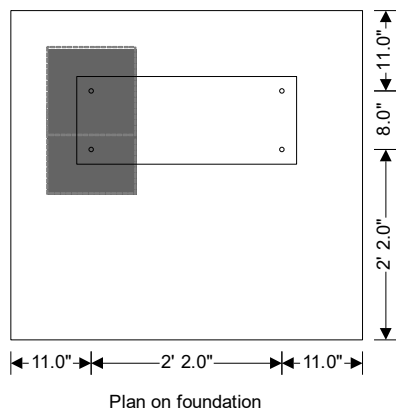
Steel strength of anchor in tension (D.5.1)

Nominal strength of anchor in tension $N_{sa} = A_{se} \times f_{uta} = 8.23$ kips
Steel strength of anchor in tension $\phi N_{sa} = \phi_{t,s} \times N_{sa} = 6.17$ kips

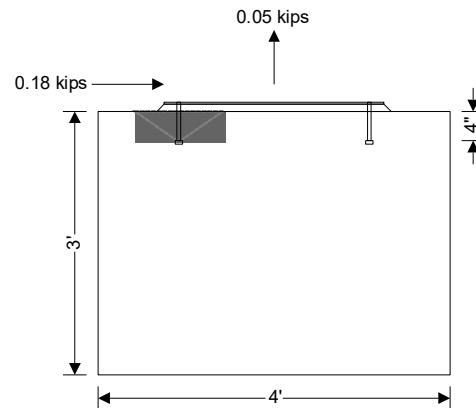
PASS - Steel strength of anchor exceeds max tension in single bolt

Check concrete breakout strength of anchor bolt in tension (D.5.2)

The spacing and embedded depth of the bolts/anchors are such that the projected area of all the anchors do not overlap. The concrete breakout strength of the anchors will therefore be based on a single anchor with the maximum axial force to a single anchor



Plan on foundation



Section A-A

Concrete breakout - tension

Single anchor

Applied axial force $N_s = N_{max,s} = 0.02$ kips
Eccentricity $e'_N = 0$ in
Coeff for basic breakout strength in tension $k_c = 24$
Breakout strength for single anchor in tension $N_b = k_c \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times h_{ef}^{1.5} \times 1 \text{ in}^{0.5} = 13.58$ kips
Projected area for groups of anchors $A_{Nc} = 144$ in²
Projected area of a single anchor $A_{Nco} = 9 \times h_{ef}^2 = 144$ in²
Min dist center of anchor to edge of concrete $C_{a,min} = 11$ in
Mod factor for groups loaded eccentrically $\psi_{ec,N} = \min(1 / (1 + ((2 \times e'_N) / (3 \times h_{ef}))), 1) = 1.000$
Modification factor for edge effects $\psi_{ed,N} = 1.0 = 1.000$
Modification factor for no cracking at service loads $\psi_{c,N} = 1.000$
Modification factor for cracked concrete $\psi_{cp,N} = 1.000$
Nominal concrete breakout strength $N_{cb} = A_{Nc} / A_{Nco} \times \psi_{ed,N} \times \psi_{c,N} \times \psi_{cp,N} \times N_b = 13.58$ kips
Concrete breakout strength $\phi N_{cb} = \phi_{t,c} \times N_{cb} = 8.82$ kips

PASS - Breakout strength exceeds tension in bolts

Pullout strength (D.5.3)

Net bearing area of the head of anchor $A_{brg} = 1$ in²

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Mod factor for no cracking at service loads $\psi_{c,P} = 1.000$
 Pullout strength for single anchor $N_p = 8 \times A_{brg} \times f_c = 40.00$ kips
 Nominal pullout strength of single anchor $N_{pn} = \psi_{c,P} \times N_p = 40.00$ kips
 Pullout strength of single anchor $\phi N_{pn} = \phi_{t,CB} \times N_{pn} = 28.00$ kips

PASS - Pullout strength of single anchor exceeds maximum axial force in single bolt

Side face blowout strength (D.5.4)

As $h_{ef} \leq 2.5 \times \min(c_{a1}, c_{a2})$ the edge distance is considered to be far from an edge and blowout strength need not be considered

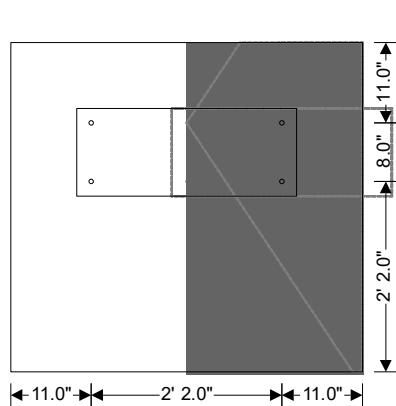
Steel strength of anchor in shear (D.6.1)

Built-up grout pads are used so nominal strength will be multiplied by 0.8 (D.6.1.3)

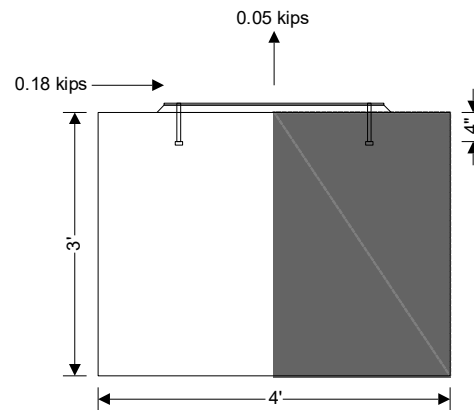
Effective number of anchors in shear $N_{boltV} = 2$
 Nom strength of anchor in shear $V_{sa} = 0.8 \times N_{boltV} \times 0.6 \times A_{se} \times f_{uta} = 7.90$ kips
 Steel strength of anchor in shear $\phi V_{sa} = \phi_{v,s} \times V_{sa} = 5.14$ kips

PASS - Steel strength of anchor exceeds shear in bolts

Concrete breakout strength in shear perpendicular to edge - Case 2. All shear resisted by rear bolts (D.6.3)



Plan on foundation



Section A-A

Concrete breakout - shear

The anchors are influenced by three or more edges where any edge distance is less than $1.5c_{a1}$ so value of c_{a1} is limited to c'_{a1} (D.6.2.4).

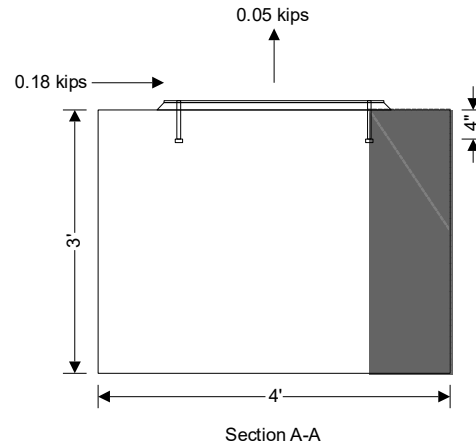
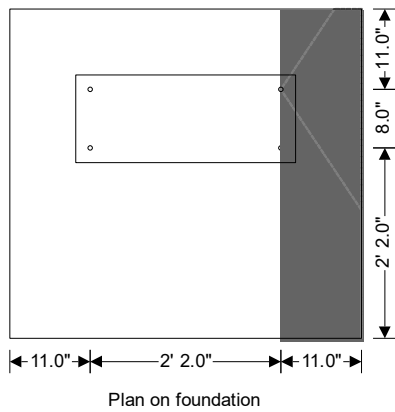
Bolt offset for limiting shear $x_{V,r} = 13.00$ in
 Limiting edge distance $c'_{a1} = 24$ in
 Applied shear $V_{app} = V = 0.18$ kips
 Edge distance x for shear near corner $c_{a1} = 37$ in
 Edge distance y for shear near corner $c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{bolty} - 1)/2) \times s_{bolty}) = 11$ in
 Load bearing length of anchor $l_e = \min(h_{ef}, 8 \times d_a) = 4$ in
 Basic concrete breakout strength $V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f_c \times 1 \text{ psi}} \times (c'_{a1})^{1.5} = 62.37$ kips
 $V_{b2} = 9 \times \lambda_a \times \sqrt{f_c \times 1 \text{ psi} \times 1 \text{ in}} \times (c'_{a1})^{1.5} = 74.82$ kips
 Basic concrete breakout strength $V_b = \text{Min}(V_{b1}, V_{b2}) = 62.37$ kips
 Projected area of a single anchor $A_{Vco} = 4.5 \times c'_{a1}{}^2 = 2592$ in²
 Projected area of a group of anchors $A_{Vc} = 1620$ in²
 Mod factor for edge effect $\psi_{ed,V} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.792$

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Eccentricity of loading $e'_v = 0$ in
Modification factor of eccentric loading $\psi_{ec,V} = \min(1, 1 / (1 + ((2 \times e'_v) / (3 \times c'_{a1})))) = 1.000$
Modification factor for cracking $\psi_{c,V} = 1.000$
Modification factor for edge distance $\psi_{h,V} = 1.0 = 1.000$
Nominal concrete break out strength in shear $V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,V} \times \psi_{ed,V} \times \psi_{c,V} \times \psi_{h,V} \times V_b = 30.86$ kips
Concrete break out strength in shear $\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 21.60$ kips

PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

Concrete breakout strength in shear - Case 1. Half of shear resisted by front bolts (D.6.3)



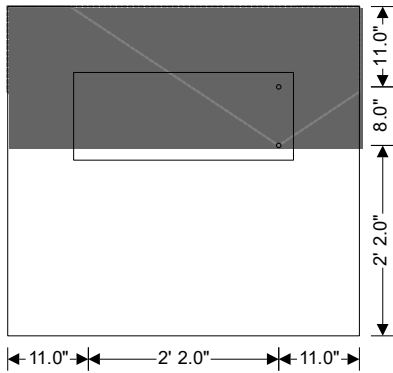
Concrete breakout - shear

Applied shear $V_{app} = V / 2 = 0.09$ kips
Edge distance x for shear near corner $c_{a1} = 11$ in
Edge distance y for shear near corner $c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{boltly} - 1) / 2) \times S_{boltly}) = 11$ in
Load bearing length of anchor $l_e = \min(h_{ef}, 8 \times d_a) = 4$ in
Basic concrete breakout strength $V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c_{a1})^{1.5} = 19.35$ kips
 $V_{b2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c_{a1})^{1.5} = 23.22$ kips
Basic concrete breakout strength $V_b = \text{Min}(V_{b1}, V_{b2}) = 19.35$ kips
Projected area of a single anchor $A_{Vco} = 4.5 \times c_{a1}^2 = 544.5$ in²
Projected area of a group of anchors $A_{Vc} = 585.7$ in²
Mod factor for edge effect $\psi_{ed,V} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c_{a1}) = 0.900$
Eccentricity of loading $e'_v = 0$ in
Modification factor of eccentric loading $\psi_{ec,V} = \min(1, 1 / (1 + ((2 \times e'_v) / (3 \times c_{a1})))) = 1.000$
Modification factor for cracking $\psi_{c,V} = 1.000$
Modification factor for edge distance $\psi_{h,V} = 1.0 = 1.000$
Nominal concrete break out strength in shear $V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,V} \times \psi_{ed,V} \times \psi_{c,V} \times \psi_{h,V} \times V_b = 18.74$ kips
Concrete break out strength in shear $\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 13.12$ kips

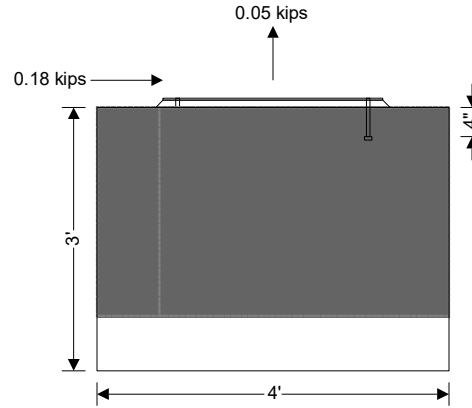
PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

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Concrete breakout strength in shear parallel to edge - Case 2. All shear resisted by rear bolts (parallel to edge - Case 2. All shear resisted by rear bolts)



Plan on foundation



Section A-A

Concrete breakout - side shear

Applied shear

$$V_{app} = V = 0.18 \text{ kips}$$

Edge distance x for shear near corner

$$c_{a1,p} = 19 \text{ in}$$

Edge distance y for shear near corner

$$c_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{boltx} - 1)/2) \times s_{boltx}) = 11 \text{ in}$$

Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 4 \text{ in}$$

Basic concrete breakout strength

$$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{(d_a) \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c_{a1,p})^{1.5}} = 43.94 \text{ kips}$$

$$V_{b,p2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c_{a1,p})^{1.5} = 52.71 \text{ kips}$$

$$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 43.94 \text{ kips}$$

Basic concrete breakout strength

$$A_{Vco,p} = 4.5 \times c_{a1,p}^2 = 1624.5 \text{ in}^2$$

Projected area of a single anchor

$$A_{Vc,p} = 1368 \text{ in}^2$$

Projected area of a group of anchors

$$\psi_{ed,V,p} = 1.000$$

Mod factor for edge effect

$$e'_{V,p} = 0 \text{ in}$$

Eccentricity of loading

$$\psi_{ec,V,p} = \min(1, 1 / (1 + ((2 \times e'_{V,p}) / (3 \times c_{a1,p})))) = 1.000$$

Modification factor of eccentric loading

$$\psi_{c,V} = 1.000$$

Modification factor for cracking

$$\psi_{h,V,p} = 1.0 = 1.000$$

Modification factor for edge distance

Nominal concrete break out strength in shear

$$V_{cbg,p} = 2 \times A_{Vc,p} / A_{Vco,p} \times \psi_{ec,V,p} \times \psi_{ed,V,p} \times \psi_{c,V} \times \psi_{h,V,p} \times V_{b,p} = 74.00 \text{ kips}$$

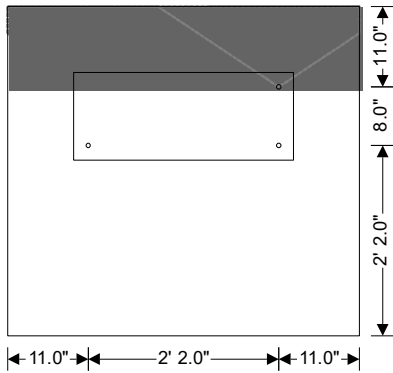
Concrete break out strength in shear

$$\phi V_{cbg,p} = \phi_{v,c} \times V_{cbg,p} = 51.80 \text{ kips}$$

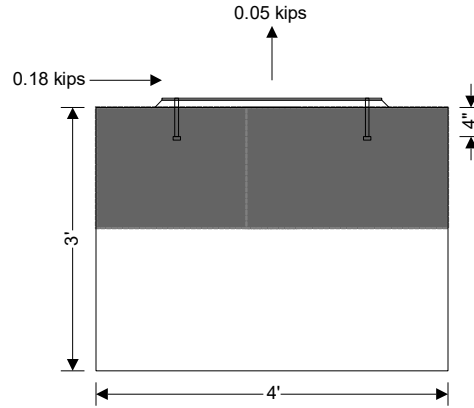
PASS - Shear breakout strength parallel to edge exceeds shear in bolts

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Concrete breakout strength in shear parallel to edge - Case 3. All shear resisted by front bolts (parallel to edge - Case 3. All shear resisted by front bolts)



Plan on foundation



Section A-A

Concrete breakout - side shear

Applied shear

$$V_{app} = V = 0.18 \text{ kips}$$

Edge distance x for shear near corner

$$c_{a1,p} = 11 \text{ in}$$

Edge distance y for shear near corner

$$c_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 11 \text{ in}$$

Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 4 \text{ in}$$

Basic concrete breakout strength

$$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{(d_a) \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c_{a1,p})^{1.5}} = 19.35 \text{ kips}$$

$$V_{b,p2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c_{a1,p})^{1.5} = 23.22 \text{ kips}$$

$$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 19.35 \text{ kips}$$

Basic concrete breakout strength

$$A_{Vco,p} = 4.5 \times c_{a1,p}^2 = 544.5 \text{ in}^2$$

Projected area of a single anchor

$$A_{Vc,p} = 792 \text{ in}^2$$

Projected area of a group of anchors

Mod factor for edge effect

$$\psi_{ed,V,p} = 1.000$$

Eccentricity of loading

$$e'_{V,p} = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,V,p} = \min(1, 1 / (1 + ((2 \times e'_{V,p}) / (3 \times c_{a1,p})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,V} = 1.000$$

Modification factor for edge distance

$$\psi_{h,V,p} = 1.0 = 1.000$$

Nominal concrete break out strength in shear

$$V_{cbg,p} = 2 \times A_{Vc,p} / A_{Vco,p} \times \psi_{ec,V,p} \times \psi_{ed,V,p} \times \psi_{c,V} \times \psi_{h,V,p} \times V_{b,p} = 56.30 \text{ kips}$$

Concrete break out strength in shear

$$\phi V_{cbg,p} = \phi_{v,c} \times V_{cbg,p} = 39.41 \text{ kips}$$

PASS - Shear breakout strength parallel to edge exceeds shear in bolts

Pryout strength of anchor in shear (D.6.3)

Coefficient of pryout strength

$$k_{cp} = 2.0$$

Nominal pryout strength of anchor in shear

$$V_{cp} = k_{cp} \times N_{cb} \times N_{boltV} = 54.31 \text{ kips}$$

Pryout strength of anchor in shear

$$\phi V_{cp} = \phi_{v,cb} \times V_{cp} = 38.01 \text{ kips}$$

PASS - Pryout strength of anchor exceeds shear in bolts

Interaction of tensile and shear forces

Critical design strength in tension

$$\phi N_n = \phi N_{sa} = 6.17 \text{ kips}$$

Critical applied tensile force

$$N_{ua} = N_{max,s} = 0.02 \text{ kips}$$

$$N_{ua} / \phi N_n = 0.004$$

Critical design strength in shear

$$\phi V_n = \phi V_{sa} = 5.14 \text{ kips}$$

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Critical applied shear force

$$V_{ua} = \text{abs}(V) = \mathbf{0.18 \text{ kips}}$$

$$V_{ua} / \phi V_n = \mathbf{0.034}$$

Full strength in both shear and tension are permitted

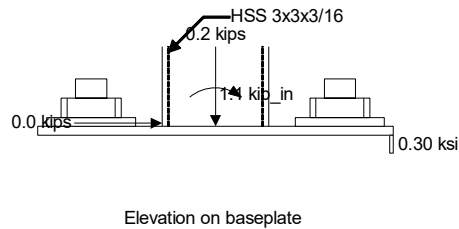
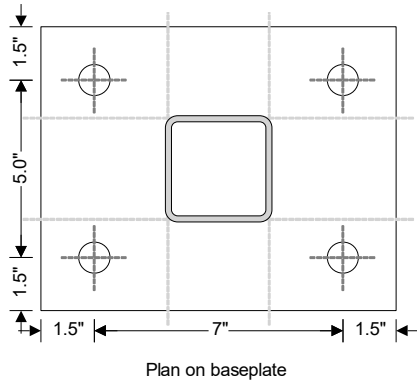
PASS - Applied tension and shear are less than tension and shear capacities

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COLUMN BASE PLATE DESIGN

In accordance with AISC Steel Design Guide 1 and AISC 360-10

Tedds calculation version 2.1.02



Bolt diameter - 0.9"
Bolt embedment - 6.0"
Flange/base weld - 0.2"
Web/base weld - 0.2"

Design forces and moments

Axial force $P_u = 0.2$ kips (Compression)
Bending moment $M_u = 1.1$ kip_in
Shear force $F_v = 0.0$ kips
Eccentricity $e = \text{ABS}(M_u / P_u) = 4.952$ in
Anchor bolt to center of plate $f = N/2 - e_1 = 3.500$ in

Column details

Column section HSS 3x3x3/16
Depth $d = 3.000$ in
Breadth $b_f = 3.000$ in
Thickness $t = 0.174$ in

Baseplate details

Depth $N = 10.000$ in
Breadth $B = 8.000$ in
Thickness $t_p = 0.250$ in
Design strength $F_y = 36.0$ ksi

Foundation geometry

Member thickness $h_a = 9.500$ in
Dist center of baseplate to left edge foundation $x_{ce1} = 17.000$ in
Dist center of baseplate to right edge foundation $x_{ce2} = 17.000$ in
Dist center of baseplate to bot edge foundation $y_{ce1} = 6.000$ in
Dist center of baseplate to top edge foundation $y_{ce2} = 16.000$ in

Holding down bolt and anchor plate details

Total number of bolts $N_{\text{bolt}} = 4$
Bolt diameter $d_o = 0.875$ in
Bolt spacing $s_{\text{bolt}} = 5.000$ in
Edge distance $e_1 = 1.500$ in
Minimum tensile strength, base plate $F_y = 36$ ksi
Minimum tensile strength, column $F_{y\text{Col}} = 50$ ksi

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Compressive strength of concrete

$$f_c = 5 \text{ ksi}$$

Strength reduction factors

Compression

$$\phi_c = 0.65$$

Flexure

$$\phi_b = 0.90$$

Weld shear

$$\phi_v = 0.75$$

Plate cantilever dimensions

Area of base plate

$$A_1 = B \times N = 80.000 \text{ in}^2$$

Maximum area of supporting surface

$$A_2 = (N + 2 \times l_{\min}) \times (B + 2 \times l_{\min}) = 168.000 \text{ in}^2$$

Nominal strength of concrete under base plate

$$P_p = 0.85 \times f_c \times A_1 \times \min(\sqrt{A_2 / A_1}, 2) = 492.7 \text{ kips}$$

Bending line cantilever distance m

$$m = (N - 0.95 \times d) / 2 = 3.575 \text{ in}$$

Bending line cantilever distance n

$$n = (B - 0.95 \times b_f) / 2 = 2.575 \text{ in}$$

Maximum bending line cantilever

$$l = \max(m, n) = 3.575 \text{ in}$$

Check eccentricity

Maximum bearing stress

$$f_{p,\max} = 0.85 \times f_c \times \phi_c \times \min(\sqrt{A_2 / A_1}, 2) = 4 \text{ ksi}$$

Maximum bearing pressure

$$q_{\max} = f_{p,\max} \times B = 32.03 \text{ kips/in}$$

Critical eccentricity

$$e_{\text{crit}} = N / 2 - P_u / (2 \times q_{\max}) = 4.996 \text{ in}$$

e ≤ e_{crit} so loads can be resisted by bearing alone. Therefore consider as a small moment

Bearing length

$$Y = N - 2 \times e = 0.096 \text{ in}$$

Bearing pressure

$$q = P_u / Y = 2.4 \text{ kips/in}$$

PASS - Maximum allowable bearing stress exceeds actual

Base plate yielding limit at bearing interface

Required plate thickness

$$t_{p,\text{req}} = \sqrt{((4 \times f_p \times Y \times (l - Y/2)) / (\phi_b \times F_y))} = 0.112 \text{ in}$$

PASS - Thickness of plate exceeds required thickness

Flange weld

Flange weld leg length

$$t_{wf} = 0.1875 \text{ in}$$

Tension capacity of flange

$$P_{tf} = b_f \times t \times F_{y\text{Col}} = 26.1 \text{ kips}$$

Force in tension flange

$$F_{tf} = M_u / (d - t) - P_u \times (b_f \times t) / A_{\text{col}} = 0.3 \text{ kips}$$

Critical force in flange

$$F_f = \min(P_{tf}, \max(F_{tf}, 0 \text{ kips})) = 0.3 \text{ kips}$$

Flange weld force per in

$$R_{wf} = F_f / b_f = 0.1 \text{ kips/in}$$

Electrode classification number

$$F_{EXX} = 70.0 \text{ ksi}$$

Design weld stress

$$\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(90\text{deg}))^{1.5}) = 47.250 \text{ ksi}$$

Design strength of weld per in

$$\phi R_{nf} = \phi F_{nw} \times t_{wf} / \sqrt{2} = 6.3 \text{ kips/in}$$

PASS - Available strength of flange weld exceeds force in flange weld

Shear weld

Shear web weld leg length

$$t_{ww} = 0.1875 \text{ in}$$

Shear web weld force per in

$$R_{wf} = F_v / (2 \times (d - 2 \times t)) = 0.005 \text{ kips/in}$$

Electrode classification number

$$F_{EXX} = 70.0 \text{ ksi}$$

Design weld stress

$$\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(0\text{deg}))^{1.5}) = 31.500 \text{ ksi}$$

Design strength of weld per in

$$\phi R_{nl} = \phi F_{nw} \times t_{ww} / \sqrt{2} = 4.2 \text{ kips/in}$$

PASS - Available strength of shear weld exceeds force in shear weld

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ANCHOR BOLT DESIGN

In accordance with ACI318-11

Tedds calculation version 2.1.02

Anchor bolt geometry

Type of anchor bolt	Cast-in headed end bolt anchor
Diameter of anchor bolt	$d_a = 0.875$ in
Number of bolts in x direction	$N_{boltx} = 2$
Number of bolts in y direction	$N_{bolty} = 2$
Total number of bolts	$n_{total} = (N_{boltx} \times 2) + (N_{bolty} - 2) \times 2 = 4$
Total number of bolts in tension	$n_{tens} = N_{boltN} = 0$
Spacing of bolts in x direction	$S_{boltx} = 7$ in
Spacing of bolts in y direction	$S_{bolty} = 5$ in
Number of threads per inch	$n_t = 9$
Effective cross-sectional area of anchor	$A_{se} = \pi / 4 \times (d_a - 0.9743 \text{ in} / n_t)^2 = 0.462$ in ²
Embedded depth of each anchor bolt	$h_{ef} = 6$ in

Material details

Minimum yield strength of steel	$f_{ya} = 36$ ksi
Nominal tensile strength of steel	$f_{uta} = 58$ ksi
Compressive strength of concrete	$f'_c = 5$ ksi
Concrete modification factor	$\lambda = 1.00$
Modification factor for cast-in anchor concrete failure	$\lambda_a = 1.0 \times \lambda = 1.00$

Strength reduction factors

Tension of steel element	$\phi_{t,s} = 0.75$
Shear of steel element	$\phi_{v,s} = 0.65$
Concrete tension	$\phi_{t,c} = 0.65$
Concrete shear	$\phi_{v,c} = 0.70$
Concrete tension for pullout	$\phi_{t,cB} = 0.70$
Concrete shear for prout	$\phi_{v,cB} = 0.70$
Shear force applied to bolt group	$V = 0.03$ kips

Steel strength of anchor in shear (D.6.1)

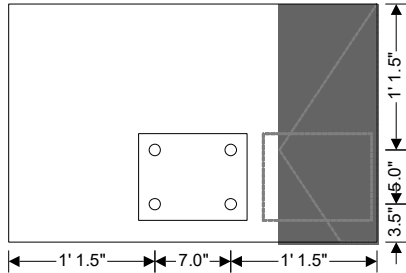
Built-up grout pads are used so nominal strength will be multiplied by 0.8 (D.6.1.3)

Effective number of anchors in shear	$N_{boltV} = 2$
Nom strength of anchor in shear	$V_{sa} = 0.8 \times N_{boltV} \times 0.6 \times A_{se} \times f_{uta} = 25.71$ kips
Steel strength of anchor in shear	$\phi V_{sa} = \phi_{v,s} \times V_{sa} = 16.71$ kips

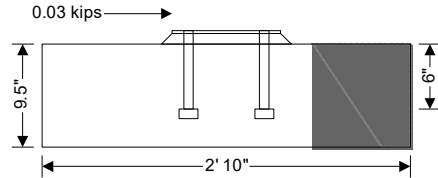
PASS - Steel strength of anchor exceeds shear in bolts

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Concrete breakout strength in shear perpendicular to edge - Case 2. All shear resisted by rear bolts (D.6.3)



Plan on foundation



Section A-A

Concrete breakout - shear

The anchors are influenced by three or more edges where any edge distance is less than $1.5c_{a1}$ so value of c_{a1} is limited to c'_{a1} (D.6.2.4).

Bolt offset for limiting shear $x_{V,r} = 11.50$ in

Limiting edge distance $c'_{a1} = 9$ in

Applied shear $V_{app} = V = 0.03$ kips

Edge distance x for shear near corner $c_{a1} = 20.5$ in

Edge distance y for shear near corner $c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 3.5$ in

Load bearing length of anchor $l_e = \min(h_{ef}, 8 \times d_a) = 6$ in

Basic concrete breakout strength $V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times (c'_{a1})^{1.5} = 18.37$ kips

$$x_{V,r} = 11.50 \text{ in}$$

$$c'_{a1} = 9 \text{ in}$$

$$V_{app} = V = 0.03 \text{ kips}$$

$$c_{a1} = 20.5 \text{ in}$$

$$c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 3.5 \text{ in}$$

$$l_e = \min(h_{ef}, 8 \times d_a) = 6 \text{ in}$$

$$V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times (c'_{a1})^{1.5} = 18.37 \text{ kips}$$

$$V_{b2} = 9 \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi} \times 1 \text{ in}} \times (c'_{a1})^{1.5} = 17.18 \text{ kips}$$

$$V_b = \text{Min}(V_{b1}, V_{b2}) = 17.18 \text{ kips}$$

$$A_{Vco} = 4.5 \times c'_{a1}{}^2 = 364.5 \text{ in}^2$$

$$A_{Vc} = 209 \text{ in}^2$$

$$\psi_{ed,v} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.778$$

$$e'_{v} = 0 \text{ in}$$

$$\psi_{ec,v} = \min(1, 1 / (1 + ((2 \times e'_{v}) / (3 \times c'_{a1})))) = 1.000$$

$$\psi_{c,v} = 1.000$$

$$\psi_{h,v} = \max(\sqrt{(1.5 \times c'_{a1} / h_a)}, 1) = 1.192$$

$$V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,v} \times \psi_{ed,v} \times \psi_{c,v} \times \psi_{h,v} \times V_b = 9.13 \text{ kips}$$

$$\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 6.39 \text{ kips}$$

Basic concrete breakout strength $V_b = \text{Min}(V_{b1}, V_{b2}) = 17.18$ kips

Projected area of a single anchor $A_{Vco} = 4.5 \times c'_{a1}{}^2 = 364.5$ in²

Projected area of a group of anchors $A_{Vc} = 209$ in²

Mod factor for edge effect $\psi_{ed,v} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.778$

Eccentricity of loading $e'_{v} = 0$ in

Modification factor of eccentric loading $\psi_{ec,v} = \min(1, 1 / (1 + ((2 \times e'_{v}) / (3 \times c'_{a1})))) = 1.000$

Modification factor for cracking $\psi_{c,v} = 1.000$

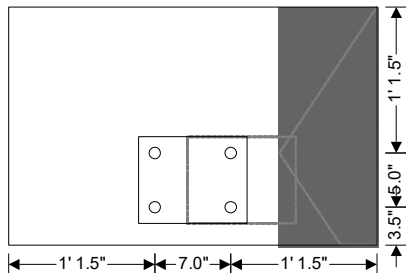
Modification factor for edge distance $\psi_{h,v} = \max(\sqrt{(1.5 \times c'_{a1} / h_a)}, 1) = 1.192$

Nominal concrete break out strength in shear $V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,v} \times \psi_{ed,v} \times \psi_{c,v} \times \psi_{h,v} \times V_b = 9.13$ kips

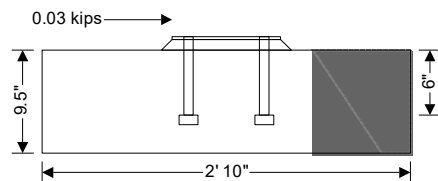
Concrete break out strength in shear $\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 6.39$ kips

PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

Concrete breakout strength in shear perpendicular to edge - Case 3. All shear resisted by front bolts (D.6.3)



Plan on foundation



Section A-A

Concrete breakout - shear

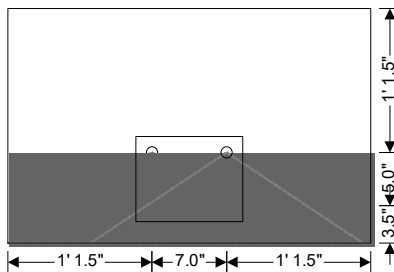
Kimely-Horn	Project THEA Lighting Project				Job Ref.	
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The anchors are influenced by three or more edges where any edge distance is less than $1.5c_{a1}$ so value of c_{a1} is limited to c'_{a1} (D.6.2.4).

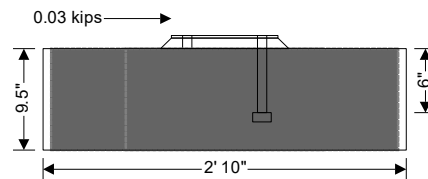
Bolt offset for limiting shear	$x_{V,f} = 4.50$ in
Limiting edge distance	$c'_{a1} = 9$ in
Applied shear	$V_{app} = V = 0.03$ kips
Edge distance x for shear near corner	$c_{a1} = 13.5$ in
Edge distance y for shear near corner	$c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 3.5$ in
Load bearing length of anchor	$l_e = \min(h_{ef}, 8 \times d_a) = 6$ in
Basic concrete breakout strength	$V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1\text{psi}} \times (c'_{a1})^{1.5} = 18.37$ kips
	$V_{b2} = 9 \times \lambda_a \times \sqrt{f'_c \times 1\text{psi} \times 1\text{in}} \times (c'_{a1})^{1.5} = 17.18$ kips
Basic concrete breakout strength	$V_b = \text{Min}(V_{b1}, V_{b2}) = 17.18$ kips
Projected area of a single anchor	$A_{Vco} = 4.5 \times c'_{a1}{}^2 = 364.5$ in ²
Projected area of a group of anchors	$A_{Vc} = 209$ in ²
Mod factor for edge effect	$\psi_{ed,V} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.778$
Eccentricity of loading	$e'_v = 0$ in
Modification factor of eccentric loading	$\psi_{ec,V} = \min(1, 1 / (1 + ((2 \times e'_v) / (3 \times c'_{a1})))) = 1.000$
Modification factor for cracking	$\psi_{c,V} = 1.000$
Modification factor for edge distance	$\psi_{h,V} = \max(\sqrt{(1.5 \times c'_{a1} / h_a)}, 1) = 1.192$
Nominal concrete break out strength in shear	$V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,V} \times \psi_{ed,V} \times \psi_{c,V} \times \psi_{h,V} \times V_b = 9.13$ kips
Concrete break out strength in shear	$\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 6.39$ kips

PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

Concrete breakout strength in shear parallel to edge - Case 2. All shear resisted by rear bolts (parallel to edge - Case 2. All shear resisted by rear bolts)



Plan on foundation



Section A-A

Concrete breakout - side shear

Applied shear	$V_{app} = V = 0.03$ kips
Edge distance x for shear near corner	$c_{a1,p} = 8.5$ in
Edge distance y for shear near corner	$c_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 13.5$ in
Load bearing length of anchor	$l_e = \min(h_{ef}, 8 \times d_a) = 6$ in
Basic concrete breakout strength	$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1\text{psi}} \times (c_{a1,p})^{1.5} = 16.86$ kips
	$V_{b,p2} = 9 \times \lambda_a \times \sqrt{f'_c \times 1\text{psi} \times 1\text{in}} \times (c_{a1,p})^{1.5} = 15.77$ kips
Basic concrete breakout strength	$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 15.77$ kips
Projected area of a single anchor	$A_{Vco,p} = 4.5 \times c_{a1,p}{}^2 = 325.1$ in ²
Projected area of a group of anchors	$A_{Vc,p} = 308.8$ in ²
Mod factor for edge effect	$\psi_{ed,V,p} = 1.000$

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Eccentricity of loading

$$e'_{v,p} = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,v,p} = \min(1, 1 / (1 + ((2 \times e'_{v,p}) / (3 \times C_{a1,p})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,v} = 1.000$$

Modification factor for edge distance

$$\psi_{h,v,p} = \max(\sqrt{(1.5 \times C_{a1,p} / h_a)}, 1) = 1.158$$

Nominal concrete break out strength in shear

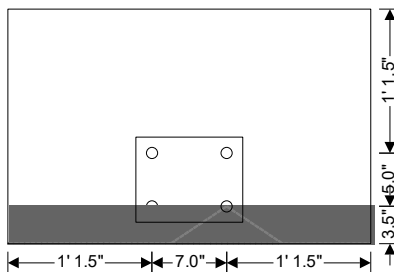
$$V_{cbg,p} = 2 \times A_{Vc,p} / A_{Vco,p} \times \psi_{ec,v,p} \times \psi_{ed,v,p} \times \psi_{c,v} \times \psi_{h,v,p} \times V_{b,p} = 34.70 \text{ kips}$$

Concrete break out strength in shear

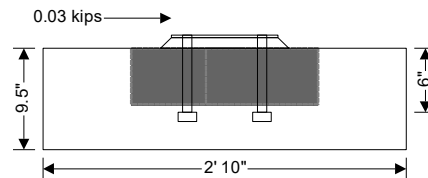
$$\phi V_{cbg,p} = \phi_{v,c} \times V_{cbg,p} = 24.29 \text{ kips}$$

PASS - Shear breakout strength parallel to edge exceeds shear in bolts

Concrete breakout strength in shear parallel to edge - Case 1. Half of shear resisted by front bolts (parallel to edge - Case 1. Half of shear resisted by front bolts)



Plan on foundation



Section A-A

Concrete breakout - side shear

Applied shear

$$V_{app} = V / 2 = 0.01 \text{ kips}$$

Edge distance x for shear near corner

$$C_{a1,p} = 3.5 \text{ in}$$

Edge distance y for shear near corner

$$C_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{boltx} - 1)/2) \times S_{boltx}) = 13.5 \text{ in}$$

Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 6 \text{ in}$$

Basic concrete breakout strength

$$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times (C_{a1,p})^{1.5} = 4.46 \text{ kips}$$

$$V_{b,p2} = 9 \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi} \times 1 \text{ in}} \times (C_{a1,p})^{1.5} = 4.17 \text{ kips}$$

$$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 4.17 \text{ kips}$$

Basic concrete breakout strength

Projected area of a single anchor

$$A_{Vco,p} = 4.5 \times C_{a1,p}^2 = 55.1 \text{ in}^2$$

Projected area of a group of anchors

$$A_{Vc,p} = 91.9 \text{ in}^2$$

Mod factor for edge effect

$$\psi_{ed,v,p} = 1.000$$

Eccentricity of loading

$$e'_{v,p} = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,v,p} = \min(1, 1 / (1 + ((2 \times e'_{v,p}) / (3 \times C_{a1,p})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,v} = 1.000$$

Modification factor for edge distance

$$\psi_{h,v,p} = 1.0 = 1.000$$

Nominal concrete break out strength in shear

$$V_{cbg,p} = 2 \times A_{Vc,p} / A_{Vco,p} \times \psi_{ec,v,p} \times \psi_{ed,v,p} \times \psi_{c,v} \times \psi_{h,v,p} \times V_{b,p} = 13.89 \text{ kips}$$

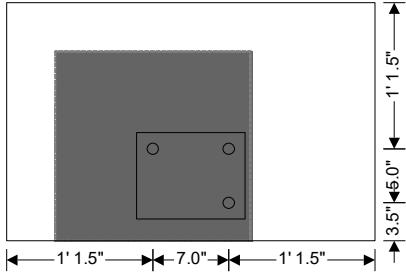
Concrete break out strength in shear

$$\phi V_{cbg,p} = \phi_{v,c} \times V_{cbg,p} = 9.72 \text{ kips}$$

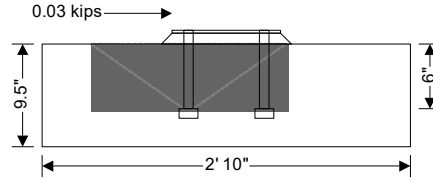
PASS - Shear breakout strength parallel to edge exceeds shear in bolts

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Pryout strength of anchor in shear (D.6.3)



Plan on foundation



Section A-A

Concrete breakout - tension

- Coeff for basic breakout strength in tension
- Breakout strength for single anchor in tension
- Projected area for groups of anchors
- Projected area of a single anchor
- Min dist center of anchor to edge of concrete
- Mod factor for groups loaded eccentrically
- Modification factor for edge effects
- Modification factor for no cracking at service loads
- Modification factor for cracked concrete
- Nominal concrete breakout strength
- Concrete breakout strength
- Coefficient of pryout strength
- Nominal pryout strength of anchor in shear
- Pryout strength of anchor in shear

$k_c = 24$
 $N_b = k_c \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times h_{ef}^{1.5} \times 1 \text{ in}^{0.5} = 24.94 \text{ kips}$
 $A_{Nc} = 315 \text{ in}^2$
 $A_{Nco} = 9 \times h_{ef}^2 = 324 \text{ in}^2$
 $c_{a,min} = 3.5 \text{ in}$
 $\psi_{ec,N} = \min(1 / (1 + ((2 \times e'_N) / (3 \times h_{ef}))), 1) = 1.000$
 $\psi_{ed,N} = 0.7 + 0.3 \times (c_{a,min} / (1.5 \times h_{ef})) = 0.817$
 $\psi_{c,N} = 1.000$
 $\psi_{cp,N} = 1.000$
 $N_{cbg} = A_{Nc} / A_{Nco} \times \psi_{ed,N} \times \psi_{c,N} \times \psi_{cp,N} \times N_b = 19.80 \text{ kips}$
 $\phi N_{cbg} = \phi_{t,c} \times N_{cbg} = 12.87 \text{ kips}$
 $k_{cp} = 2.0$
 $V_{cpg} = k_{cp} \times N_{cbg} = 39.61 \text{ kips}$
 $\phi V_{cpg} = \phi_{v,cB} \times V_{cpg} = 27.72 \text{ kips}$

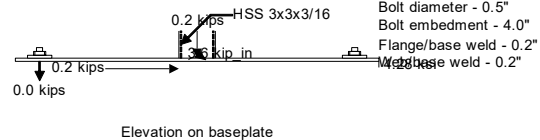
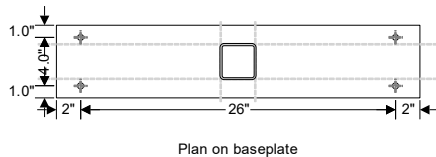
PASS - Pryout strength of anchor exceeds shear in bolts

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COLUMN BASE PLATE DESIGN

In accordance with AISC Steel Design Guide 1 and AISC 360-10

Tedds calculation version 2.1.02



Design forces and moments

Axial force	$P_u = 0.2$ kips (Compression)
Bending moment	$M_u = 3.6$ kip_in
Shear force	$F_v = 0.2$ kips
Eccentricity	$e = ABS(M_u / P_u) = 23.571$ in
Anchor bolt to center of plate	$f = N/2 - e_1 = 13.000$ in

Column details

Column section	HSS 3x3x3/16
Depth	$d = 3.000$ in
Breadth	$b_f = 3.000$ in
Thickness	$t = 0.174$ in

Baseplate details

Depth	$N = 30.000$ in
Breadth	$B = 6.000$ in
Thickness	$t_p = 0.250$ in
Design strength	$F_y = 36.0$ ksi

Foundation geometry

Member thickness	$h_a = 10.000$ in
Dist center of baseplate to left edge foundation	$x_{ce1} = 24.000$ in
Dist center of baseplate to right edge foundation	$x_{ce2} = 24.000$ in
Dist center of baseplate to bot edge foundation	$y_{ce1} = 6.000$ in
Dist center of baseplate to top edge foundation	$y_{ce2} = 7.000$ in

Holding down bolt and anchor plate details

Total number of bolts	$N_{bolt} = 4$
Bolt diameter	$d_o = 0.500$ in
Bolt spacing	$s_{bolt} = 4.000$ in
Edge distance	$e_1 = 2.000$ in
Minimum tensile strength, base plate	$F_y = 36$ ksi
Minimum tensile strength, column	$F_{yCol} = 50$ ksi
Compressive strength of concrete	$f'_c = 5$ ksi

Strength reduction factors

Compression	$\phi_c = 0.65$
Flexure	$\phi_b = 0.90$
Weld shear	$\phi_v = 0.75$

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Plate cantilever dimensions

Area of base plate	$A_1 = B \times N = 180.000 \text{ in}^2$
Maximum area of supporting surface	$A_2 = (N + 2 \times l_{\min}) \times (B + 2 \times l_{\min}) = 432.000 \text{ in}^2$
Nominal strength of concrete under base plate	$P_p = 0.85 \times f'_c \times A_1 \times \min(\sqrt{A_2 / A_1}, 2) = 1185.1 \text{ kips}$
Bending line cantilever distance m	$m = (N - 0.95 \times d) / 2 = 13.575 \text{ in}$
Bending line cantilever distance n	$n = (B - 0.95 \times b_f) / 2 = 1.575 \text{ in}$
Maximum bending line cantilever	$l = \max(m, n) = 13.575 \text{ in}$

Check eccentricity

Maximum bearing stress	$f_{p,\max} = 0.85 \times f'_c \times \phi_c \times \min(\sqrt{A_2 / A_1}, 2) = 4.28 \text{ ksi}$
Maximum bearing pressure	$q_{\max} = f_{p,\max} \times B = 25.68 \text{ kips/in}$
Critical eccentricity	$e_{\text{crit}} = N / 2 - P_u / (2 \times q_{\max}) = 14.997 \text{ in}$

$e > e_{\text{crit}}$ so loads cannot be resisted by bearing alone. Therefore consider as a large moment

Plate dimensions adequate as $(f + N/2)^2 \geq (2 \times P_u \times (e + f)) / q_{\max}$ and a real solution for bearing length exists

Bearing length - quadratic solution 1	$Y_1 = (f + N/2) + \sqrt{((f + N/2)^2 - (2 \times P_u \times (e + f)) / q_{\max})} = 55.992 \text{ in}$
Bearing length - quadratic solution 2	$Y_2 = (f + N/2) - \sqrt{((f + N/2)^2 - (2 \times P_u \times (e + f)) / q_{\max})} = 0.008 \text{ in}$
Bearing length	$Y = \min(Y_1, Y_2) = 0.008 \text{ in}$
Tension force in bolts	$T_u = q_{\max} \times Y - P_u = 0.0 \text{ kips}$
Max tension in single bolt	$T_{\text{rod}} = T_u / (N_{\text{bolt}} / 2) = 0.0 \text{ kips}$

Base plate yielding limit at bearing interface

Required plate thickness	$t_{p,\text{req}} = \sqrt{((4 \times f_{p,\max} \times Y \times (l - Y/2)) / (\phi_b \times F_y))} = 0.237 \text{ in}$
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PASS - Thickness of plate exceeds required thickness

Base plate yielding limit at tension interface

Distance from bolt CL to plate bending lines	$x = \text{abs}(m - e_1) = 11.575 \text{ in}$
Plate thickness required	$t_{p,\text{req}} = 2.11 \times \sqrt{((T_u \times x) / (B \times F_y))} = 0.106 \text{ in}$

PASS - Thickness of plate exceeds required thickness

Combined tension and bending in anchor bolts

Gross cross sectional area of anchor	$A_{\text{bolt}} = \pi \times d_a^2 / 4 = 0.196 \text{ in}^2$
Thickness of washer	$t_{\text{wash}} = 0.250 \text{ in}$
Shear stress in anchor	$f_v = F_v / (N_{\text{boltV}} \times A_{\text{bolt}}) = 0.45 \text{ ksi}$
Lever arm	$z = t_p + t_{\text{wash}} / 2 = 0.375 \text{ in}$
Bending in anchor	$M_l = F_v \times z / N_{\text{boltV}} = 0.00 \text{ kips_ft}$
Plastic modulus of anchor	$Z_{\text{bolt}} = d_a^3 / 6 = 0.021 \text{ in}^3$
Stress in anchor due to bending	$f_{\text{tb}} = M_l / Z_{\text{bolt}} = 1.6 \text{ ksi}$
Axial stress in anchor	$f_{\text{ta}} = T_{\text{rod}} / A_{\text{bolt}} = 0.1 \text{ ksi}$
Tensile stress in anchor	$f_t = f_{\text{tb}} + f_{\text{ta}} = 1.7 \text{ ksi}$
Nominal tensile stress of anchor (Table J3.2)	$F_{\text{nt}} = 0.75 \times f_{\text{uta}} = 43.5 \text{ ksi}$
Nominal shear stress of anchor (Table J3.2)	$F_{\text{nv}} = 0.45 \times f_{\text{uta}} = 26.1 \text{ ksi}$
Tensile stress of anchor	$\phi F_{\text{nt}} = \phi \times F_{\text{nt}} = 32.6 \text{ ksi}$
Modified tensile stress (Eqn J3-3a)	$\phi F'_{\text{nt}} = \min(\phi \times (1.3 \times F_{\text{nt}} - (F_{\text{nt}} / (\phi \times F_{\text{nv}})) \times f_v), \phi F_{\text{nt}}) = 32.6 \text{ ksi}$

PASS - Combined shear and bending resistance of rods exceed tensile stress in rods

Tension weld

Tension flange weld leg length	$t_{\text{wf}} = 0.1875 \text{ in}$
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Effective flange weld width $l_{T_{weld,eff}} = l_{T_{weld,eff_ud}} = 2$ in
Tensile load per inch $R_{wf} = T_{rod} / l_{T_{weld,eff}} = 0.0$ kips/in
Electrode classification number $F_{EXX} = 70.0$ ksi
Design weld stress $\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(90deg))^{1.5}) = 47.250$ ksi
Design strength of weld per in $\phi R_{nf} = \phi F_{nw} \times t_{wf} / \sqrt{(2)} = 6.3$ kips/in
PASS - Available strength of weld exceeds force in tension weld

Local stress on flange $f_{T,local} = (T_{rod}) / (l_{T_{weld,eff}} \times t_f) = 0.068$ ksi
Column flange allowable stress $F_{yCol} / 1.67 = 29.940$ ksi
PASS - Local column capacity exceeds local column stress

Shear weld

Shear web weld leg length $t_{ww} = 0.1875$ in
Shear web weld force per in $R_{wl} = F_v / (2 \times (d - 2 \times t)) = 0.033$ kips/in
Electrode classification number $F_{EXX} = 70.0$ ksi
Design weld stress $\phi F_{nw} = \phi_v \times 0.60 \times F_{EXX} \times (1.0 + 0.5 \times (\sin(0deg))^{1.5}) = 31.500$ ksi
Design strength of weld per in $\phi R_{nl} = \phi F_{nw} \times t_{ww} / \sqrt{(2)} = 4.2$ kips/in
PASS - Available strength of shear weld exceeds force in shear weld

ANCHOR BOLT DESIGN

In accordance with ACI318-11

Tedds calculation version 2.1.02

Anchor bolt geometry

Type of anchor bolt Cast-in headed end bolt anchor
Diameter of anchor bolt $d_a = 0.5$ in
Number of bolts in x direction $N_{boltx} = 2$
Number of bolts in y direction $N_{bolty} = 2$
Total number of bolts $n_{total} = (N_{boltx} \times 2) + (N_{bolty} - 2) \times 2 = 4$
Total number of bolts in tension $n_{tens} = (N_{boltN} \times 2) + (N_{bolty} - 2) = 2$
Spacing of bolts in x direction $S_{boltx} = 26$ in
Spacing of bolts in y direction $S_{bolty} = 4$ in
Number of threads per inch $n_t = 13$
Effective cross-sectional area of anchor $A_{se} = \pi / 4 \times (d_a - 0.9743 \text{ in} / n_t)^2 = 0.142$ in²
Embedded depth of each anchor bolt $h_{ef} = 4$ in

Material details

Minimum yield strength of steel $f_{ya} = 36$ ksi
Nominal tensile strength of steel $f_{uta} = 58$ ksi
Compressive strength of concrete $f'_c = 5$ ksi
Concrete modification factor $\lambda = 1.00$
Modification factor for cast-in anchor concrete failure $\lambda_a = 1.0 \times \lambda = 1.00$

Strength reduction factors

Tension of steel element $\phi_{t,s} = 0.75$
Shear of steel element $\phi_{v,s} = 0.65$
Concrete tension $\phi_{t,c} = 0.65$
Concrete shear $\phi_{v,c} = 0.70$

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Concrete tension for pullout

$$\phi_{t,cB} = \mathbf{0.70}$$

Concrete shear for pryout

$$\phi_{v,cB} = \mathbf{0.70}$$

Steel strength of anchor in tension (D.5.1)

Nominal strength of anchor in tension

$$N_{sa} = A_{se} \times f_{uta} = \mathbf{8.23 \text{ kips}}$$

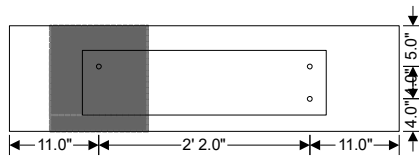
Steel strength of anchor in tension

$$\phi N_{sa} = \phi_{t,s} \times N_{sa} = \mathbf{6.17 \text{ kips}}$$

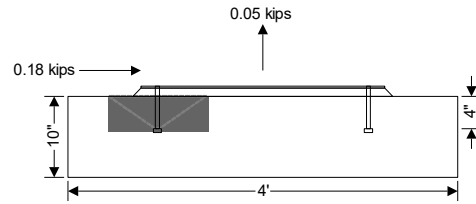
PASS - Steel strength of anchor exceeds max tension in single bolt

Check concrete breakout strength of anchor bolt in tension (D.5.2)

The spacing and embedded depth of the bolts/anchors are such that the projected area of all the anchors do not overlap. The concrete breakout strength of the anchors will therefore be based on a single anchor with the maximum axial force to a single anchor



Plan on foundation



Section A-A

Concrete breakout - tension

Single anchor

Applied axial force

$$N_s = N_{max,s} = \mathbf{0.02 \text{ kips}}$$

Eccentricity

$$e'_N = \mathbf{0 \text{ in}}$$

Coeff for basic breakout strength in tension

$$k_c = \mathbf{24}$$

Breakout strength for single anchor in tension

$$N_b = k_c \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times h_{ef}^{1.5} \times 1 \text{ in}^{0.5} = \mathbf{13.58 \text{ kips}}$$

Projected area for groups of anchors

$$A_{Nc} = \mathbf{120 \text{ in}^2}$$

Projected area of a single anchor

$$A_{Nco} = 9 \times h_{ef}^2 = \mathbf{144 \text{ in}^2}$$

Min dist center of anchor to edge of concrete

$$C_{a,min} = \mathbf{4 \text{ in}}$$

Mod factor for groups loaded eccentrically

$$\psi_{ec,N} = \min(1 / (1 + ((2 \times e'_N) / (3 \times h_{ef}))), 1) = \mathbf{1.000}$$

Modification factor for edge effects

$$\psi_{ed,N} = 0.7 + 0.3 \times (C_{a,min} / (1.5 \times h_{ef})) = \mathbf{0.900}$$

Modification factor for no cracking at service loads

$$\psi_{c,N} = \mathbf{1.000}$$

Modification factor for cracked concrete

$$\psi_{cp,N} = \mathbf{1.000}$$

Nominal concrete breakout strength

$$N_{cb} = A_{Nc} / A_{Nco} \times \psi_{ed,N} \times \psi_{c,N} \times \psi_{cp,N} \times N_b = \mathbf{10.18 \text{ kips}}$$

Concrete breakout strength

$$\phi N_{cb} = \phi_{t,c} \times N_{cb} = \mathbf{6.62 \text{ kips}}$$

PASS - Breakout strength exceeds tension in bolts

Pullout strength (D.5.3)

Net bearing area of the head of anchor

$$A_{brg} = \mathbf{1 \text{ in}^2}$$

Mod factor for no cracking at service loads

$$\psi_{c,P} = \mathbf{1.000}$$

Pullout strength for single anchor

$$N_p = 8 \times A_{brg} \times f'_c = \mathbf{40.00 \text{ kips}}$$

Nominal pullout strength of single anchor

$$N_{pn} = \psi_{c,P} \times N_p = \mathbf{40.00 \text{ kips}}$$

Pullout strength of single anchor

$$\phi N_{pn} = \phi_{t,cB} \times N_{pn} = \mathbf{28.00 \text{ kips}}$$

PASS - Pullout strength of single anchor exceeds maximum axial force in single bolt

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Side face blowout strength (D.5.4)

As $h_{ef} \leq 2.5 \times \min(c_{a1}, c_{a2})$ the edge distance is considered to be far from an edge and blowout strength need not be considered

Steel strength of anchor in shear (D.6.1)

Built-up grout pads are used so nominal strength will be multiplied by 0.8 (D.6.1.3)

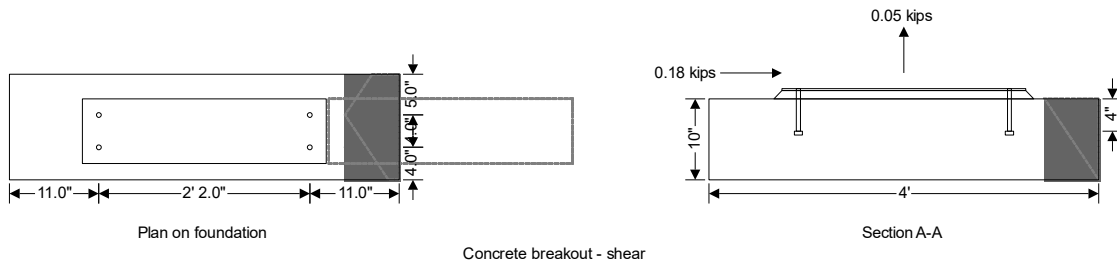
Effective number of anchors in shear $N_{boltV} = 2$

Nom strength of anchor in shear $V_{sa} = 0.8 \times N_{boltV} \times 0.6 \times A_{se} \times f_{uta} = 7.90$ kips

Steel strength of anchor in shear $\phi V_{sa} = \phi_{v,s} \times V_{sa} = 5.14$ kips

PASS - Steel strength of anchor exceeds shear in bolts

Concrete breakout strength in shear perpendicular to edge - Case 2. All shear resisted by rear bolts (D.6.3)



The anchors are influenced by three or more edges where any edge distance is less than $1.5c_{a1}$ so value of c_{a1} is limited to c'_{a1} (D.6.2.4).

Bolt offset for limiting shear $X_{V,r} = 30.33$ in

Limiting edge distance $c'_{a1} = 6.67$ in

Applied shear $V_{app} = V = 0.18$ kips

Edge distance x for shear near corner $c_{a1} = 37$ in

Edge distance y for shear near corner $c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{boltV} - 1)/2) \times S_{boltV}) = 4$ in

Load bearing length of anchor $l_e = \min(h_{ef}, 8 \times d_a) = 4$ in

Basic concrete breakout strength $V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c'_{a1})^{1.5} = 9.13$ kips

$V_{b2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c'_{a1})^{1.5} = 10.95$ kips

Basic concrete breakout strength $V_b = \text{Min}(V_{b1}, V_{b2}) = 9.13$ kips

Projected area of a single anchor $A_{Vco} = 4.5 \times c'_{a1}{}^2 = 200$ in²

Projected area of a group of anchors $A_{Vc} = 130$ in²

Mod factor for edge effect $\psi_{ed,V} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.820$

Eccentricity of loading $e'_{v} = 0$ in

Modification factor of eccentric loading $\psi_{ec,V} = \min(1, 1 / (1 + ((2 \times e'_{v}) / (3 \times c'_{a1})))) = 1.000$

Modification factor for cracking $\psi_{c,V} = 1.000$

Modification factor for edge distance $\psi_{h,V} = 1.0 = 1.000$

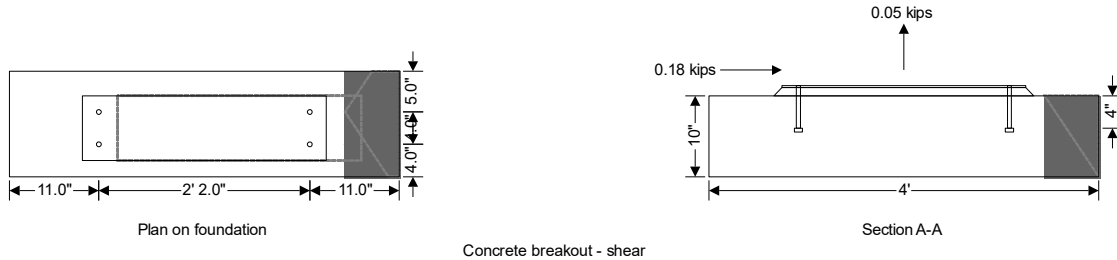
Nominal concrete break out strength in shear $V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,V} \times \psi_{ed,V} \times \psi_{c,V} \times \psi_{h,V} \times V_b = 4.87$ kips

Concrete break out strength in shear $\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 3.41$ kips

PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

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Concrete breakout strength in shear - Case 1. Half of shear resisted by front bolts (D.6.3)



The anchors are influenced by three or more edges where any edge distance is less than $1.5c_{a1}$ so value of c_{a1} is limited to c'_{a1} (D.6.2.4).

Bolt offset for limiting shear

$$x_{V,f} = 4.33 \text{ in}$$

Limiting edge distance

$$c'_{a1} = 6.67 \text{ in}$$

Applied shear

$$V_{app} = V / 2 = 0.09 \text{ kips}$$

Edge distance x for shear near corner

$$c_{a1} = 11 \text{ in}$$

Edge distance y for shear near corner

$$c_{a2} = \min(y_{ce1}, y_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 4 \text{ in}$$

Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 4 \text{ in}$$

Basic concrete breakout strength

$$V_{b1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{d_a} \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi}} \times (c'_{a1})^{1.5} = 9.13 \text{ kips}$$

$$V_{b2} = 9 \times \lambda_a \times \sqrt{f'_c \times 1 \text{ psi} \times 1 \text{ in}} \times (c'_{a1})^{1.5} = 10.95 \text{ kips}$$

Basic concrete breakout strength

$$V_b = \text{Min}(V_{b1}, V_{b2}) = 9.13 \text{ kips}$$

Projected area of a single anchor

$$A_{Vco} = 4.5 \times c'_{a1}{}^2 = 200 \text{ in}^2$$

Projected area of a group of anchors

$$A_{Vc} = 130 \text{ in}^2$$

Mod factor for edge effect

$$\psi_{ed,V} = 0.7 + 0.3 \times c_{a2} / (1.5 \times c'_{a1}) = 0.820$$

Eccentricity of loading

$$e'_V = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,V} = \min(1, 1 / (1 + ((2 \times e'_V) / (3 \times c'_{a1})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,V} = 1.000$$

Modification factor for edge distance

$$\psi_{h,V} = 1.0 = 1.000$$

Nominal concrete break out strength in shear

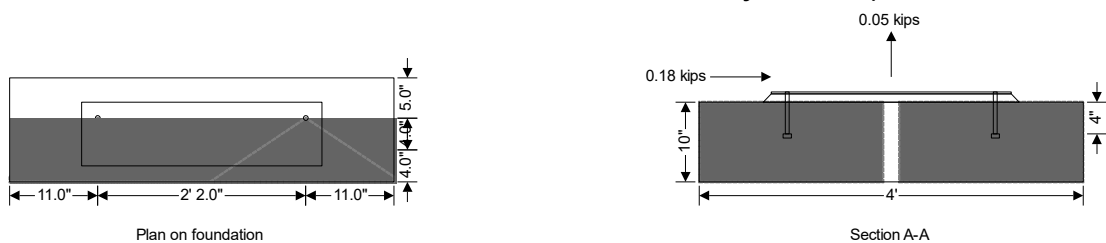
$$V_{cbg} = A_{Vc} / A_{Vco} \times \psi_{ec,V} \times \psi_{ed,V} \times \psi_{c,V} \times \psi_{h,V} \times V_b = 4.87 \text{ kips}$$

Concrete break out strength in shear

$$\phi V_{cbg} = \phi_{v,c} \times V_{cbg} = 3.41 \text{ kips}$$

PASS - Shear breakout perpendicular to edge strength exceeds shear in bolts

Concrete breakout strength in shear parallel to edge - Case 2. All shear resisted by rear bolts (parallel to edge - Case 2. All shear resisted by rear bolts)



Applied shear

$$V_{app} = V = 0.18 \text{ kips}$$

Edge distance x for shear near corner

$$c_{a1,p} = 8 \text{ in}$$

Edge distance y for shear near corner

$$c_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{bolt} - 1)/2) \times s_{bolt}) = 11 \text{ in}$$

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Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 4 \text{ in}$$

Basic concrete breakout strength

$$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{(d_a) \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c'_{a1,p})^{1.5}} = 13.54 \text{ kips}$$

$$V_{b,p2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c'_{a1,p})^{1.5} = 16.24 \text{ kips}$$

Basic concrete breakout strength

$$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 13.54 \text{ kips}$$

Projected area of a single anchor

$$A_{V_{co,p}} = 4.5 \times c'_{a1,p}{}^2 = 338 \text{ in}^2$$

Projected area of a group of anchors

$$A_{V_{c,p}} = 480 \text{ in}^2$$

Mod factor for edge effect

$$\psi_{ed,V,p} = 1.000$$

Eccentricity of loading

$$e'_{V,p} = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,V,p} = \min(1, 1 / (1 + ((2 \times e'_{V,p}) / (3 \times c'_{a1,p})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,V} = 1.000$$

Modification factor for edge distance

$$\psi_{h,V,p} = \max(\sqrt{(1.5 \times c'_{a1,p} / h_a)}, 1) = 1.140$$

Nominal concrete break out strength in shear

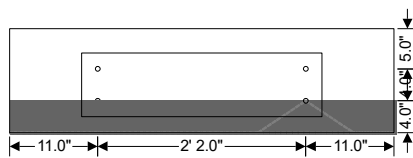
$$V_{cb,p} = 2 \times A_{V_{c,p}} / A_{V_{co,p}} \times \psi_{ed,V,p} \times \psi_{c,V} \times \psi_{h,V,p} \times V_{b,p} = 43.83 \text{ kips}$$

Concrete break out strength in shear

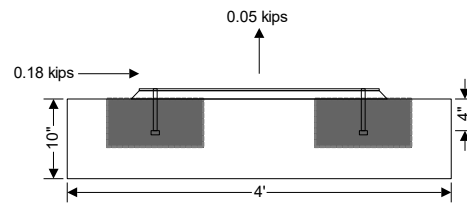
$$\phi V_{cb,p} = \phi_{v,c} \times V_{cb,p} = 30.68 \text{ kips}$$

PASS - Shear breakout strength parallel to edge exceeds shear in bolts

Concrete breakout strength in shear parallel to edge - Case 1. Half of shear resisted by front bolts (parallel to edge - Case 1. Half of shear resisted by front bolts)



Plan on foundation



Section A-A

Concrete breakout - side shear

Applied shear

$$V_{app} = V / 2 = 0.09 \text{ kips}$$

Edge distance x for shear near corner

$$c_{a1,p} = 4 \text{ in}$$

Edge distance y for shear near corner

$$c_{a2,p} = \min(x_{ce1}, x_{ce2}) - (((N_{boltx} - 1) / 2) \times s_{boltx}) = 11 \text{ in}$$

Load bearing length of anchor

$$l_e = \min(h_{ef}, 8 \times d_a) = 4 \text{ in}$$

Basic concrete breakout strength

$$V_{b,p1} = 7 \times (l_e / d_a)^{0.2} \times \sqrt{(d_a) \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi})} \times (c_{a1,p})^{1.5}} = 4.24 \text{ kips}$$

$$V_{b,p2} = 9 \times \lambda_a \times \sqrt{(f'_c \times 1 \text{ psi} \times 1 \text{ in})} \times (c_{a1,p})^{1.5} = 5.09 \text{ kips}$$

Basic concrete breakout strength

$$V_{b,p} = \text{Min}(V_{b,p1}, V_{b,p2}) = 4.24 \text{ kips}$$

Projected area of a single anchor

$$A_{V_{co,p}} = 4.5 \times c_{a1,p}{}^2 = 72 \text{ in}^2$$

Projected area of a group of anchors

$$A_{V_{c,p}} = 144 \text{ in}^2$$

Mod factor for edge effect

$$\psi_{ed,V,p} = 1.000$$

Eccentricity of loading

$$e'_{V,p} = 0 \text{ in}$$

Modification factor of eccentric loading

$$\psi_{ec,V,p} = \min(1, 1 / (1 + ((2 \times e'_{V,p}) / (3 \times c_{a1,p})))) = 1.000$$

Modification factor for cracking

$$\psi_{c,V} = 1.000$$

Modification factor for edge distance

$$\psi_{h,V,p} = 1.0 = 1.000$$

Nominal concrete break out strength in shear

$$V_{cb,p} = 2 \times A_{V_{c,p}} / A_{V_{co,p}} \times \psi_{ed,V,p} \times \psi_{c,V} \times \psi_{h,V,p} \times V_{b,p} = 16.98 \text{ kips}$$

Concrete break out strength in shear

$$\phi V_{cb,p} = \phi_{v,c} \times V_{cb,p} = 11.88 \text{ kips}$$

PASS - Shear breakout strength parallel to edge exceeds shear in bolts

Pryout strength of anchor in shear (D.6.3)

Coefficient of prying strength

$$k_{cp} = 2.0$$

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Nominal pryout strength of anchor in shear

$$V_{cp} = k_{cp} \times N_{cb} \times N_{boltV} = \mathbf{40.73 \text{ kips}}$$

Pryout strength of anchor in shear

$$\phi V_{cp} = \phi_{v,cb} \times V_{cp} = \mathbf{28.51 \text{ kips}}$$

PASS - Pryout strength of anchor exceeds shear in bolts

Interaction of tensile and shear forces

Critical design strength in tension

$$\phi N_n = \phi N_{sa} = \mathbf{6.17 \text{ kips}}$$

Critical applied tensile force

$$N_{ua} = N_{max,s} = \mathbf{0.02 \text{ kips}}$$

$$N_{ua} / \phi N_n = \mathbf{0.004}$$

Critical design strength in shear

$$\phi V_n = \phi V_{cbg,r} = \mathbf{3.41 \text{ kips}}$$

Critical applied shear force

$$V_{ua} = \text{abs}(V) = \mathbf{0.18 \text{ kips}}$$

$$V_{ua} / \phi V_n = \mathbf{0.052}$$

Full strength in both shear and tension are permitted

PASS - Applied tension and shear are less than tension and shear capacities




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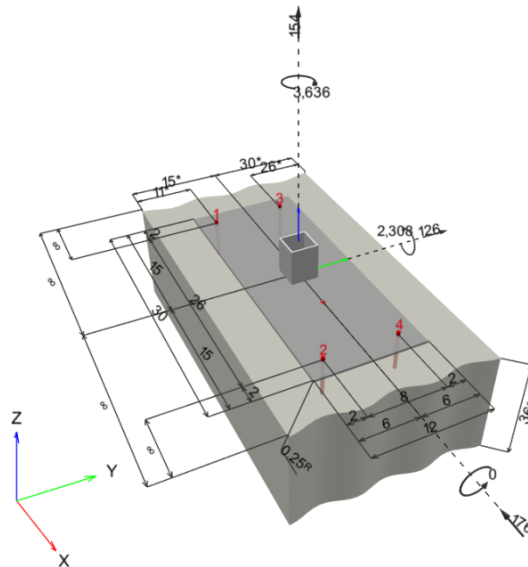
Specifier's comments: Abutment & Straddle Bent Sides

1 Input data

Anchor type and diameter:	HDA-PR M10x100/20	
Item number:	339346 HDA-PR M10x100/20	
Effective embedment depth:	$h_{ef} = 3.937 \text{ in.}, h_{nom} = 3.937 \text{ in.}$	
Material:	1.4401, 1.4404, 1.4571	
Evaluation Service Report:	ESR-1546	
Issued Valid:	3/1/2018 3/1/2020	
Proof:	Design Method ACI 318 / AC193	
Stand-off installation:	$e_b = 0.000 \text{ in.}$ (no stand-off); $t = 0.250 \text{ in.}$	
Anchor plate ^R :	$l_x \times l_y \times t = 30.000 \text{ in.} \times 12.000 \text{ in.} \times 0.250 \text{ in.}$; (Recommended plate thickness: not calculated)	
Profile:	Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. x 3.000 in. x 0.188 in.	
Base material:	cracked concrete, 5000, $f'_c = 5,000 \text{ psi}$; $h = 36.000 \text{ in.}$	
Reinforcement:	tension: condition B, shear: condition B; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar	
Seismic loads (cat. C, D, E, or F)	no	

^R - The anchor calculation is based on a rigid anchor plate assumption.

Geometry [in.] & Loading [lb, in.lb]



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1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 154; V _x = -176; V _y = 126; M _x = 0; M _y = -2,308; M _z = -3,636;	no	3

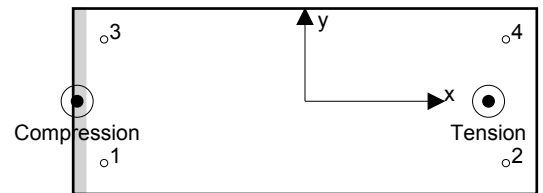
2 Load case/Resulting anchor forces

Load case: Design loads

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	4	115	-64	95
2	82	71	-64	-32
3	4	98	-24	95
4	82	41	-24	-32



max. concrete compressive strain: 0.00 [‰]
 max. concrete compressive stress: 4 [psi]
 resulting tension force in (x/y)=(11.877/0.000): 172 [lb]
 resulting compression force in (x/y)=(-14.743/0.000): 18 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N _{ua} [lb]	Capacity φ N _n [lb]	Utilization β _N = N _{ua} /φ N _n	Status
Steel Strength*	82	7,830	2	OK
Pullout Strength*	82	8,266	1	OK
Concrete Breakout Failure**	172	9,602	2	OK

* highest loaded anchor **anchor group (anchors in tension)



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3.1 Steel Strength

N_{sa} = ESR value refer to ICC-ES ESR-1546
 $\phi N_{sa} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

$A_{se,N}$ [in. ²]	f_{uta} [psi]
0.09	116,000

Calculations

N_{sa} [lb]
10,440

Results

N_{sa} [lb]	ϕ_{steel}	ϕN_{sa} [lb]	N_{ua} [lb]
10,440	0.750	7,830	82

3.2 Pullout Strength

$N_{pn,f_c} = N_{p,2500} (f_c'/2500)^{0.5}$ refer to ICC-ES ESR-1546
 $\phi N_{pn,f_c} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

f_c' [psi]	$N_{p,2500}$ [lb]
5,000	8,992

Calculations

$(f_c'/2500)^{0.5}$
1.414

Results

N_{pn,f_c} [lb]	$\phi_{concrete}$	$\phi N_{pn,f_c}$ [lb]	N_{ua} [lb]
12,717	0.650	8,266	82

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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3.3 Concrete Breakout Failure

$$N_{cbg} = \left(\frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \quad \text{ACI 318-08 Eq. (D-5)}$$

$$\phi N_{cbg} \geq N_{ua} \quad \text{ACI 318-08 Eq. (D-1)}$$

A_{Nc} see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]	$\psi_{c,N}$
3.937	11.877	0.000	11.000	1.000
c_{ac} [in.]	k_c	λ	f_c [psij]	
0.000	24	1	5,000	

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\psi_{ec1,N}$	$\psi_{ec2,N}$	$\psi_{ed,N}$	$\psi_{cp,N}$	N_b [lb]
468.54	139.71	0.332	1.000	1.000	1.000	13,257

Results

N_{cbg} [lb]	$\phi_{concrete}$	ϕN_{cbg} [lb]	N_{ua} [lb]
14,772	0.650	9,602	172

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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4 Shear load

	Load V_{ua} [lb]	Capacity ϕV_n [lb]	Utilization $\beta_v = V_{ua}/\phi V_n$	Status
Steel Strength*	115	3,945	3	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength*	115	15,561	1	OK
Concrete edge failure in direction y-**	188	21,440	1	OK

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel Strength

V_{sa} = ESR value refer to ICC-ES ESR-1546
 $\phi V_{steel} \geq V_{ua}$ ACI 318-08 Eq. (D-2)

Variables

$A_{se,V}$ [in. ²]	f_{uta} [psi]	$\alpha_{v,seis}$
0.09	116,000	0.926

Calculations

V_{sa} [lb]
6,070

Results

V_{sa} [lb]	ϕ_{steel}	ϕV_{sa} [lb]	V_{ua} [lb]
6,070	0.650	3,945	115



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4.2 Pryout Strength

$$V_{cp} = k_{cp} \left[\left(\frac{A_{Nc}}{A_{Nc0}} \right) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \right] \quad \text{ACI 318-08 Eq. (D-30)}$$

$$\phi V_{cp} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

$$A_{Nc} \text{ see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)}$$

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\Psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_{c,N}}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\Psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\Psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

k_{cp}	h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]
2	3.937	0.000	0.000	11.000
$\Psi_{c,N}$	c_{ac} [in.]	k_c	λ	f_c [psi]
1.000	-	24	1	5,000

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\Psi_{ec1,N}$	$\Psi_{ec2,N}$	$\Psi_{ed,N}$	$\Psi_{cp,N}$	N_b [lb]
117.14	139.71	1.000	1.000	1.000	1.000	13,257

Results

V_{cp} [lb]	$\phi_{concrete}$	ϕV_{cp} [lb]	V_{ua} [lb]
22,230	0.700	15,561	115

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4.3 Concrete edge failure in direction y-

$$V_{cbg} = \left(\frac{A_{Vc}}{A_{Vc0}} \right) \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} \Psi_{parallel,V} V_b \quad \text{ACI 318-08 Eq. (D-22)}$$

$$\phi V_{cbg} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

A_{Vc} see ACI 318-08, Part D.6.2.1, Fig. RD.6.2.1(b)

$$A_{Vc0} = 4.5 c_{a1}^2 \quad \text{ACI 318-08 Eq. (D-23)}$$

$$\Psi_{ec,V} = \left(\frac{1}{1 + \frac{2e_v}{3c_{a1}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-26)}$$

$$\Psi_{ed,V} = 0.7 + 0.3 \left(\frac{c_{a2}}{1.5c_{a1}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-28)}$$

$$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \geq 1.0 \quad \text{ACI 318-08 Eq. (D-29)}$$

$$V_b = \left(7 \left(\frac{l_e}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda \sqrt{f'_c} c_{a1}^{1.5} \quad \text{ACI 318-08 Eq. (D-24)}$$

Variables

c_{a1} [in.]	c_{a2} [in.]	e_{cV} [in.]	$\Psi_{c,V}$	h_a [in.]
11.000	-	4.489	1.000	36.000
l_e [in.]	λ	d_a [in.]	f'_c [psi]	$\Psi_{parallel,V}$
3.940	1.000	0.750	5,000	1.000

Calculations

A_{Vc} [in. ²]	A_{Vc0} [in. ²]	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{h,V}$	V_b [lb]
973.50	544.50	0.786	1.000	1.000	21,792

Results

V_{cbg} [lb]	$\phi_{concrete}$	ϕV_{cbg} [lb]	V_{ua} [lb]
30,629	0.700	21,440	188

5 Combined tension and shear loads

β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
0.018	0.029	5/3	1	OK

$$\beta_{NV} = \beta_N^{\zeta} + \beta_V^{\zeta} \leq 1$$

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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6 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2018, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>

Fastening meets the design criteria!

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7 Installation data

Profile: Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. x 3.000 in. x 0.188 in.

Hole diameter in the fixture: $d_f = 0.472$ in.

Plate thickness (input): 0.250 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Manual cleaning of the drilled hole according to instructions for use is required.

Anchor type and diameter: HDA-PR M10x100/20

Item number: 339346 HDA-PR M10x100/20

Installation torque: 443 in.lb

Hole diameter in the base material: 0.787 in.

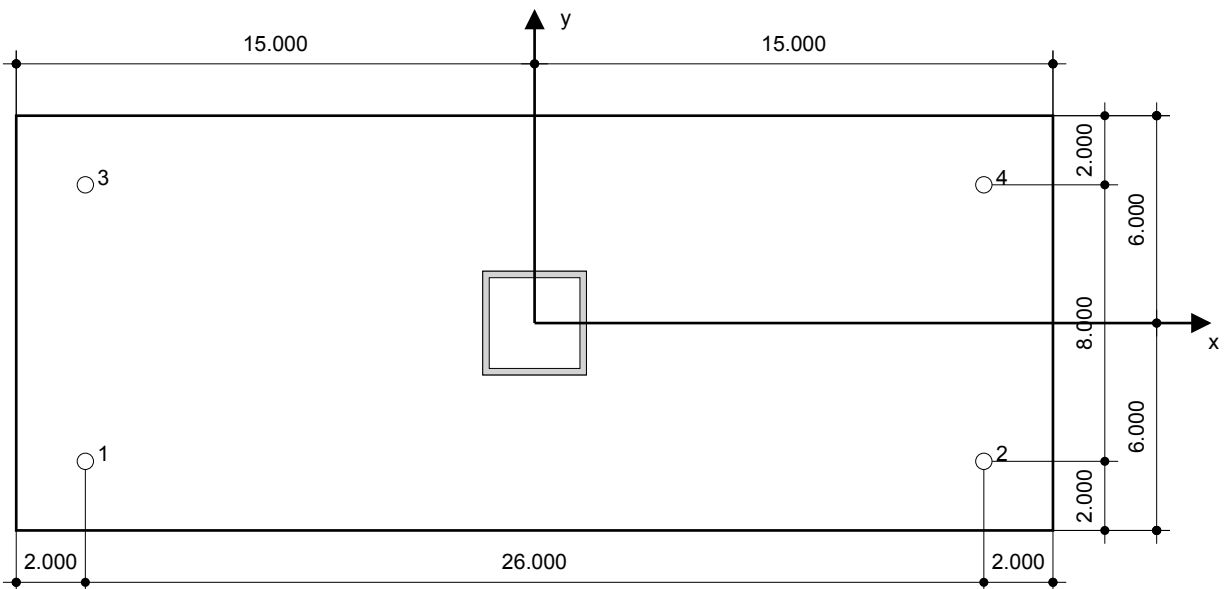
Hole depth in the base material: 4.213 in.

Minimum thickness of the base material: 7.100 in.

Hilti HDA undercut anchor with 3.937008 in embedment, M10x100/20, Stainless steel, installation per ESR-1546

7.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> Suitable Rotary Hammer Properly sized stop drill bit for specific drill depth 	<ul style="list-style-type: none"> Manual blow-out pump 	<ul style="list-style-type: none"> HDA-ST setting tool Torque wrench



Coordinates Anchor in.

Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}
1	-13.000	-4.000	-	-	11.000	34.000
2	13.000	-4.000	-	-	11.000	34.000
3	-13.000	4.000	-	-	19.000	26.000
4	13.000	4.000	-	-	19.000	26.000

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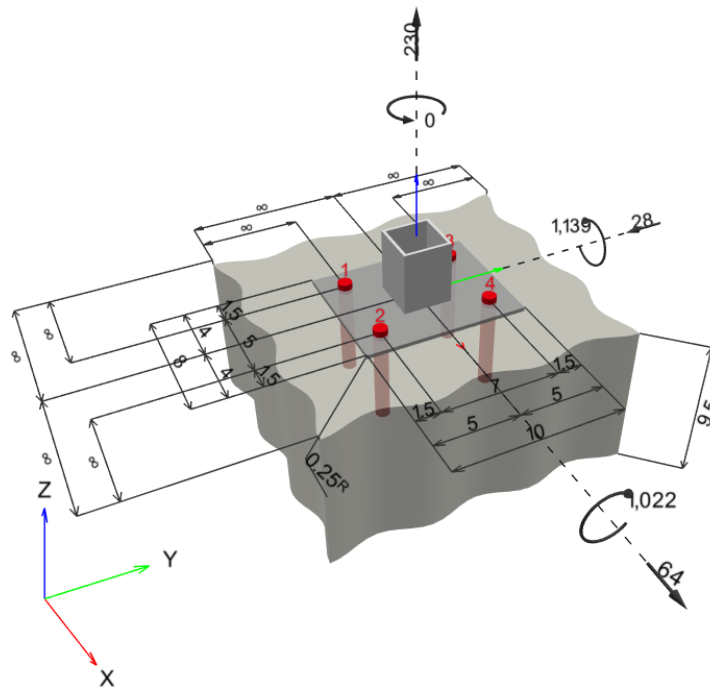
Specifier's comments: Straddle Bent Middle

1 Input data

Anchor type and diameter:	Hex Head ASTM F 1554 GR. 36 7/8	
Item number:	not available	
Effective embedment depth:	$h_{ef} = 5.724$ in.	
Material:	ASTM F 1554	
Proof:	Design Method ACI 318-08 / CIP	
Stand-off installation:	$e_b = 0.000$ in. (no stand-off); $t = 0.250$ in.	
Anchor plate ^R :	$l_x \times l_y \times t = 8.000$ in. \times 10.000 in. \times 0.250 in.; (Recommended plate thickness: not calculated)	
Profile:	Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. \times 3.000 in. \times 0.188 in.	
Base material:	cracked concrete, 5000, $f'_c = 5,000$ psi; $h = 9.500$ in.	
Reinforcement:	tension: condition B, shear: condition B; edge reinforcement: none or < No. 4 bar	
Seismic loads (cat. C, D, E, or F)	no	

^R - The anchor calculation is based on a rigid anchor plate assumption.

Geometry [in.] & Loading [lb, in.lb]



Input data and results must be checked for conformity with the existing conditions and for plausibility!
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1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 230; V _x = 64; V _y = -28; M _x = -1,022; M _y = -1,139; M _z = 0;	no	2

2 Load case/Resulting anchor forces

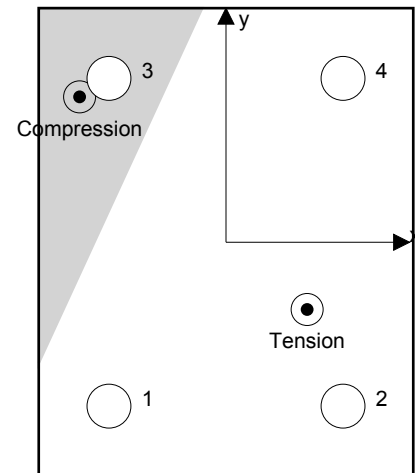
Load case: Design loads

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	59	17	16	-7
2	211	17	16	-7
3	0	17	16	-7
4	113	17	16	-7

max. concrete compressive strain: 0.01 [‰]
 max. concrete compressive stress: 35 [psi]
 resulting tension force in (x/y)=(1.733/-1.436): 382 [lb]
 resulting compression force in (x/y)=(-3.127/3.105): 152 [lb]



Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N _{ua} [lb]	Capacity φ N _n [lb]	Utilization β _N = N _{ua} /φ N _n	Status
Steel Strength*	211	20,097	2	OK
Pullout Strength*	211	24,948	1	OK
Concrete Breakout Failure**	382	24,254	2	OK
Concrete Side-Face Blowout, direction **	N/A	N/A	N/A	N/A

* highest loaded anchor **anchor group (anchors in tension)



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3.1 Steel Strength

$N_{sa} = A_{se,N} f_{uta}$ ACI 318-08 Eq. (D-3)
 $\phi N_{sa} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

$A_{se,N}$ [in. ²]	f_{uta} [psi]
0.46	58,000

Calculations

N_{sa} [lb]
26,796

Results

N_{sa} [lb]	ϕ_{steel}	ϕN_{sa} [lb]	N_{ua} [lb]
26,796	0.750	20,097	211

3.2 Pullout Strength

$N_{pN} = \psi_{c,p} N_p$ ACI 318-08 Eq. (D-14)
 $N_p = 8 A_{brg} f'_c$ ACI 318-08 Eq. (D-15)
 $\phi N_{pN} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

$\psi_{c,p}$	A_{brg} [in. ²]	f'_c [psi]
1.000	0.89	5,000

Calculations

N_p [lb]
35,640

Results

N_{pn} [lb]	$\phi_{concrete}$	ϕN_{pn} [lb]	N_{ua} [lb]
35,640	0.700	24,948	211

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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3.3 Concrete Breakout Failure

$$N_{cbg} = \left(\frac{A_{Nc}}{A_{Nc0}} \right) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \quad \text{ACI 318-08 Eq. (D-5)}$$

$$\phi N_{cbg} \geq N_{ua} \quad \text{ACI 318-08 Eq. (D-1)}$$

A_{Nc} see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\Psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\Psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\Psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]	$\Psi_{c,N}$
5.724	0.900	0.269	∞	1.000
c_{ac} [in.]	k_c	λ	f_c [psij]	
0.000	24	1	5,000	

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\Psi_{ec1,N}$	$\Psi_{ec2,N}$	$\Psi_{ed,N}$	$\Psi_{cp,N}$	N_b [lb]
500.94	294.88	0.905	0.970	1.000	1.000	23,241

Results

N_{cbg} [lb]	$\phi_{concrete}$	ϕN_{cbg} [lb]	N_{ua} [lb]
34,649	0.700	24,254	382

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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4 Shear load

	Load V_{ua} [lb]	Capacity ϕV_n [lb]	Utilization $\beta_v = V_{ua}/\phi V_n$	Status
Steel Strength*	17	10,450	1	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength**	70	59,136	1	OK
Concrete edge failure in direction **	N/A	N/A	N/A	N/A

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel Strength

$$V_{sa} = 0.6 A_{se,V} f_{uta} \quad \text{ACI 318-08 Eq. (D-20)}$$

$$\phi V_{steel} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

Variables

$A_{se,V}$ [in. ²]	f_{uta} [psi]
0.46	58,000

Calculations

V_{sa} [lb]
16,078

Results

V_{sa} [lb]	ϕ_{steel}	ϕV_{sa} [lb]	V_{ua} [lb]
16,078	0.650	10,450	17

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4.2 Pryout Strength

$$V_{cp,g} = k_{cp} \left[\left(\frac{A_{Nc}}{A_{Nc0}} \right) \Psi_{ec,N} \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \right] \quad \text{ACI 318-08 Eq. (D-31)}$$

$$\phi V_{cp,g} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

 A_{Nc} see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\Psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\Psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\Psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

k_{cp}	h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]
2	5.724	0.000	0.000	∞
$\Psi_{c,N}$	c_{ac} [in.]	k_c	λ	f_c [psi]
1.000	-	24	1	5,000

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\Psi_{ec1,N}$	$\Psi_{ec2,N}$	$\Psi_{ed,N}$	$\Psi_{cp,N}$	N_b [lb]
535.94	294.88	1.000	1.000	1.000	1.000	23,241

Results

$V_{cp,g}$ [lb]	$\phi_{concrete}$	$\phi V_{cp,g}$ [lb]	V_{ua} [lb]
84,479	0.700	59,136	70

5 Combined tension and shear loads

β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
0.016	0.002	5/3	1	OK

$$\beta_{NV} = \beta_N^\zeta + \beta_V^\zeta \leq 1$$



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6 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2018, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
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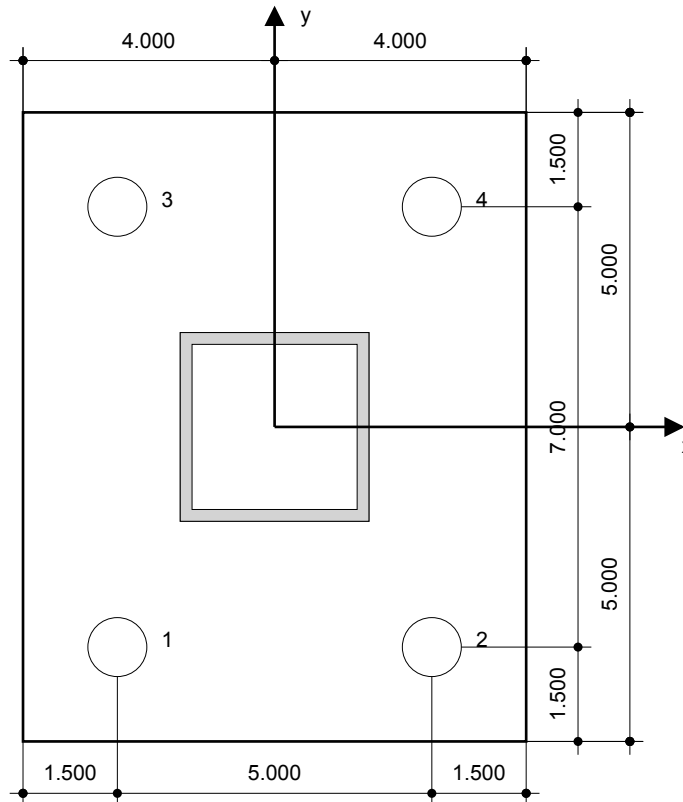
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7 Installation data

Profile: Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. x 3.000 in. x 0.188 in.
 Hole diameter in the fixture: $d_f = 0.938$ in.
 Plate thickness (input): 0.250 in.
 Recommended plate thickness: not calculated

Anchor type and diameter: Hex Head ASTM F 1554 GR. 36 7/8
 Item number: not available
 Installation torque: -
 Hole diameter in the base material: - in.
 Hole depth in the base material: 5.724 in.
 Minimum thickness of the base material: 6.776 in.

Hilti Hex Head headed stud anchor with 5.724 in embedment, 7/8, Steel galvanized, installation per instruction for use



Coordinates Anchor in.

Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}
1	-2.500	-3.500	-	-	-	-
2	2.500	-3.500	-	-	-	-
3	-2.500	3.500	-	-	-	-
4	2.500	3.500	-	-	-	-

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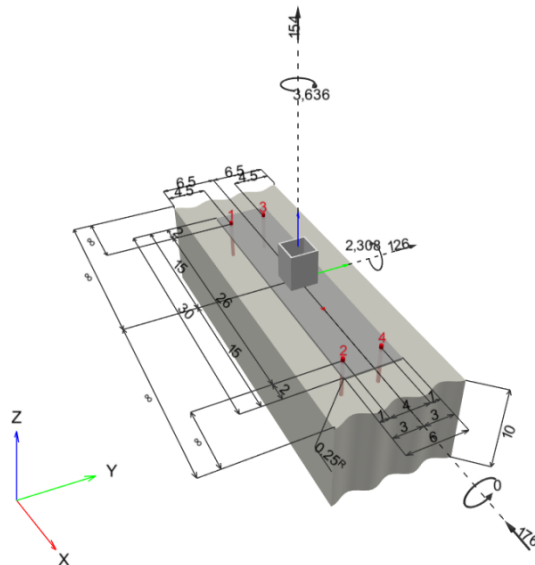
Specifier's comments: MSE Wall

1 Input data

Anchor type and diameter:	HDA-PR M10x100/20	
Item number:	339346 HDA-PR M10x100/20	
Effective embedment depth:	$h_{ef} = 3.937 \text{ in.}, h_{nom} = 3.937 \text{ in.}$	
Material:	1.4401, 1.4404, 1.4571	
Evaluation Service Report:	ESR-1546	
Issued Valid:	3/1/2018 3/1/2020	
Proof:	Design Method ACI 318 / AC193	
Stand-off installation:	$e_b = 0.000 \text{ in.}$ (no stand-off); $t = 0.250 \text{ in.}$	
Anchor plate ^R :	$l_x \times l_y \times t = 30.000 \text{ in.} \times 6.000 \text{ in.} \times 0.250 \text{ in.}$; (Recommended plate thickness: not calculated)	
Profile:	Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. x 3.000 in. x 0.188 in.	
Base material:	cracked concrete, 5000, $f'_c = 5,000 \text{ psi}$; $h = 10.000 \text{ in.}$	
Reinforcement:	tension: condition B, shear: condition B; no supplemental splitting reinforcement present edge reinforcement: none or < No. 4 bar	
Seismic loads (cat. C, D, E, or F)	no	

^R - The anchor calculation is based on a rigid anchor plate assumption.

Geometry [in.] & Loading [lb, in.lb]



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1.1 Design results

Case	Description	Forces [lb] / Moments [in.lb]	Seismic	Max. Util. Anchor [%]
1	Combination 1	N = 154; V _x = -176; V _y = 126; M _x = 0; M _y = -2,308; M _z = -3,636;	no	9

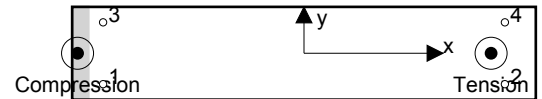
2 Load case/Resulting anchor forces

Load case: Design loads

Anchor reactions [lb]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	3	114	-55	100
2	82	66	-55	-37
3	3	105	-33	100
4	82	50	-33	-37



max. concrete compressive strain: 0.00 [‰]
 max. concrete compressive stress: 5 [psi]
 resulting tension force in (x/y)=(12.107/0.000): 171 [lb]
 resulting compression force in (x/y)=(-14.653/0.000): 17 [lb]

Anchor forces are calculated based on the assumption of a rigid anchor plate.

3 Tension load

	Load N _{ua} [lb]	Capacity φ N _n [lb]	Utilization β _N = N _{ua} /φ N _n	Status
Steel Strength*	82	7,830	2	OK
Pullout Strength*	82	8,266	1	OK
Concrete Breakout Failure**	171	5,773	3	OK

* highest loaded anchor **anchor group (anchors in tension)



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3.1 Steel Strength

N_{sa} = ESR value refer to ICC-ES ESR-1546
 $\phi N_{sa} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

$A_{se,N}$ [in. ²]	f_{uta} [psi]
0.09	116,000

Calculations

N_{sa} [lb]
10,440

Results

N_{sa} [lb]	ϕ_{steel}	ϕN_{sa} [lb]	N_{ua} [lb]
10,440	0.750	7,830	82

3.2 Pullout Strength

$N_{pn,f_c} = N_{p,2500} (f_c'/2500)^{0.5}$ refer to ICC-ES ESR-1546
 $\phi N_{pn,f_c} \geq N_{ua}$ ACI 318-08 Eq. (D-1)

Variables

f_c' [psi]	$N_{p,2500}$ [lb]
5,000	8,992

Calculations

$(f_c'/2500)^{0.5}$
1.414

Results

N_{pn,f_c} [lb]	$\phi_{concrete}$	$\phi N_{pn,f_c}$ [lb]	N_{ua} [lb]
12,717	0.650	8,266	82



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3.3 Concrete Breakout Failure

$$N_{cbg} = \left(\frac{A_{Nc}}{A_{Nc0}} \right) \psi_{ec,N} \psi_{ed,N} \psi_{c,N} \psi_{cp,N} N_b \quad \text{ACI 318-08 Eq. (D-5)}$$

$$\phi N_{cbg} \geq N_{ua} \quad \text{ACI 318-08 Eq. (D-1)}$$

A_{Nc} see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_N}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]	$\psi_{c,N}$
3.937	12.107	0.000	4.500	1.000
c_{ac} [in.]	k_c	λ	f_c [psij]	
0.000	24	1	5,000	

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\psi_{ec1,N}$	$\psi_{ec2,N}$	$\psi_{ed,N}$	$\psi_{cp,N}$	N_b [lb]
307.32	139.71	0.328	1.000	0.928	1.000	13,257

Results

N_{cbg} [lb]	$\phi_{concrete}$	ϕN_{cbg} [lb]	N_{ua} [lb]
8,881	0.650	5,773	171

Input data and results must be checked for conformity with the existing conditions and for plausibility!
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4 Shear load

	Load V_{ua} [lb]	Capacity ϕV_n [lb]	Utilization $\beta_v = V_{ua}/\phi V_n$	Status
Steel Strength*	114	3,945	3	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout Strength*	114	9,476	2	OK
Concrete edge failure in direction y+**	266	3,265	9	OK

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel Strength

V_{sa} = ESR value refer to ICC-ES ESR-1546
 $\phi V_{steel} \geq V_{ua}$ ACI 318-08 Eq. (D-2)

Variables

$A_{se,V}$ [in. ²]	f_{uta} [psi]	$\alpha_{v,seis}$
0.09	116,000	0.926

Calculations

V_{sa} [lb]
6,070

Results

V_{sa} [lb]	ϕ_{steel}	ϕV_{sa} [lb]	V_{ua} [lb]
6,070	0.650	3,945	114



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4.2 Pryout Strength

$$V_{cp} = k_{cp} \left[\left(\frac{A_{Nc}}{A_{Nc0}} \right) \Psi_{ed,N} \Psi_{c,N} \Psi_{cp,N} N_b \right] \quad \text{ACI 318-08 Eq. (D-30)}$$

$$\phi V_{cp} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

A_{Nc} see ACI 318-08, Part D.5.2.1, Fig. RD.5.2.1(b)

$$A_{Nc0} = 9 h_{ef}^2 \quad \text{ACI 318-08 Eq. (D-6)}$$

$$\Psi_{ec,N} = \left(\frac{1}{1 + \frac{2 e_{c,N}}{3 h_{ef}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-9)}$$

$$\Psi_{ed,N} = 0.7 + 0.3 \left(\frac{c_{a,min}}{1.5 h_{ef}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-11)}$$

$$\Psi_{cp,N} = \text{MAX} \left(\frac{c_{a,min}}{c_{ac}}, \frac{1.5 h_{ef}}{c_{ac}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-13)}$$

$$N_b = k_c \lambda \sqrt{f'_c} h_{ef}^{1.5} \quad \text{ACI 318-08 Eq. (D-7)}$$

Variables

k_{cp}	h_{ef} [in.]	$e_{c1,N}$ [in.]	$e_{c2,N}$ [in.]	$c_{a,min}$ [in.]
2	3.937	0.000	0.000	4.500
$\Psi_{c,N}$	c_{ac} [in.]	k_c	λ	f'_c [psi]
1.000	-	24	1	5,000

Calculations

A_{Nc} [in. ²]	A_{Nc0} [in. ²]	$\Psi_{ec1,N}$	$\Psi_{ec2,N}$	$\Psi_{ed,N}$	$\Psi_{cp,N}$	N_b [lb]
76.83	139.71	1.000	1.000	0.928	1.000	13,257

Results

V_{cp} [lb]	$\phi_{concrete}$	ϕV_{cp} [lb]	V_{ua} [lb]
13,537	0.700	9,476	114

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4.3 Concrete edge failure in direction y+

$$V_{cbg} = \left(\frac{A_{Vc}}{A_{Vc0}} \right) \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} \Psi_{parallel,V} V_b \quad \text{ACI 318-08 Eq. (D-22)}$$

$$\phi V_{cbg} \geq V_{ua} \quad \text{ACI 318-08 Eq. (D-2)}$$

 A_{Vc} see ACI 318-08, Part D.6.2.1, Fig. RD.6.2.1(b)

$$A_{Vc0} = 4.5 c_{a1}^2 \quad \text{ACI 318-08 Eq. (D-23)}$$

$$\Psi_{ec,V} = \left(\frac{1}{1 + \frac{2e_v}{3c_{a1}}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-26)}$$

$$\Psi_{ed,V} = 0.7 + 0.3 \left(\frac{c_{a2}}{1.5c_{a1}} \right) \leq 1.0 \quad \text{ACI 318-08 Eq. (D-28)}$$

$$\Psi_{h,V} = \sqrt{\frac{1.5c_{a1}}{h_a}} \geq 1.0 \quad \text{ACI 318-08 Eq. (D-29)}$$

$$V_b = \left(7 \left(\frac{l_e}{d_a} \right)^{0.2} \sqrt{d_a} \right) \lambda \sqrt{f'_c} c_{a1}^{1.5} \quad \text{ACI 318-08 Eq. (D-24)}$$

Variables

c_{a1} [in.]	c_{a2} [in.]	e_{cV} [in.]	$\Psi_{c,V}$	h_a [in.]
4.500	-	9.751	1.000	10.000
l_e [in.]	λ	d_a [in.]	f'_c [psi]	$\Psi_{parallel,V}$
3.940	1.000	0.750	5,000	1.000

Calculations

A_{Vc} [in. ²]	A_{Vc0} [in. ²]	$\Psi_{ec,V}$	$\Psi_{ed,V}$	$\Psi_{h,V}$	V_b [lb]
182.25	91.13	0.409	1.000	1.000	5,702

Results

V_{cbg} [lb]	$\phi_{concrete}$	ϕV_{cbg} [lb]	V_{ua} [lb]
4,665	0.700	3,265	266

5 Combined tension and shear loads

β_N	β_V	ζ	Utilization $\beta_{N,V}$ [%]	Status
0.030	0.081	5/3	2	OK

$$\beta_{NV} = \beta_N^{\zeta} + \beta_V^{\zeta} \leq 1$$



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6 Warnings

- The anchor design methods in PROFIS Engineering require rigid anchor plates per current regulations (AS 5216:2018, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the anchor plate are not considered - the anchor plate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required anchor plate thickness with CBFEM to limit the stress of the anchor plate based on the assumptions explained above. The proof if the rigid anchor plate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Condition A applies where the potential concrete failure surfaces are crossed by supplementary reinforcement proportioned to tie the potential concrete failure prism into the structural member. Condition B applies where such supplementary reinforcement is not provided, or where pullout or pryout strength governs.
- Refer to the manufacturer's product literature for cleaning and installation instructions.
- For additional information about ACI 318 strength design provisions, please go to <https://submittals.us.hilti.com/PROFISAnchorDesignGuide/>

Fastening meets the design criteria!

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7 Installation data

Profile: Square HSS (AISC), HSS3X3X.1875; (L x W x T) = 3.000 in. x 3.000 in. x 0.188 in.

Hole diameter in the fixture: $d_f = 0.472$ in.

Plate thickness (input): 0.250 in.

Recommended plate thickness: not calculated

Drilling method: Hammer drilled

Cleaning: Manual cleaning of the drilled hole according to instructions for use is required.

Anchor type and diameter: HDA-PR M10x100/20

Item number: 339346 HDA-PR M10x100/20

Installation torque: 443 in.lb

Hole diameter in the base material: 0.787 in.

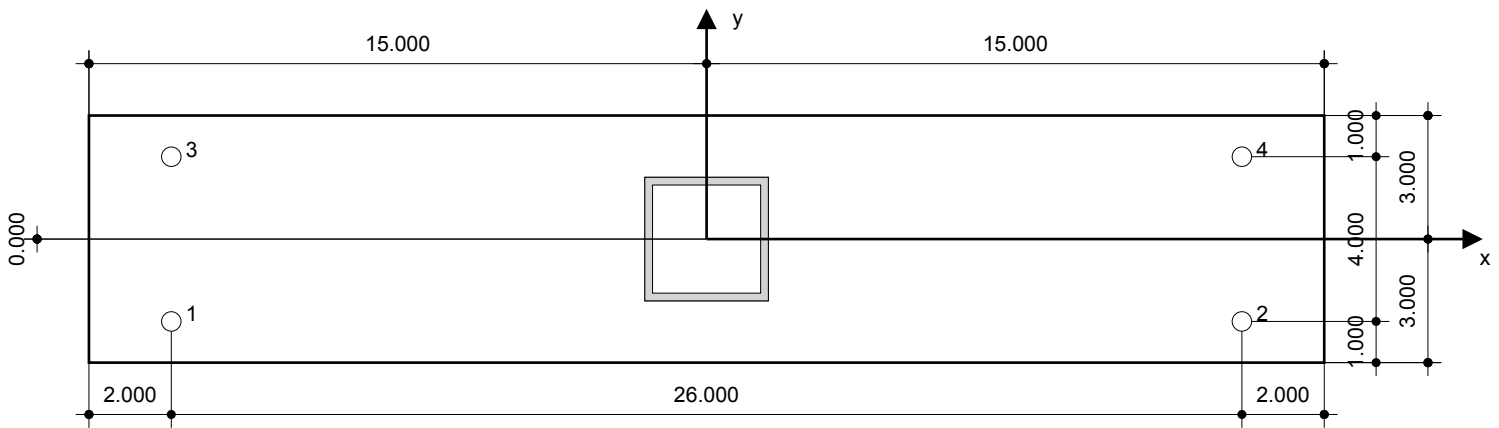
Hole depth in the base material: 4.213 in.

Minimum thickness of the base material: 7.100 in.

Hilti HDA undercut anchor with 3.937008 in embedment, M10x100/20, Stainless steel, installation per ESR-1546

7.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> • Suitable Rotary Hammer • Properly sized stop drill bit for specific drill depth 	<ul style="list-style-type: none"> • Manual blow-out pump 	<ul style="list-style-type: none"> • HDA-ST setting tool • Torque wrench



Coordinates Anchor in.

Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}
1	-13.000	-2.000	-	-	4.500	8.500
2	13.000	-2.000	-	-	4.500	8.500
3	-13.000	2.000	-	-	8.500	4.500
4	13.000	2.000	-	-	8.500	4.500

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8 Remarks; Your Cooperation Duties

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